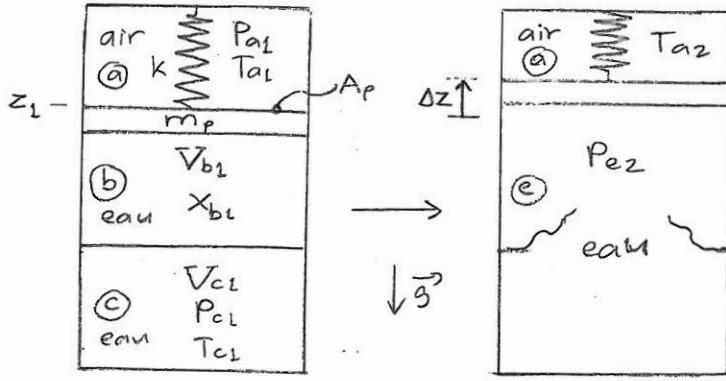


MEC1210 - Automne 2024: Mini-contrôle 1 (Solutionnaire)



- ①
- $P_{a1} = 50 \text{ kPa}$
 - $T_{a1} = 25^\circ\text{C}$
 - $z_1 = 1 \text{ cm} = 0.01 \text{ m}$
 - $V_{b1} = V_{c1} = 0.004 \text{ m}^3$
 - $X_{b1} = 0.883$
 - $P_{c1} = 600 \text{ kPa}$
 - $T_{c1} = 350^\circ\text{C}$
- ②
- $T_{a2} = 52^\circ\text{C}$
 - $\Delta z = 4.582 \text{ cm} = 0.04582 \text{ m}$
 - $P_{e2} = 300 \text{ kPa}$

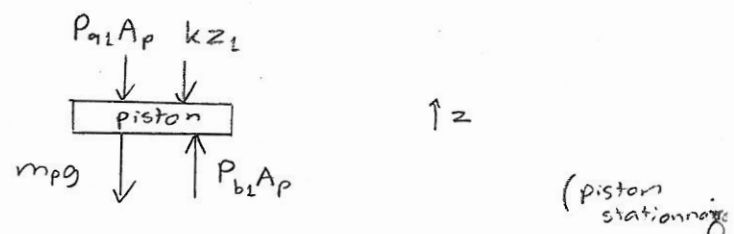
- $m_p = 16.3099 \text{ kg}$
- $A_p = 0.016 \text{ m}^2$
- $k = 64 \text{ kN/m}$
- Cylindre vertical, fixe, rigide
- Piston sans friction
- Isolant thermique parfait pour parois/piston ($Q_{\text{ext}}, Q_{\text{air-eau}} = 0$)
- Piston stationnaire à ① & ②
- $\Delta \bar{U}_{\text{piston, ressort, membrane}} = 0$
- air \rightarrow gaz parfait à c_p, c_v variables avec $R = 0.287 \frac{\text{kJ}}{\text{kg}\cdot\text{K}}$
- $\Delta E_{\text{air, eau}} = 0$

Suppositions additionnelles:

- mélange d'eau uniforme

- $m_{b1}, \text{phase}_{b1}, m_{c1}, \text{phase}_{c1} = ?$
- $P_{a2}, T_{e2} = ?$
- $\bar{W}_{\text{sur piston}} = ?$
- $m_a = ?$ (via 1^{ère} loi) & $\bar{V}_{a1} = ?$

- i) $m_{b1}, \text{phase}_{b1} = ? : P_{b1} = ?$



$$\Sigma F_z = P_{b1}A_p - P_{a1}A_p - m_p g - k z_1 = m_p g$$

$$P_{b1} = P_{a1} + \frac{m_p g}{A_p} + \frac{k z_1}{A_p}$$

$$= 50 \text{ kPa} + \frac{(16.3099 \text{ kg})(9.81 \text{ m/s}^2) \times 1 \text{ kPa}}{(0.016 \text{ m}^2)} + \frac{(64 \text{ kN/m})(0.01 \text{ m})}{(0.016 \text{ m}^2)} \times \frac{\text{kPa}}{\text{KN/m}^2}$$

$P_{b1} = 100 \text{ kPa}$

$P_{b1} = 100 \text{ kPa}$
 $x_{b1} = 0,883$

phase_{b1} = mélange liquide-vapeur saturé ($x_{b1} < 1$)

Table A-5: pour $P = 100 \text{ kPa}$, $v_f = 0.001043 \text{ m}^3/\text{kg}$
 $v_g = 1.6941$
 $(u_f = 417.40 \text{ kJ/kg})$
 $(u_{fg} = 2088.2)$

$v_{b1} = v_f + x_{b1}(v_g - v_f) = 0.001043 + 0.883(1.6941 - 0.001043)$
 $v_{b1} = 1.4960 \text{ m}^3/\text{kg}$ ($u_{b1} = u_f + x_{b1}u_{fg} = 2261.28 \text{ kJ/kg}$)

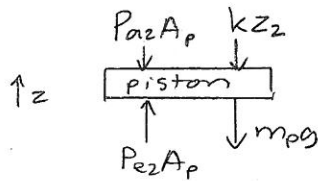
$m_{b1} = \frac{V_{b1}}{v_{b1}} = \frac{0.004 \text{ m}^3}{1.4960 \text{ m}^3/\text{kg}} = \boxed{2.6738 \times 10^{-3} \text{ kg}}$

ii) m_{c1} , phase_{c1} = ? : $P_{c1} = 600 \text{ kPa}$ } $T_{c1} > T_{\text{sat@600kPa}} = 158.83 \text{ }^\circ\text{C}$
 $T_{c1} = 350 \text{ }^\circ\text{C}$ } phase_{c1} = vapeur surchauffée

Table A-6: $v_{c1} = 0.47428 \text{ m}^3/\text{kg}$
 $(u_{c1} = 2881.6 \text{ kJ/kg})$

$m_{c1} = \frac{V_{c1}}{v_{c1}} = \frac{0.004 \text{ m}^3}{0.47428 \text{ m}^3/\text{kg}} = \boxed{8.4338 \times 10^{-3} \text{ kg}}$

b) i) $P_{a2} = ?$:



$\sum F_z = P_{e2} A_p - P_{a2} A_p - m_p g - k z_2 = m_p g \rightarrow 0$ (piston stationnaire)

$P_{a2} = P_{e2} - \frac{m_p g}{A_p} - \frac{k z_2}{A_p} \Rightarrow z_2 = z_1 + \Delta z = (1 + 4.582) \text{ cm}$
 $= 5.582 \text{ cm} = 0.05582 \text{ m}$

$P_{a2} = 300 \text{ kPa} - \frac{(16.3099 \text{ kg})(9.81 \frac{\text{m}}{\text{s}^2})}{(0.016 \text{ m}^2)} \times \frac{1 \text{ kPa}}{10^3 \frac{\text{kg} \cdot \text{m/s}^2}{\text{m}^2}} - \frac{(64 \frac{\text{kN}}{\text{m}})(0.05582 \text{ m})}{(0.016 \text{ m}^2)} \times \frac{\text{kPa}}{\text{kN/m}}$

$P_{a2} = 66.72 \text{ kPa}$

ii) $T_{e2} = ?$: $P_{e2} = 300 \text{ kPa}$

$v_{e2} = \frac{V_{e2}}{m_e} = \frac{V_{b1} + V_{c1} + A_p \Delta z}{m_{b1} + m_{c1}}$
 $= \frac{(0.004 + 0.004) \text{ m}^3 + (0.016 \text{ m}^2)(0.04582 \text{ m})}{(2.6738 + 8.4338) \times 10^{-3} \text{ kg}}$

$v_{e2} = 0.78623 \text{ m}^3/\text{kg} > v_g @ 300 \text{ kPa} = 0.60582 \text{ m}^3/\text{kg}$

Ⓔ vapeur surchauffée

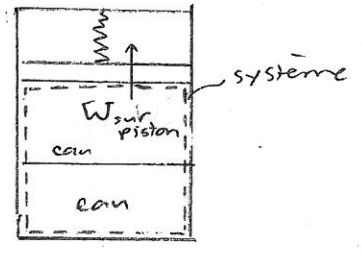
Table A-6 : pour $P_{e2} = 0.3 \text{ MPa}$ et $v_{e2} = 0.78623 \text{ m}^3/\text{kg}$
 interpolation donne

$$T_{e2} = 200 + \frac{(250-200)}{(0.79645-0.71643)} (0.78623-0.71643)$$

$$T_{e2} = 243.61 \text{ }^\circ\text{C}$$

(similairement : $u_{e2} = 2718.95 \text{ kJ/kg}$)

c) $W_{\text{sur piston}} = ? ;$



1ère loi : $\Delta E_{\text{sys } 12} = E_{\text{in } 12} - E_{\text{out } 12}$

$$\Delta U_{\text{eau}} + \cancel{\Delta U_{\text{membrane}}} + \cancel{\Delta E_{\text{eau membrane}}} = 0$$

$$+ \cancel{\Delta E_{\text{eau membrane}}} = -W_{\text{sur piston}}$$

$$(m_{b1} + m_{c1}) u_{e2} - (m_{b1} u_{b1} + m_{c1} u_{c1}) = -W_{\text{sur piston}}$$

$$W_{\text{sur piston}} = m_{b1} (u_{b1} - u_{e2}) + m_{c1} (u_{c1} - u_{e2})$$

$$\Rightarrow u_{b1} = 2261.28 \text{ kJ/kg} \quad (\text{voir partie a})$$

$$\Rightarrow u_{c1} = 2881.6 \text{ kJ/kg} \quad (\text{voir partie a})$$

$$\Rightarrow u_{e2} = 2718.95 \text{ kJ/kg} \quad (\text{voir partie b})$$

$$\Rightarrow m_{b1} = 2.6738 \times 10^{-3} \text{ kg}$$

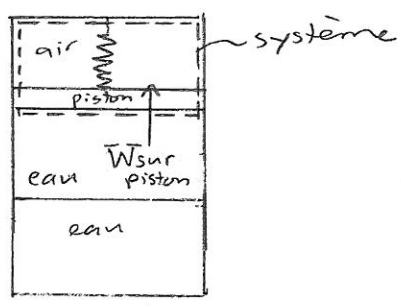
$$\Rightarrow m_{c1} = 8.4338 \times 10^{-3} \text{ kg}$$

$$W_{\text{sur piston}} = (2.6738 \times 10^{-3} \text{ kg})(2261.28 - 2718.95) \frac{\text{kJ}}{\text{kg}} + (8.4338 \times 10^{-3} \text{ kg})(2881.6 - 2718.95) \frac{\text{kJ}}{\text{kg}}$$

$$W_{\text{sur piston}} = 0.14804 \text{ kJ}$$

Note: $W_{\text{sur piston}}$ ne peut pas être calculé par $\int P dV$ car on ne connaît pas comment P à la surface inférieure du piston varie avec le volume (déplacement du piston) surtout que le processus ① → ② n'est pas nécessairement quasi-statique dans ce cas-ci.

d) i) $m_a = ?$ (par la 1^{ère} loi)



1^{ère} loi:

$$\Delta E_{sys} = E_{in} - E_{out}$$

$$\Delta U_{air} + \cancel{\Delta E_{ressort\ piston}} + \cancel{\Delta E_{c\ air\ ressort\ piston}} + \cancel{\Delta E_p\ air} + \cancel{\Delta E_p\ ressort} + \Delta E_p\ piston = W_{sur\ piston}$$

$$m_a(u_{a2} - u_{a1}) + \left(\frac{k}{2}z_2^2 - \frac{k}{2}z_1^2\right) + m_p g \Delta z = W_{sur\ piston}$$

$$m_a(u_{a2} - u_{a1}) = W_{sur\ piston} - \frac{k}{2}(z_2^2 - z_1^2) - m_p g \Delta z$$

$$m_a = \frac{W_{sur\ piston} - \frac{k}{2}(z_2^2 - z_1^2) - m_p g \Delta z}{u_{a2} - u_{a1}}$$

$$\Rightarrow W_{sur\ piston} = 0.14804 \text{ kJ}$$

$$\Rightarrow u_{a1} = u(T_{a1} = 25^\circ\text{C} = 298\text{K}) \stackrel{A-17}{=} 212.64 \frac{\text{kJ}}{\text{kg}}$$

$$\Rightarrow u_{a2} = u(T_{a2} = 52^\circ\text{C} = 325\text{K}) \stackrel{A-17}{=} 232.02 \frac{\text{kJ}}{\text{kg}}$$

$$m_a = \frac{0.14804 \text{ kJ} - \frac{1}{2}(64 \frac{\text{kN}}{\text{m}})(0.05582^2 - 0.01^2) \text{ m}^2 \times \frac{1 \text{ kJ}}{\text{kNm}} - (16.3099 \text{ kg})(9.81 \frac{\text{m}}{\text{s}^2})(0.04582 \text{ m}) \times \frac{1 \text{ kJ}}{10^3 \frac{\text{kg} \cdot \text{m}^2}{\text{s}^2}}}{(232.02 - 212.64) \text{ kJ/kg}}$$

$$m_a = 2.2807 \times 10^{-3} \text{ kg}$$

ii) $\bar{V}_{a1} = ?$: $P_{a1} \bar{V}_{a1} = m_a R T_{a1}$

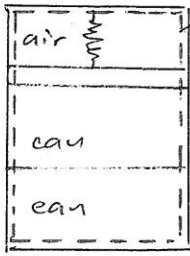
$$\bar{V}_{a1} = \frac{m_a R T_{a1}}{P_{a1}} = \frac{(2.2807 \times 10^{-3} \text{ kg})(0.287 \frac{\text{kPa} \cdot \text{m}^3}{\text{kg} \cdot \text{K}})(25+273)\text{K}}{(50 \text{ kPa})}$$

$$\bar{V}_{a1} = 0.0039 \text{ m}^3$$

Partie d) Solutions alternative

Solution I (acceptable)

i)



1^{ère} loi : $\Delta E_{\text{sys}} = E_{\text{in}} - E_{\text{out}}$

$$\Delta \bar{U}_{\text{air}} + \Delta \bar{U}_{\text{eau}} + \Delta \bar{U}_{\text{piston}} + \Delta E_{\text{c}} + \Delta E_{\text{p}} + \Delta E_{\text{p}} = 0$$

$\begin{matrix} \rightarrow 0 \\ \text{ressort} \\ \text{membrane} \end{matrix}$
 $\begin{matrix} \rightarrow 0 \\ \text{sys} \end{matrix}$
 $\begin{matrix} \rightarrow 0 \\ \text{air} \\ \text{eau} \\ \text{membrane} \end{matrix}$

$$+ \Delta E_{\text{p}}_{\text{ressort}} + \Delta E_{\text{p}}_{\text{piston}} = 0$$

$$m_a (u_{a2} - u_{a1}) + \left[(m_{b1} + m_{c1}) u_{e2} - (m_{b1} u_{b1} + m_{c1} u_{c1}) \right] + \frac{k}{Z} (z_2^2 - z_1^2) + m_p g \Delta z = 0$$

$= W_{\text{sur piston}}$

$$m_a = \frac{\left[m_{b1} (u_{b1} - u_{e2}) + m_{c1} (u_{c1} - u_{e2}) \right] - \frac{k}{Z} (z_2^2 - z_1^2) - m_p g \Delta z}{u_{a2} - u_{a1}}$$

(même réponse que sur page 4)

ii) $V_{a1} = m_a R T_{a1} / P_{a1}$ (même que page 4)

Solution II (non acceptable car 1^{ère} loi pas utilisée tel que demandé)

(max: 1,75 pts)

i) $\frac{P_{a1} V_{a1}}{T_{a1}} = m_a R = \frac{P_{a2} V_{a2}}{T_{a2}} \Rightarrow V_{a2} = V_{a1} - A_p \Delta z$

$$\frac{P_{a1} V_{a1}}{T_{a1}} = \frac{P_{a2} (V_{a1} - A_p \Delta z)}{T_{a2}}$$

Isoler V_{a1} donne :

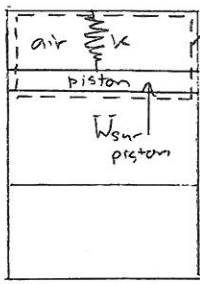
$$V_{a1} = \frac{A_p \Delta z}{1 - \frac{P_{a1} T_{a2}}{P_{a2} T_{a1}}} = \frac{(0,016 \text{ m})(0,04582 \text{ m}^2)}{1 - \left(\frac{50 \text{ kPa}}{66,72 \text{ kPa}} \right) \left(\frac{52+273}{25+273} \right) \frac{\text{K}}{\text{K}}}$$

$$V_{a1} = 0,0040 \text{ m}^3$$

i) $m_a = \frac{P_{a1} V_{a1}}{R T_{a1}} = \frac{(50 \text{ kPa})(0,0040 \text{ m}^3)}{(0,287 \frac{\text{kPa} \cdot \text{m}^3}{\text{kg} \cdot \text{K}})(25+273) \text{ K}} = 2,3459 \times 10^{-3} \text{ kg}$

(Note: petites différences dans valeurs de V_{a1} & m_a versus p.4, causées par les interpolations et arrondissement de la méthode utilisant la 1^{ère} loi,

Partie c) Solution alternative



1ère loi : $\Delta E_{\text{sys}} = E_{12}^{\text{in}} - E_{12}^{\text{out}}$

$$\Delta \bar{U}_{\text{air}} + \cancel{\Delta \bar{U}_{\text{piston}} + \Delta \bar{U}_{\text{ressort}}} + \cancel{\Delta E_c} + \cancel{\Delta E_p} + \Delta E_p + \Delta E_p$$

$$+ \Delta E_p = + W_{\text{sur piston}}$$

$$m_a(u_{a2} - u_{a1}) + \frac{k}{2}(z_2^2 - z_1^2) + m_p g \Delta z = \bar{W}_{\text{sur piston}}$$

$$\bar{W}_{\text{sur piston}} = m_a(u_{a2} - u_{a1}) + \frac{k}{2}(z_2^2 - z_1^2) + m_p g \Delta z$$

$$\Rightarrow m_a = \frac{P_{a1} V_{a1}}{R T_{a1}} \rightarrow V_{a1} = \frac{A_p L z}{1 - \frac{P_{a1} T_{a2}}{P_{a2} T_{a1}}}$$

$$V_{a1} = 0.0040 \text{ m}^3$$

$$m_a = 2.3459 \times 10^{-3} \text{ kg}$$

$$\Rightarrow u_{a1} = u(T_{a1} = 298 \text{ K}) = 212.64 \text{ kJ/kg}$$

$$\Rightarrow u_{a2} = u(T_{a2} = 325 \text{ K}) = 232.02 \text{ kJ/kg}$$

$$\bar{W}_{\text{sur piston}} = (2.3459 \times 10^{-3} \text{ m}^3)(232.02 - 212.64) \frac{\text{kJ}}{\text{kg}} + \frac{(64 \frac{\text{kJ}}{\text{m}})}{2} (0.05582^2 - 0.01^2) \text{ m}^2$$

$$+ (16.3099 \text{ kg})(9.81 \frac{\text{m}}{\text{s}^2})(0.04582 \text{ m}) \times 1 \text{ kJ} / 10^3 \text{ kg} \cdot \frac{\text{m}^2}{\text{s}^2}$$

$$\bar{W}_{\text{sur piston}} = 0.14930 \text{ kJ}$$

} voir bas
de la page
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