



PHS 6317 Nanoengineering of thin films

Course schedule – Winter 2024

12 January	Introduction – Scientific and technological challenges
19	Fabrication methods – Vacuum physics and vapor-phase techniques
26*	Fabrication methods – Plasma processes and process optimization
2 February	Fabrication methods - Plasma-surface interactions and diagnostics
9**	Fabrication methods – Thermal/Plasma spray technologies
16*	Optics of thin films 1, optical characterization, <i>Miniquiz1 (5%)</i>
23*	Optics of thin films 2, design of optical filters
1*** March	<i>Presentations – Emerging fabrication techniques (30%)</i>
March 4-8 - Winter/Spring break	
15**	Tribo-mechanical properties of films and coatings
22**	Electrochemical properties – corrosion and tribo-corrosion(<i>filter-20%</i>)
5 April	Functional films and coatings – Part 1 , <i>Miniquiz 2 (5%)</i>
12	Functional films and coatings – Part 2
16	Life cycle analysis and environmental impact, visits
18***	<i>Presentations – Emerging applications of nanostructured films (40%)</i>

Deadlines:

Project #1 – Fabrication technique:

Choice of the subject: **26 January**

Abstract and references: **9 February**

Report and presentation: **1st March**

Projet #2 – Design of an optical filter:

Choice of the subject: **23 February**

Report: **22 March**

Projet #3 – Application of nanostructured thin films:

Choice of the subject: **16 February**

Abstract and references: **15 March**

Presentation: **18 April p.m.**

Report: **22 April at 23:59**

Project #3: Applications of nanostructured films and coatings

Thomas Sicotte and Alexandre Gamache - Cellules photovoltaïques à pérovskite

Alexandre Lussier - Fenêtres intelligentes thermochromiques

Mohamed Ammari - Thermal barrier coatings for aerospace gas turbine engine

Luc Montpetit - Passivation of CdZnTe for x-ray detectors

Veronika Cervenkova - Solar-thermal energy conversion - Transition metal nitrides

Émilien Martel - Electrochromic, photochromic and gasochromic coatings for consumer optics

Étienne Tremblay et Nathan Sasseville - Couches minces pour l'électronique organique – OLEDs

Thomas Lapointe - Photodétecteurs et leur conception/optimisation à l'aide des couches minces

Alexandre Carrière et Youssef Ben Mami - Électrodes transparentes pour la fabrication des cellules solaires

Arghavan Yazdanpanah Ardakani - Nanoengineering thin-films to produce hydrophobic coatings for aircraft surfaces

Mathieu Bruzzese – Oxidation-resistance barrier coatings for aerospace applications

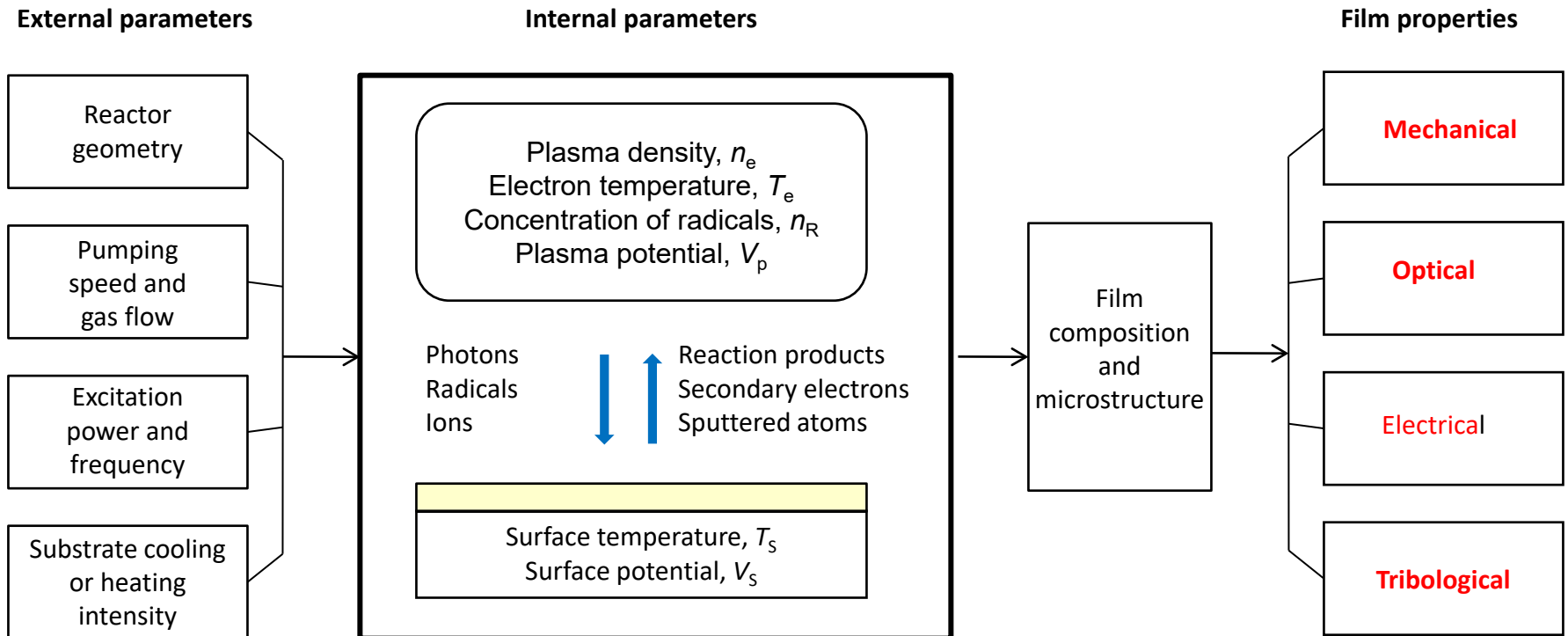
Bastien Izacard – Atomic oxygen barrier coatings for satellites

Alexandre Fall - Carbon nanotubes for sodium-ion batteries

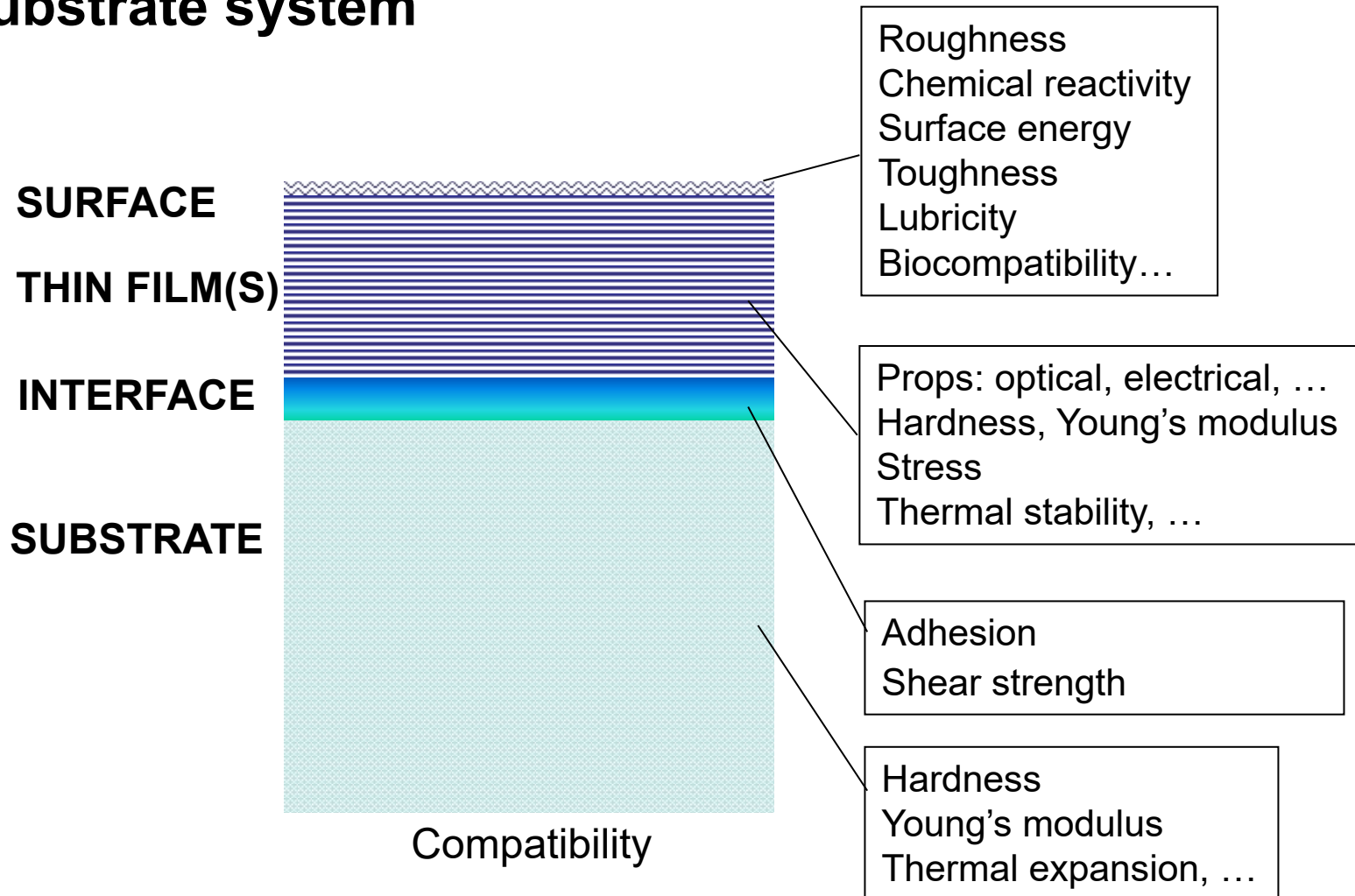
Alexandre Pinel - Couches minces d'hydroxyapatites pour les implants en biomedical

Christelle Abou Zeidan – Carbon nanotubes for flexible electronics

Plasma system and process and materials control

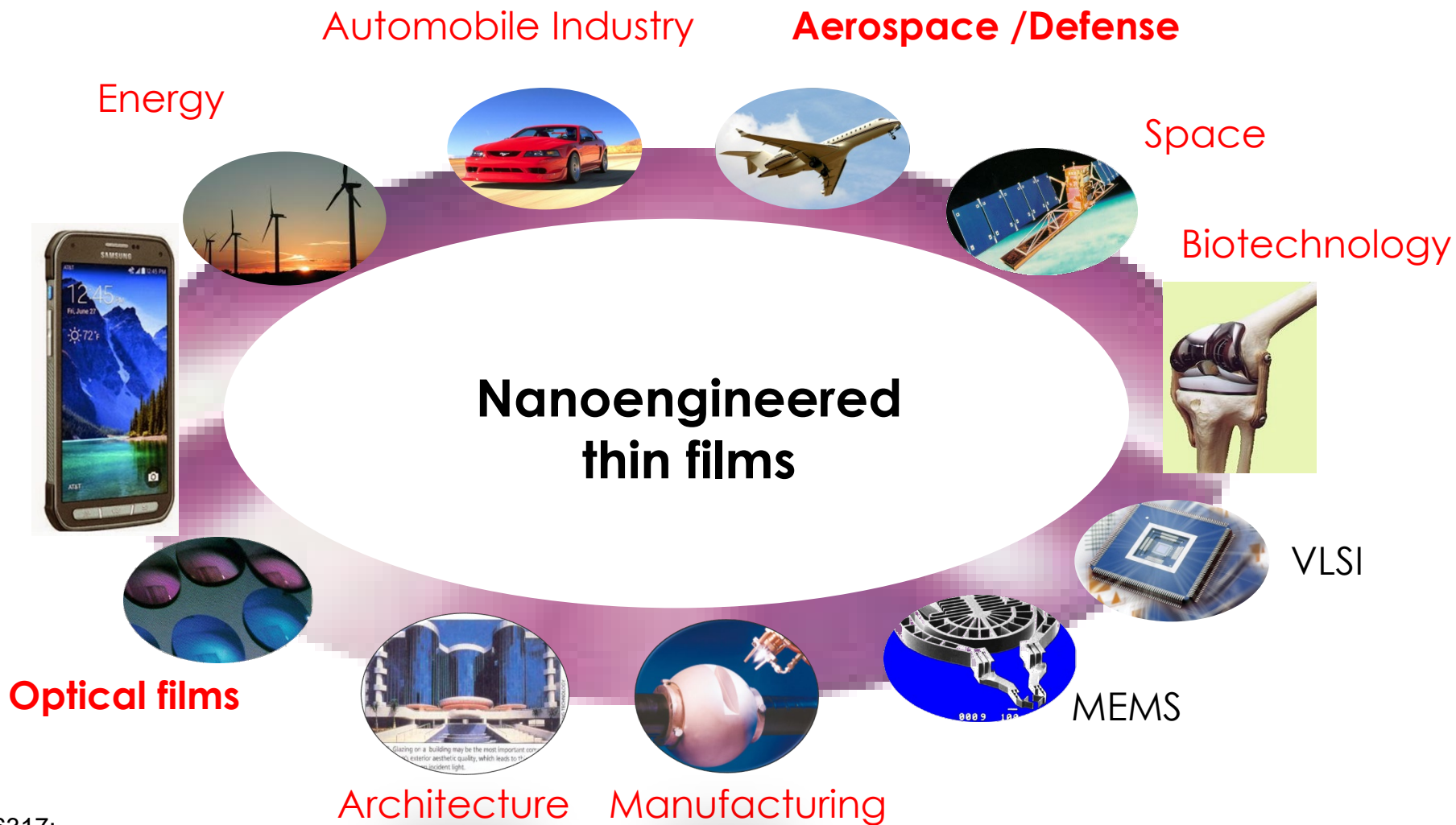


Control of the properties through the microstructure: Film-substrate system



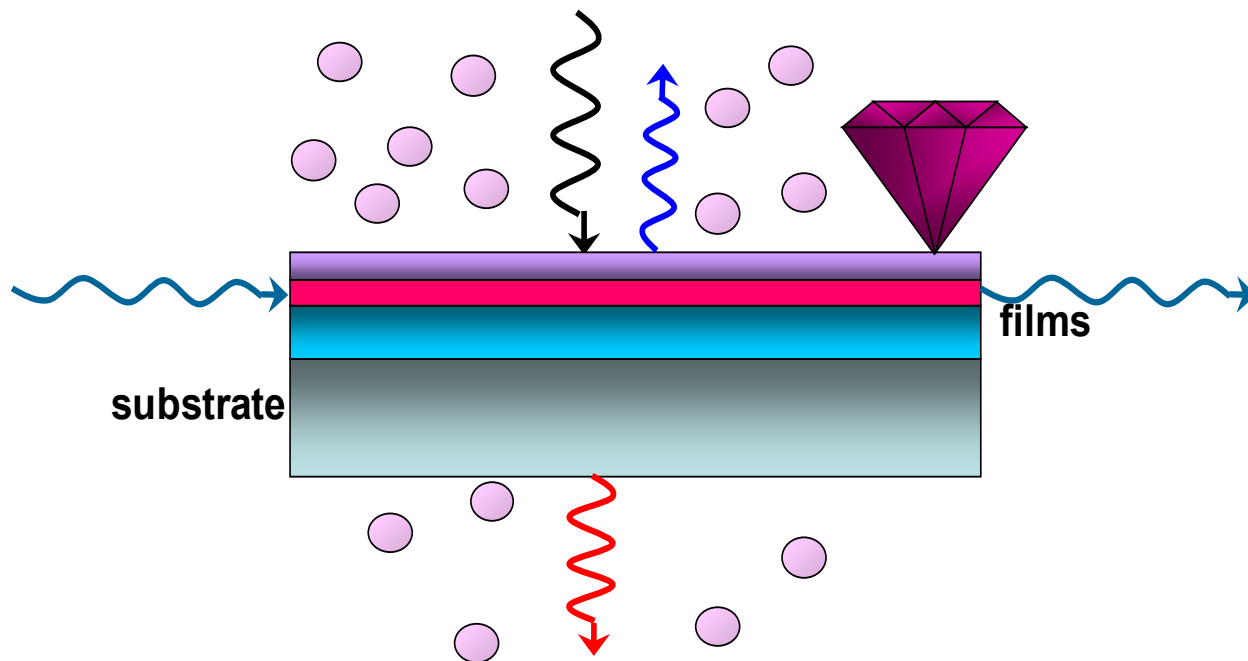


Multisectoral character of advanced materials





Nanostructured functional and multifunctional thin films



The concept of nanostructured functional and multifunctional coatings

-
"We are limited only by our imagination"

Challenges

Main/complementary properties

Compatibility (substrate, process,...)

Process control

Stability

Industrial scale, cost

Deposition technologies

New materials:

- passive functional

- active - smart,

- compounds, nano-materials, nanocomposites

Coating architectures:

- single layers

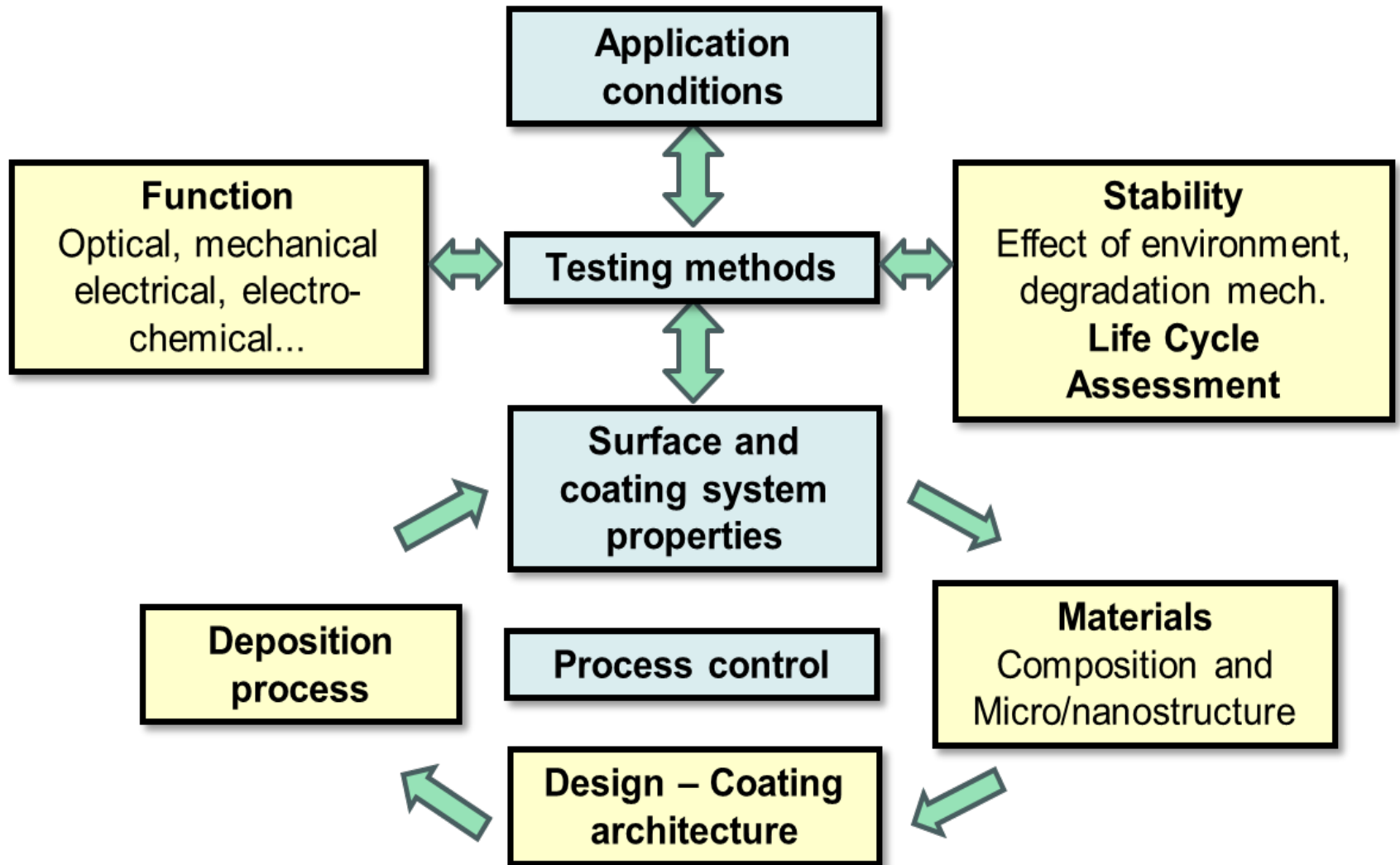
- (discrete) multilayers

- graded layers

- nanostructures

- control of interfaces

The **holistic approach** to surface engineering



Development of passive thin films

Optical coatings:

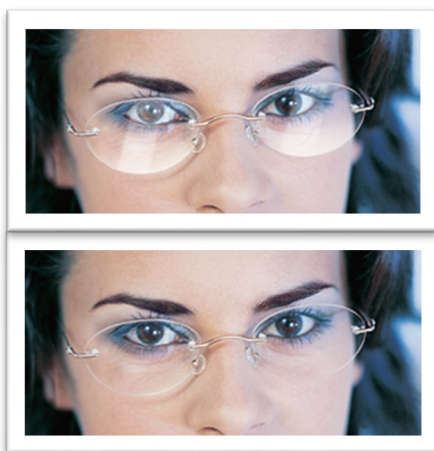
- Choice of the fabrication technique
- New technologies

Gas and vapor diffusion barriers:

- Thin films on plastics



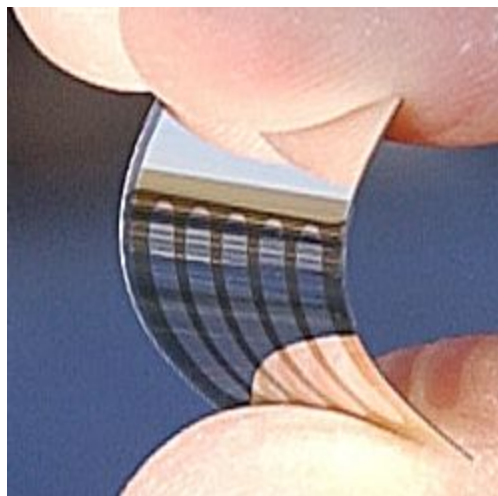
Optical coatings



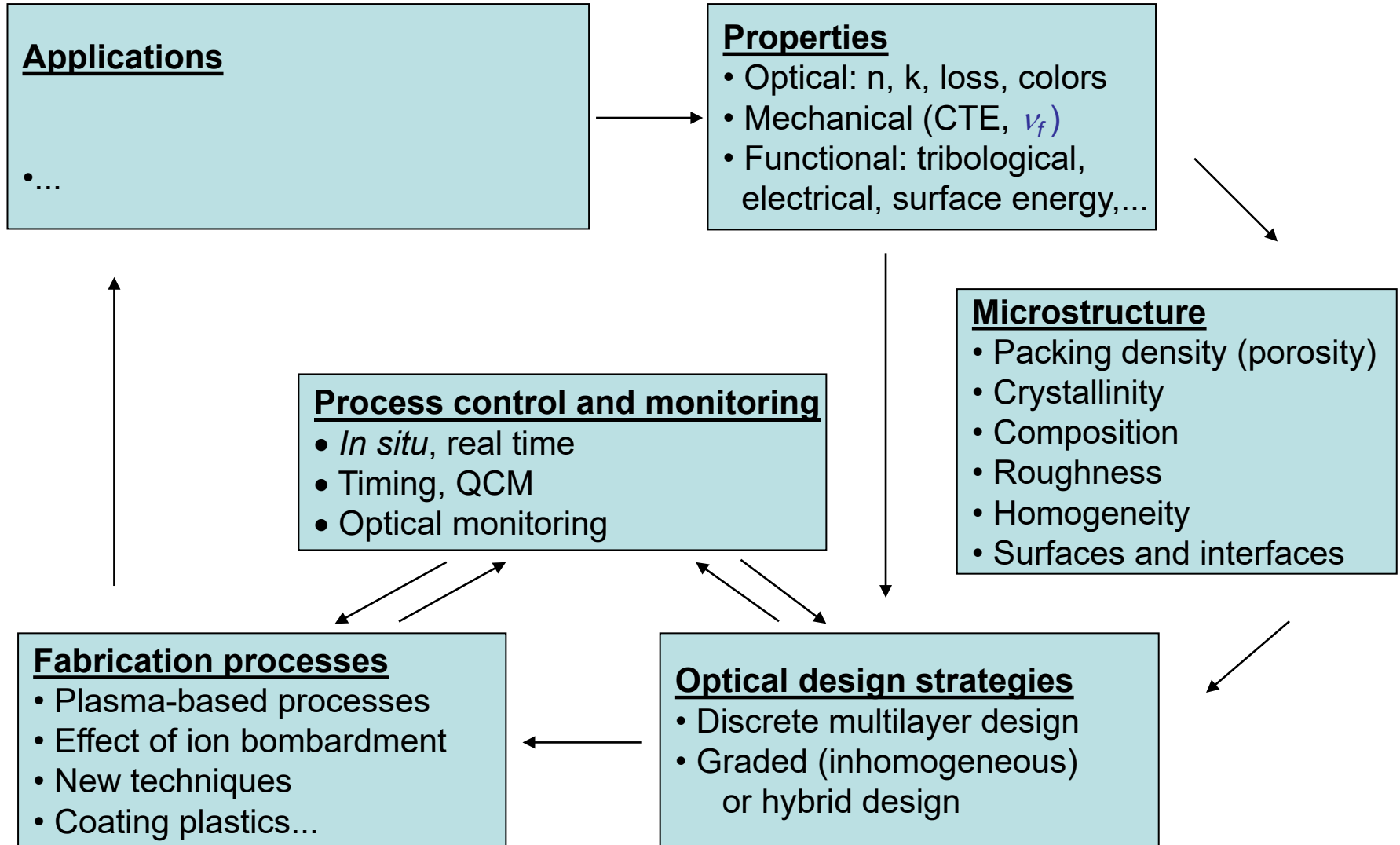
The AR council
(www.arccouncil.org)



Bank of Canada



Optical coatings – from design to manufacture



Requirements for optical films

1. Optical properties – complex refractive index

$$N = n - ik$$

x.xx

filters

x.xxx

waveguides

$\leq 10^{-5}$

transparent

2. Mechanical and tribological properties
3. Environmental stability (T , RH, ...)
4. Functional properties (hydrophobicity/hydrophilicity, electrical conductivity, gas/vapor permeation barriers ...)
5. Active properties (electrochromic, thermochromic, photochromic and other properties)



Refractive index of optical coatings

L. Martinu and D. Poitras
J. Vac. Sci. Technol. A 18,
2619-2645 (2000)

L. Martinu et al., Chapter 9 in the “Handbook
of Film Deposition Technologies”,
P.M. Martin, ed., Elsevier 2010

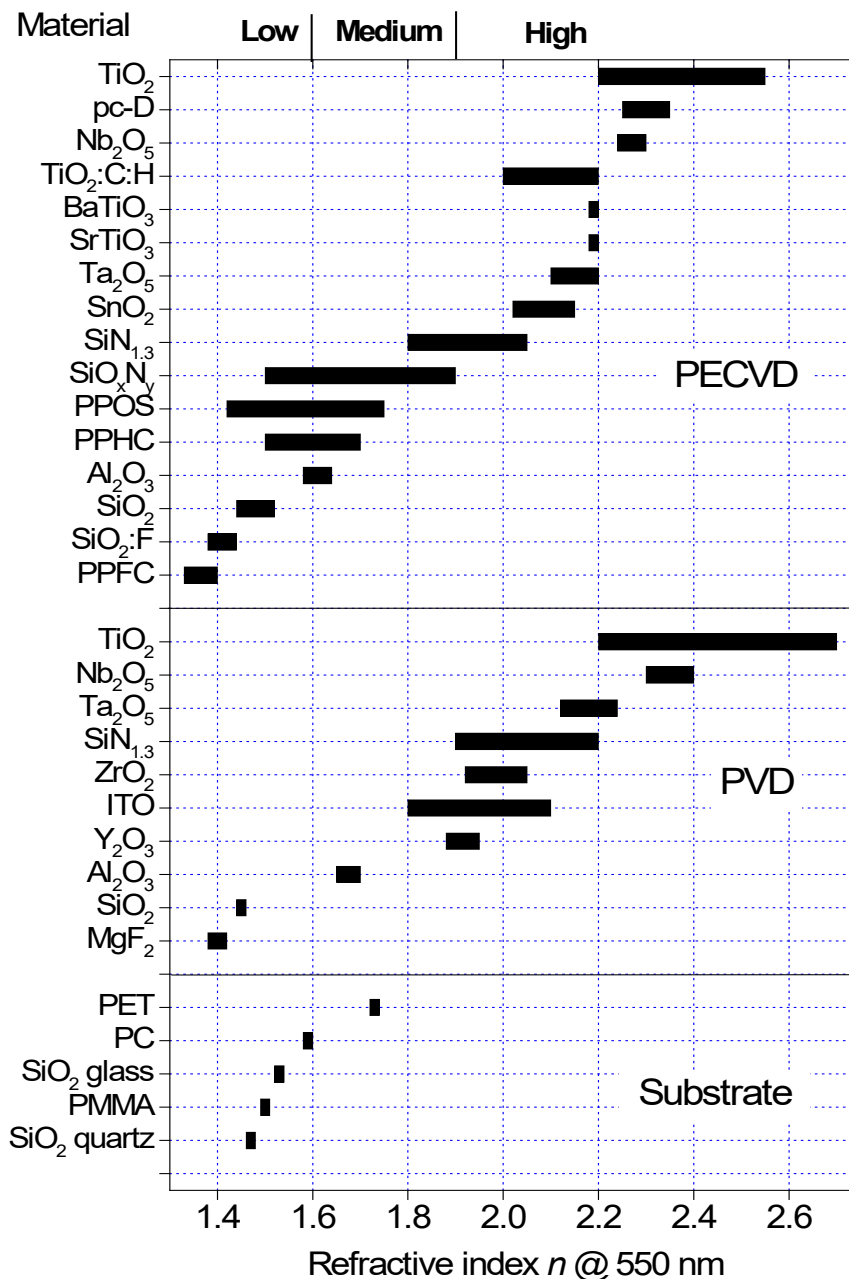
Requirements:

Choice of n_H and n_L

Compatibility with substrates

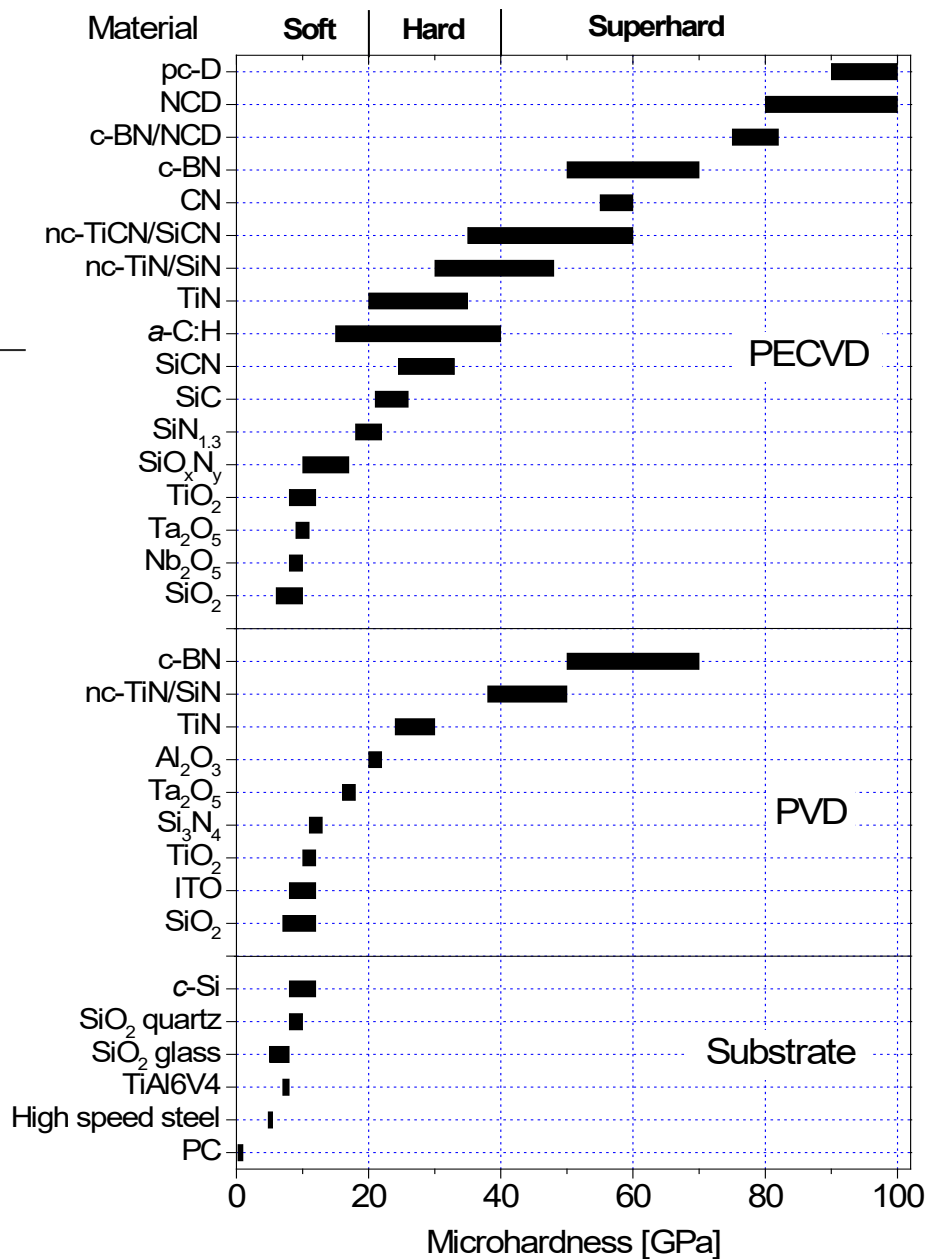
Durability and environmental stability

Compatibility with other process technologies





Microhardness of different coatings

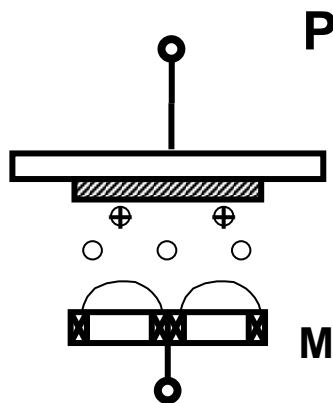


L. Martinu and D. Poitras
J. Vac. Sci. Technol. A, 18 (2000) 2619

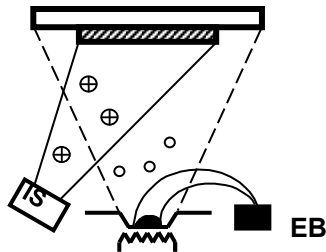
L. Martinu et al., Chapter 8 in "Handbook of Film Deposition Technologies,"
P. Martin, ed., Elsevier 2010

J.E. Klemberg-Sapieha et al.,
Appl. Optics 43 (2004) 2670

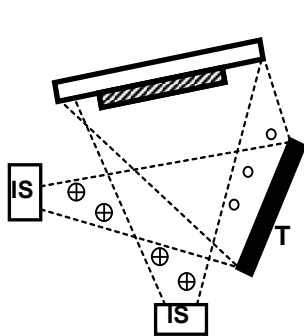
Comparison of different deposition techniques



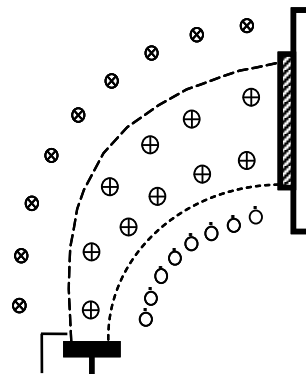
MS: DCMC, PDMS, RFMS, HiPIMS



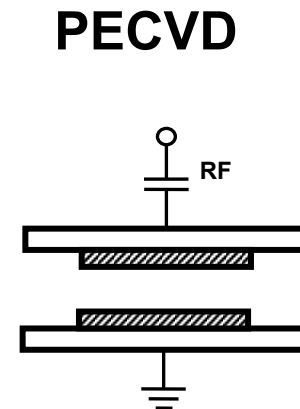
IBAD



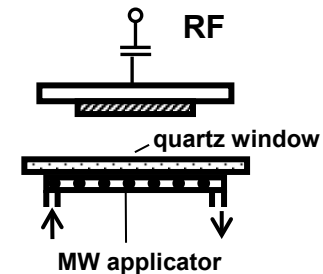
DIBS



FCAD



RF/AC PECVD



Dual mode MW/RF
PECVD

J.E. Klemberg-Sapieha et al., *Appl. Opt.*, 43 (2004) 2670

L. Martinu et al., in 50 Years of Vacuum Coatings, SVC, 2007

L. Martinu et al., in Handbook of Thin Film Deposition Technology, Elsevier, 2010

Deposition techniques and parameters

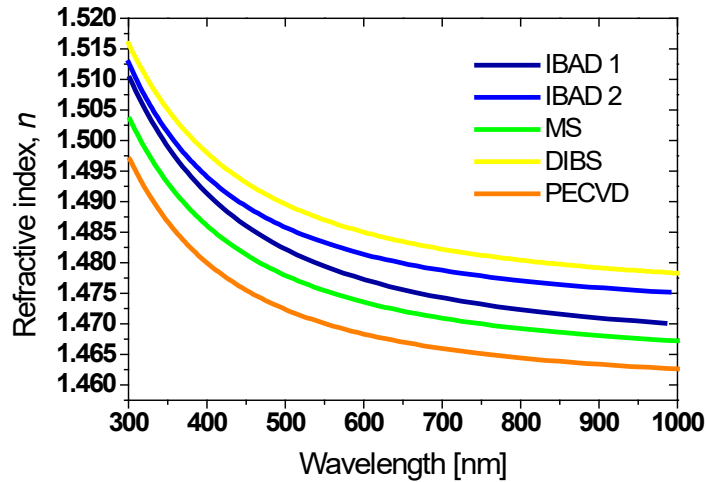
Deposition technique	Coating	Conditions					
		p [Torr]	T_s [°C]	V_B [V]	E_i [eV]	I [$\mu\text{A}/\text{cm}^2$]	r_D [nm/s]
IBAD 1	SiO ₂	6.0×10^{-5}	60	0	200	100	0.15
	TiO ₂	1.1×10^{-4}	100	0	150	185	0.07
IBAD 2	SiO ₂	1.2×10^{-4}	60	0	115	65	0.20
	Ta ₂ O ₅	1.5×10^{-4}	100	0	115	65	0.20
	TiO ₂	1.3×10^{-4}	80	0	105	100	0.35
MS	SiO ₂	3.1×10^{-4}	80	0			0.23
	Ta ₂ O ₅	3.5×10^{-4}	80	0			0.25
	TiO ₂	3.8×10^{-4}	80	0			0.13
DIBS	SiO ₂	2.4×10^{-4}	100	0	300	200	0.37
	Ta ₂ O ₅	2.4×10^{-4}	100	0	300	200	0.53
PECVD	SiO ₂	6.0×10^{-2}	30	600	240	80	2.30
	Ta ₂ O ₅	2.5×10^{-2}	30	600	300	90	0.80
	TiO ₂	2.5×10^{-2}	30	450	225	70	0.60
FCAD	TiO ₂	2.6×10^{-3}	30	120	50	2500	1.70

Thickness $d \sim 1000$ nm

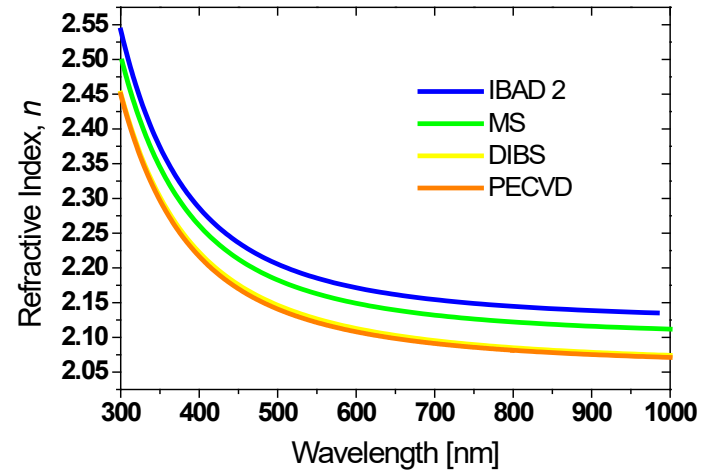
Two types of pre-characterized **substrates**: **c-Si** (50 mm diameter) and **FS** (25 mm diameter)

Refractive index dispersion curves

SiO₂

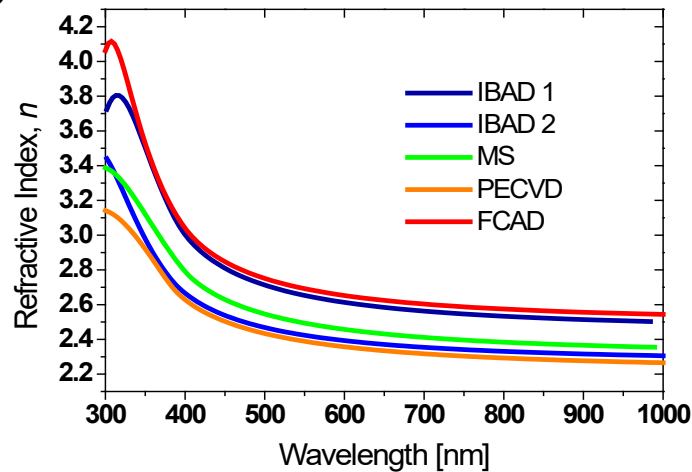


Ta₂O₅



$n_{550} = 1.47 - 1.49$

TiO₂

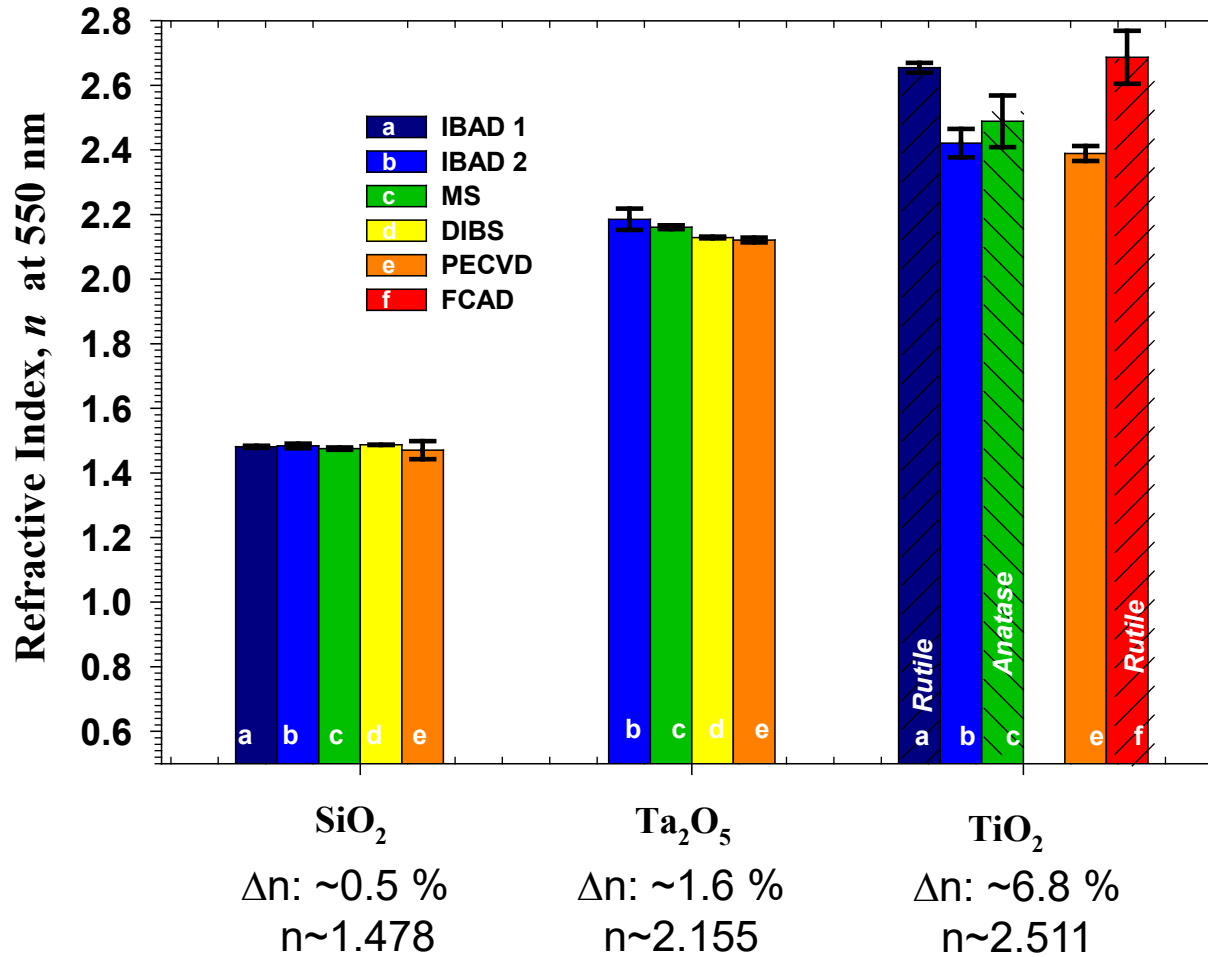


$n_{550} = 2.13 - 2.19$

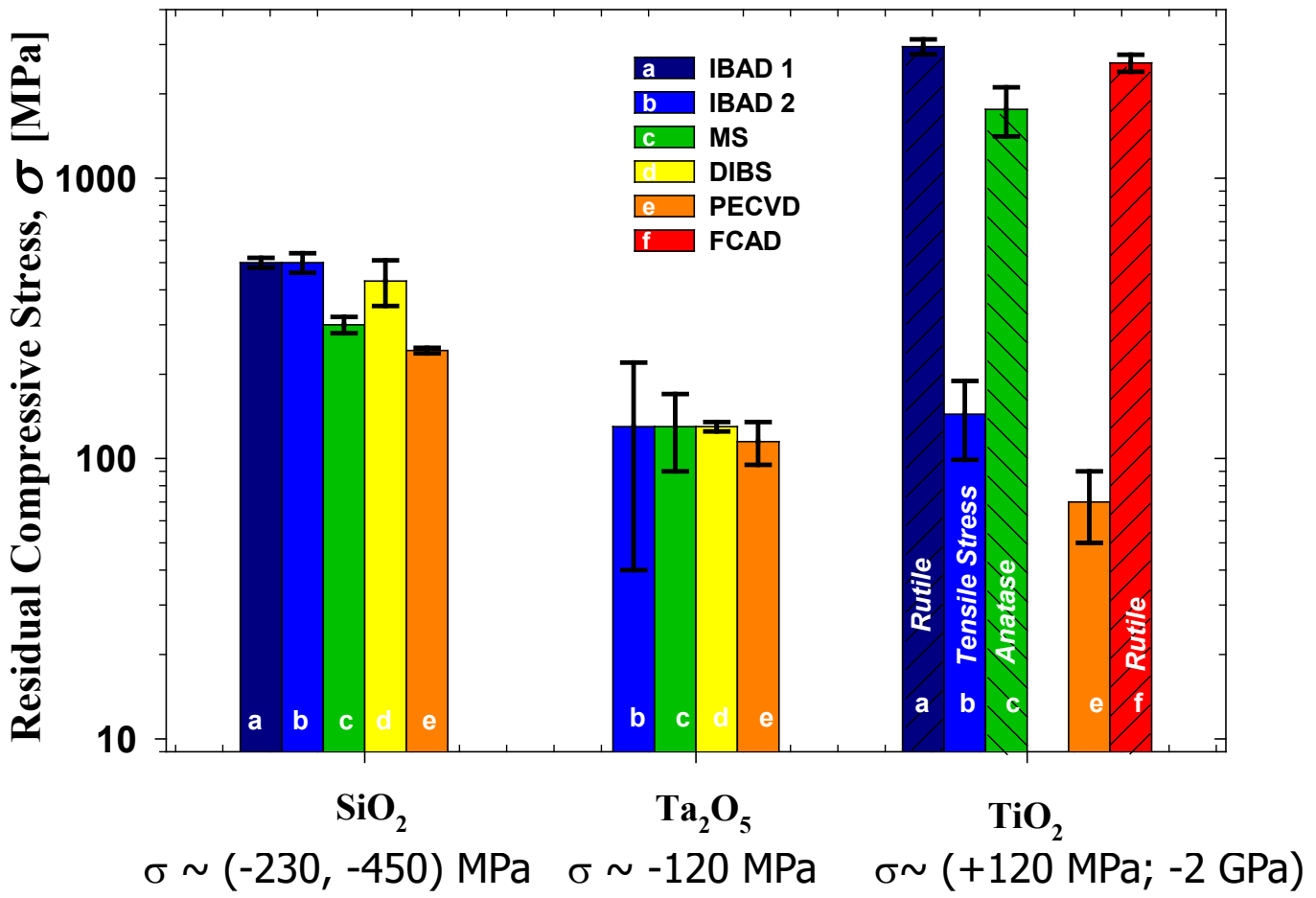
$k < 10^{-5}$

$n_{550} = 2.35 - 2.70$

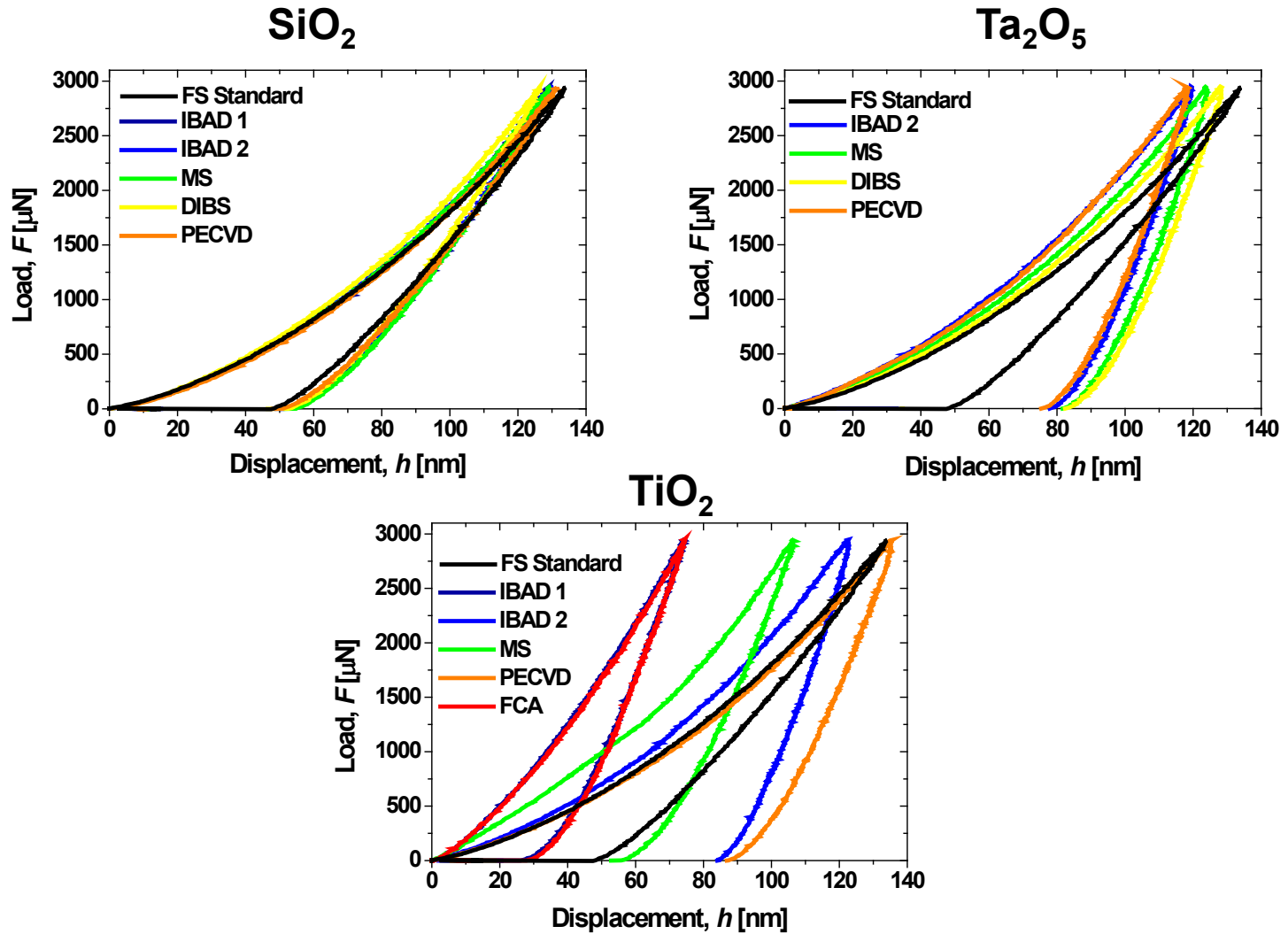
Comparison of n_{550} values



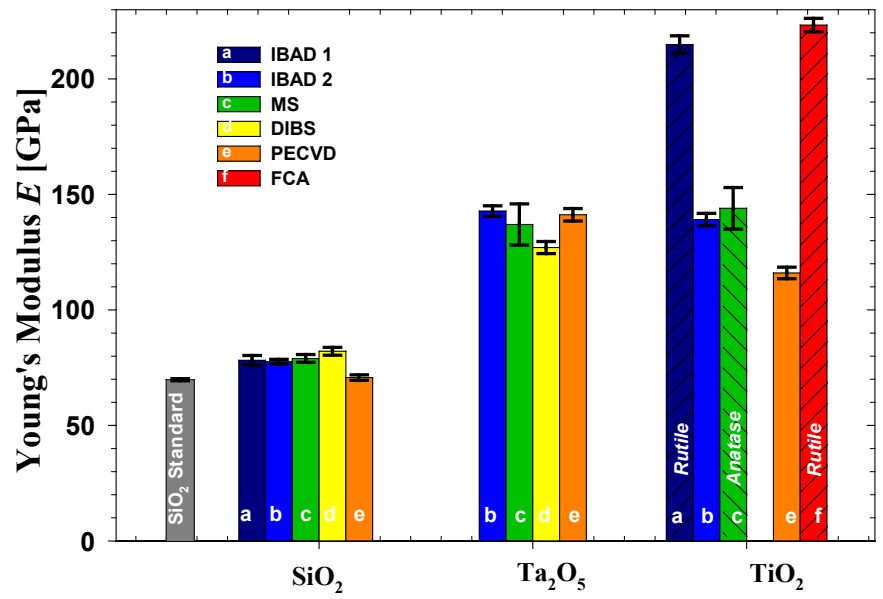
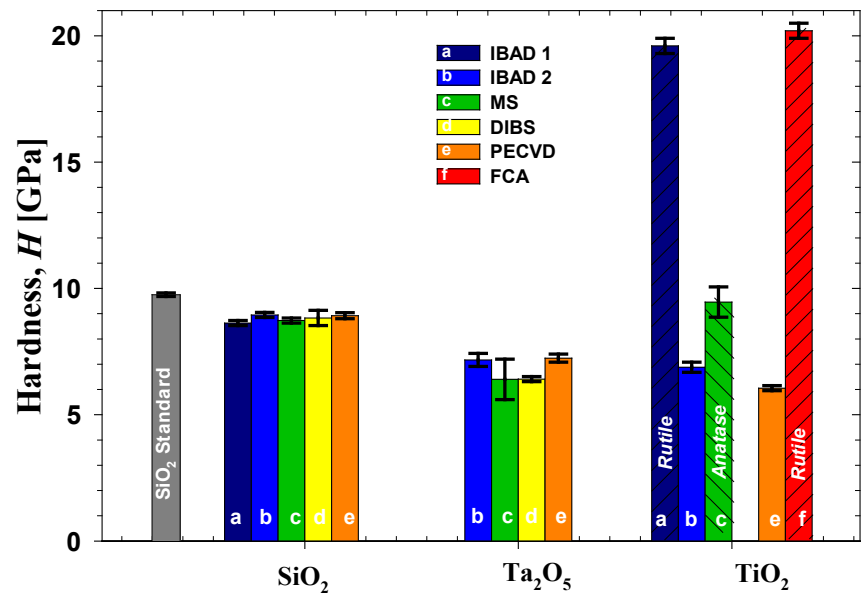
Residual stress



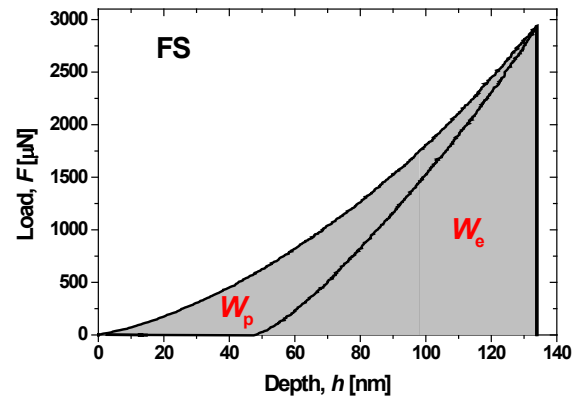
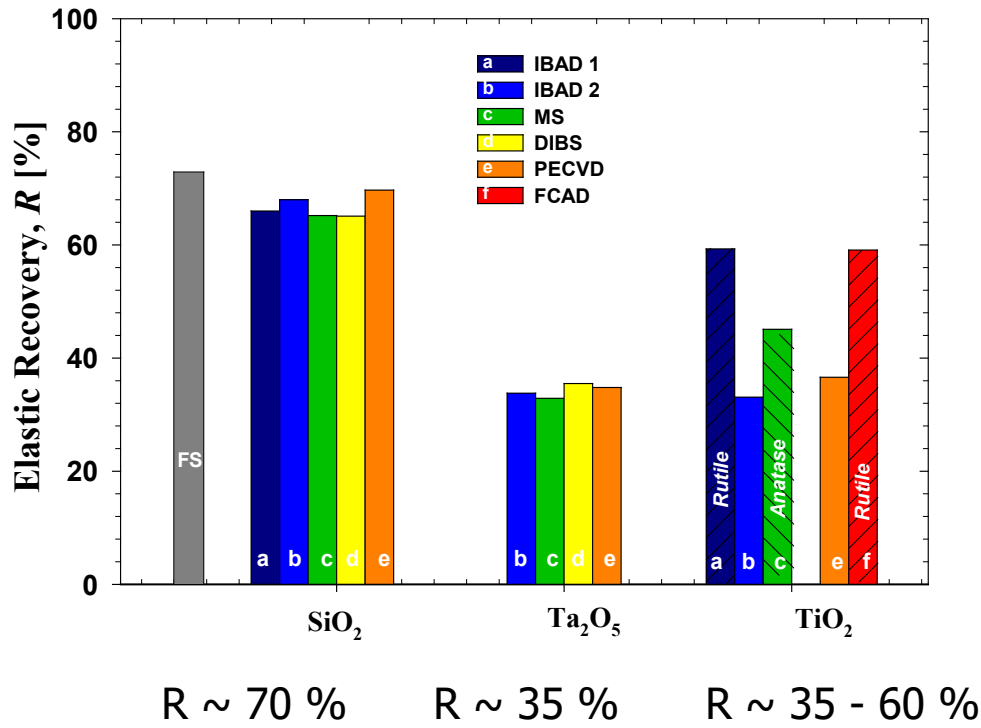
Load-displacement curves



Hardness and Young's modulus

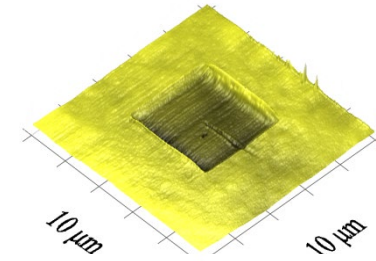
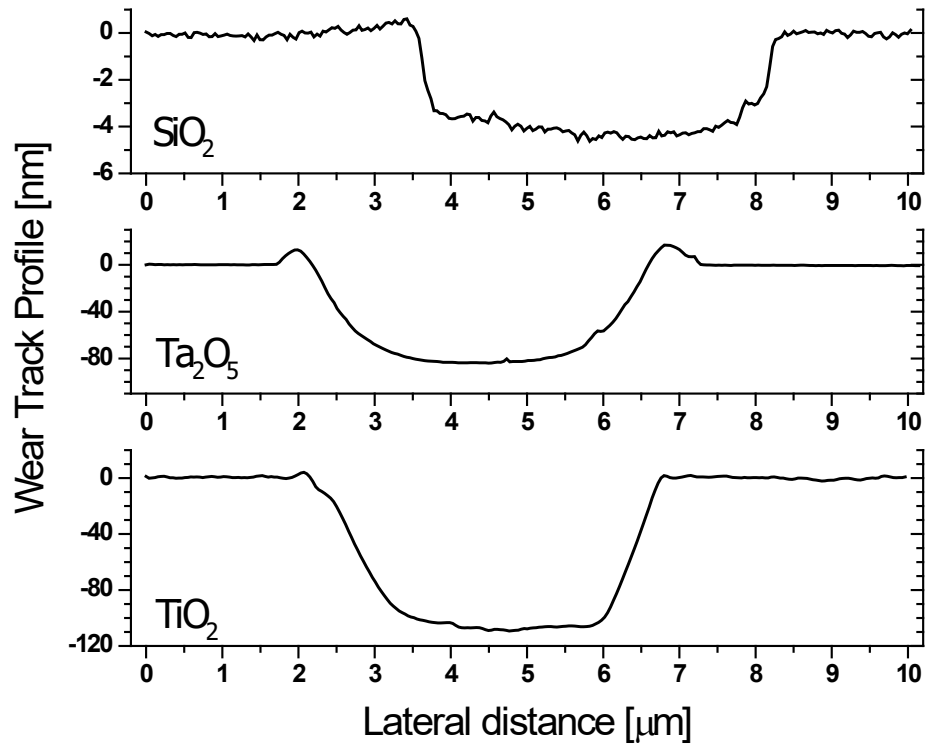


Elastic recovery

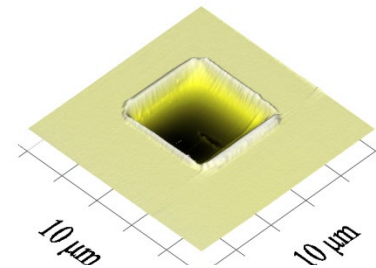


$$R = \frac{W_e}{W_{Tot}}$$

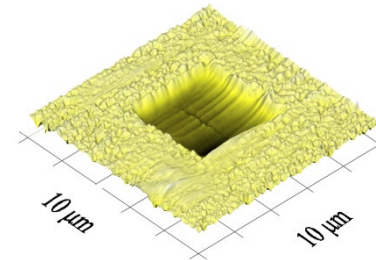
Wear test



IBAD 2



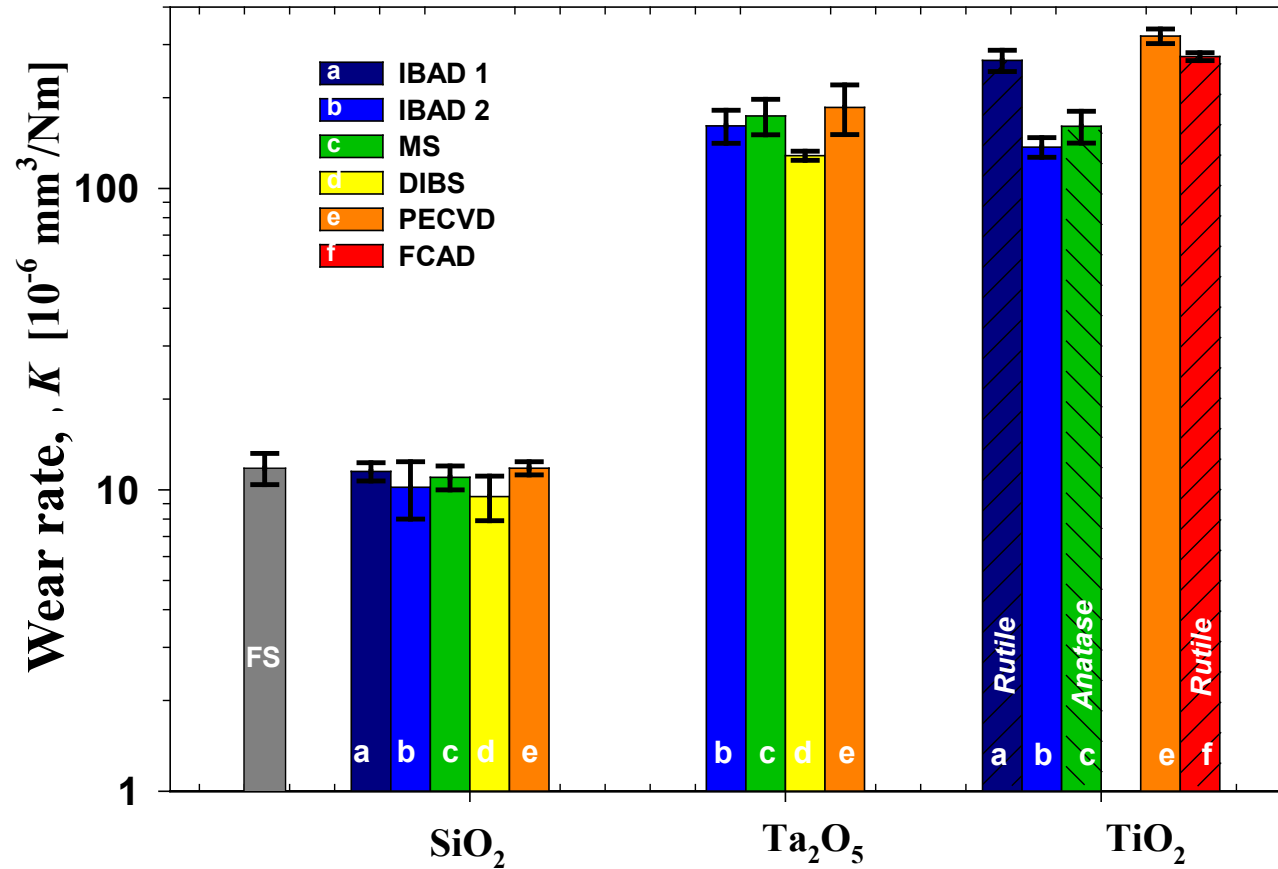
DIBS



FCAD

Reference: $K_{FS} = 10.6 \pm 0.9 [10^{-6} \text{ mm}^3/\text{Nm}]$

Wear rate



Energetic conditions during the film growth

Technique	SiO ₂		Ta ₂ O ₅		TiO ₂	
	E_i [eV]	Φ_i / Φ_N	E_i [eV]	Φ_i / Φ_N	E_i [eV]	Φ_i / Φ_N
IBAD-1	200	1.8	-	-	150	5.2
IBAD-2	100	0.9	100	1.7	100	0.6
MS	10 ?	1 ?	10 ?	1 ?	10 ?	1 ?
DIBS	300	1.5	300	2.1	-	-
PECVD	240	0.1	300	0.6	225	0.2
FCAD	-	-	-	-	50	2.9

Energy per deposited particle: $E_p \sim E_i \frac{\Phi_i}{\Phi_N}$ $\Phi_N = r_D \frac{\rho N_A}{m_A}$

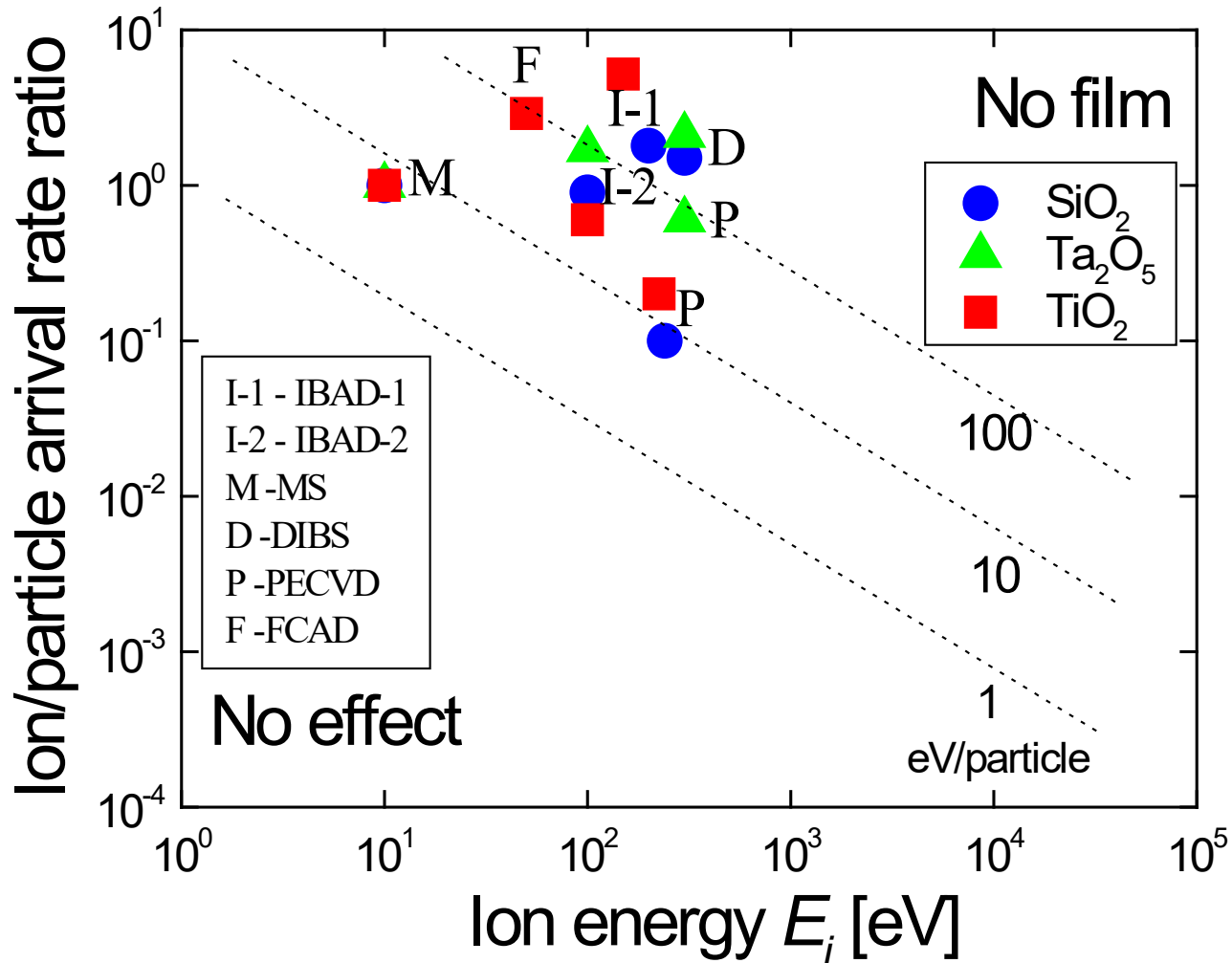
Φ_i – flux of ions

Φ_N – flux of condensed particles

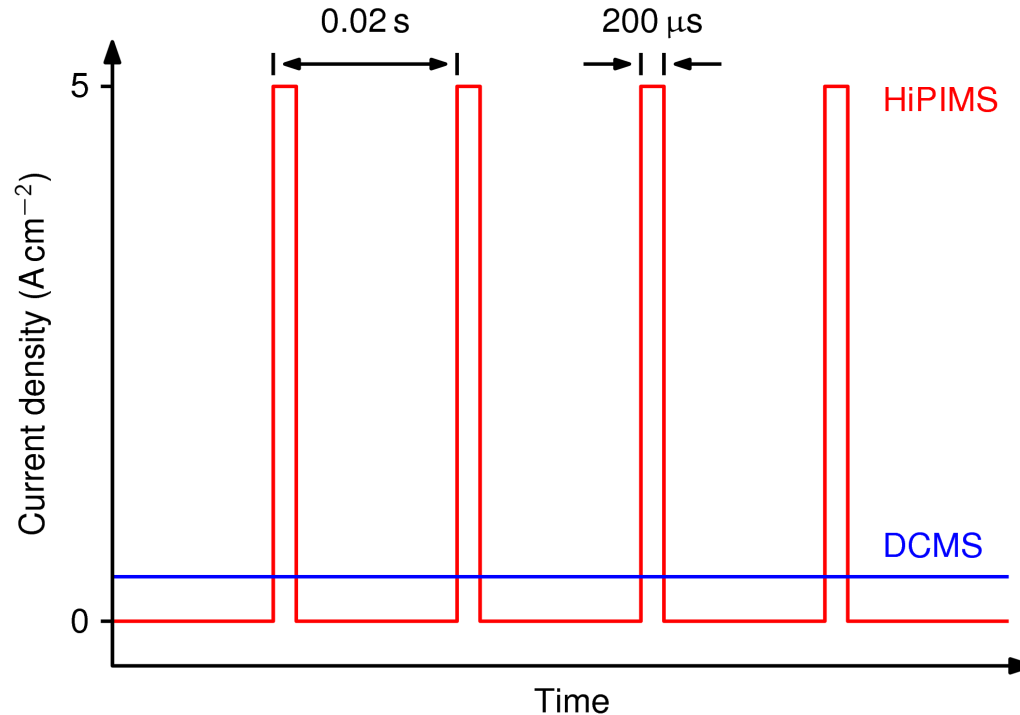
ρ – density

m_A – molecular weight

Energetic conditions during the film growth



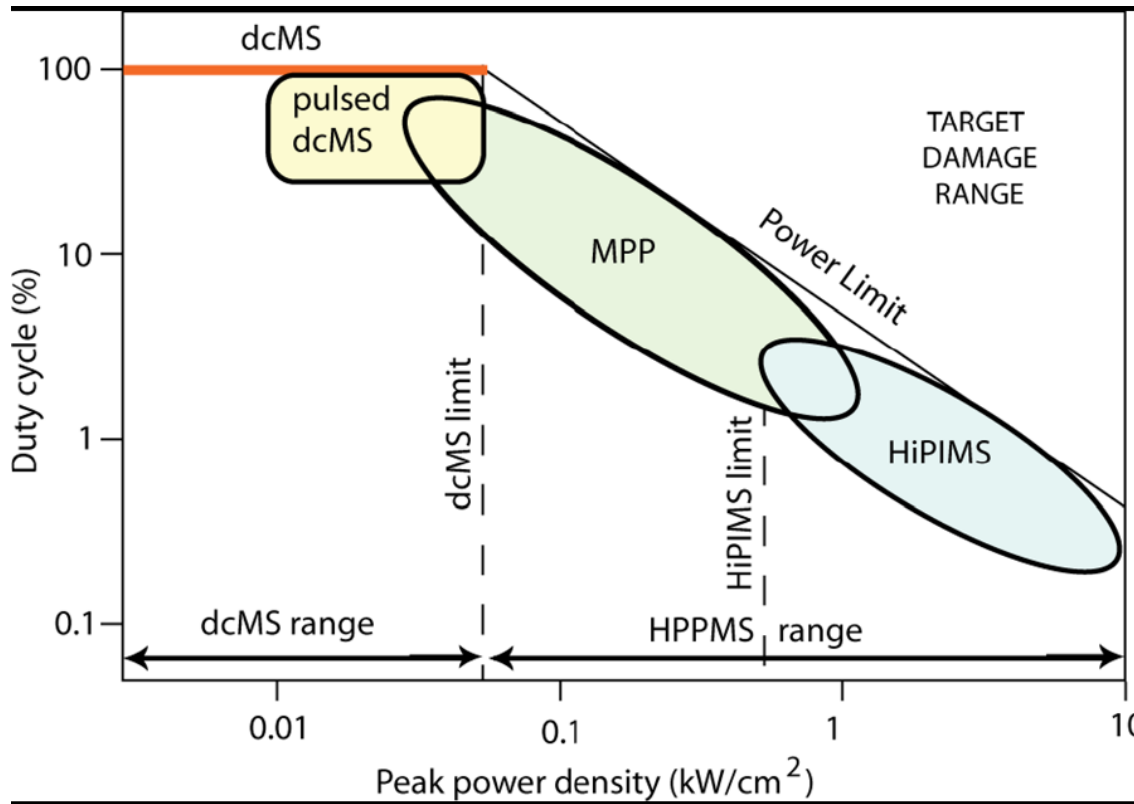
High Power Impulse Magnetron Sputtering - HiPIMS



New coating properties due to:

- high density plasmas – films obtained from ionized species
- high ion fluxes toward the substrate
- effect of ion bombardment on the microstructural evolution

Pulsed discharges

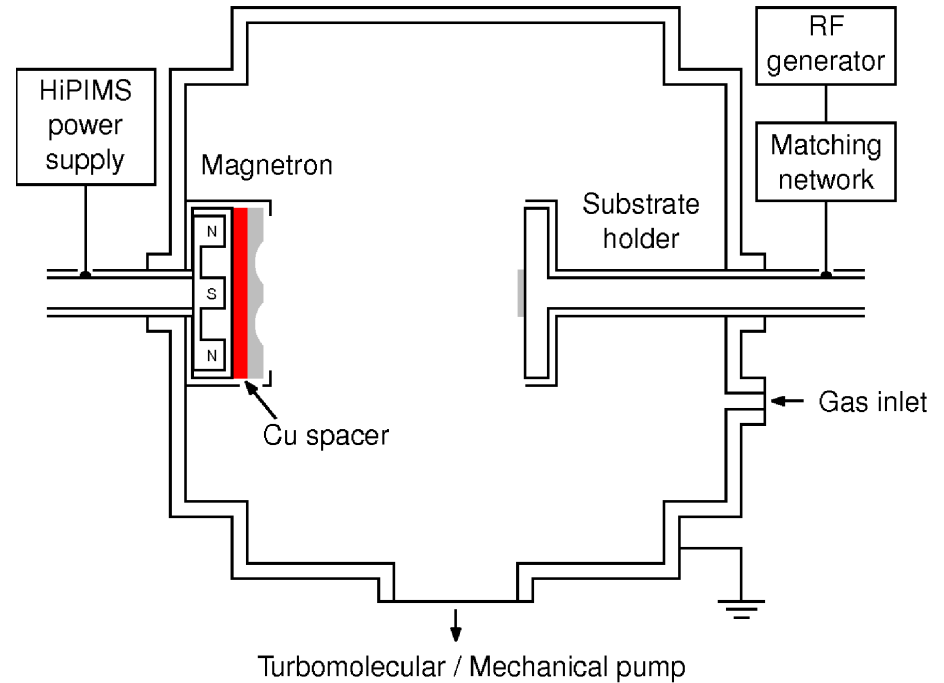
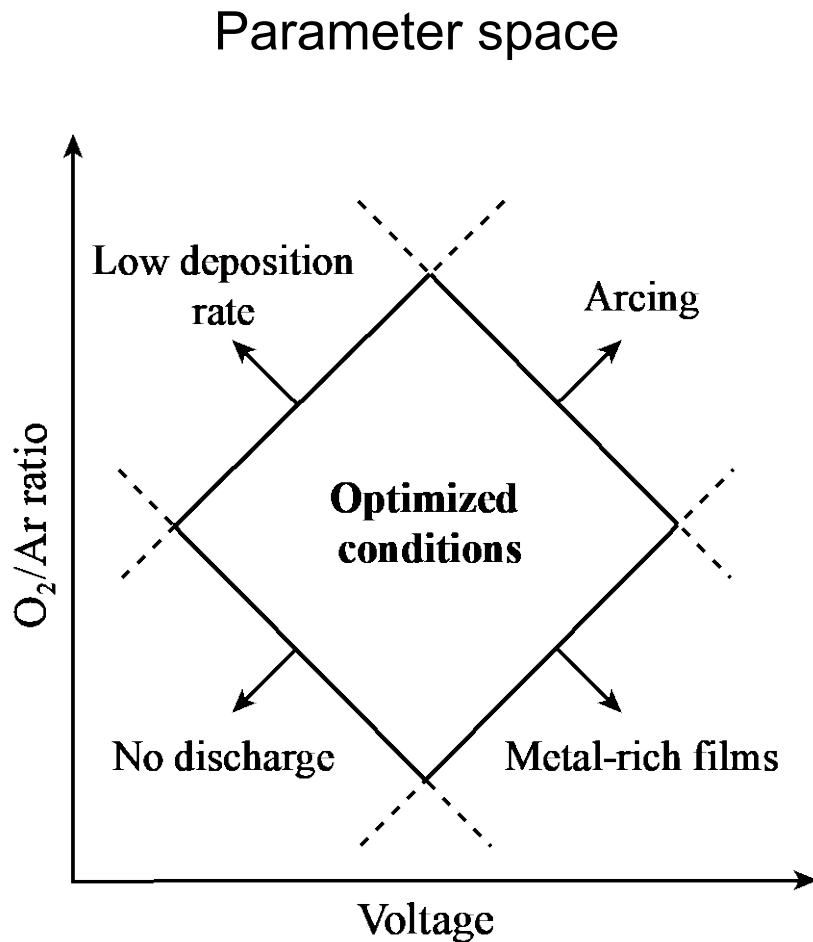


Nomenclature for pulsed discharges

[Recent review articles and comparisons:](#)

- J.T. Gudmundsson, N. Brenning, D. Lundin and U. Helmersson, J. Vac. Sci. Technol. A 30 (2012) 030801-1-35 (above)
- A. Anders, Surf. Coat. Technol. (2011), J. Vac. Sci. Technol. A 28 (2010) 783
- K. Sarakinos et al., Surface & Coatings Technology, 204 (2010) 1661
- MPP vs. HiPIMS: M. Hala et al, SCT 2012, JPD-AP, 45 (2012) 055204

HiPIMS process optimization



Effect of magnetic field:

J. Capek et al., J. Appl. Phys., 111 (2012)

Hysteresis suppression:

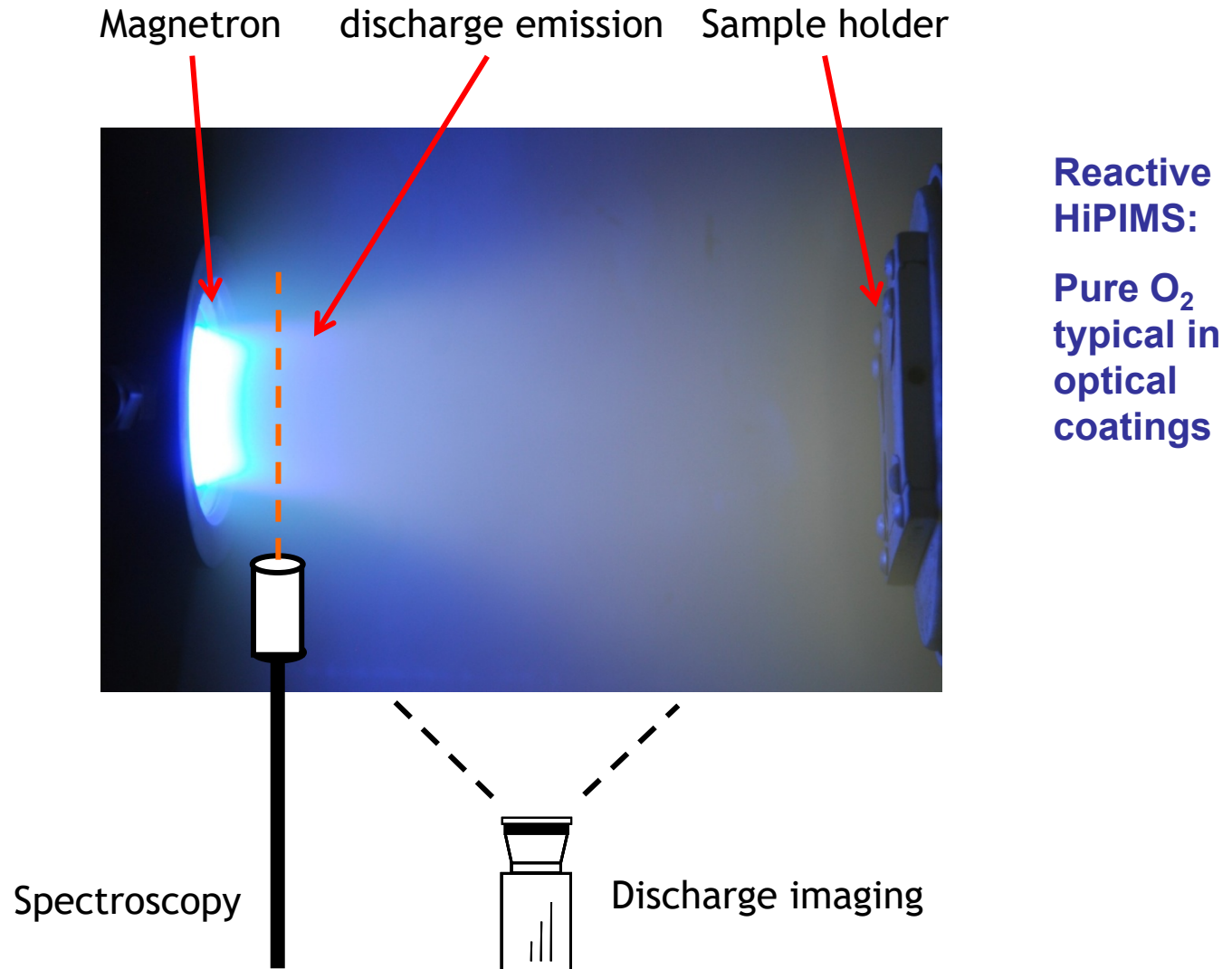
M. Hala et al., J. Phys. D: Appl. Phys., 45 (2012)

M. Hala et al., Surf. Coat. Technol. 2012

Time and space resolved OES:

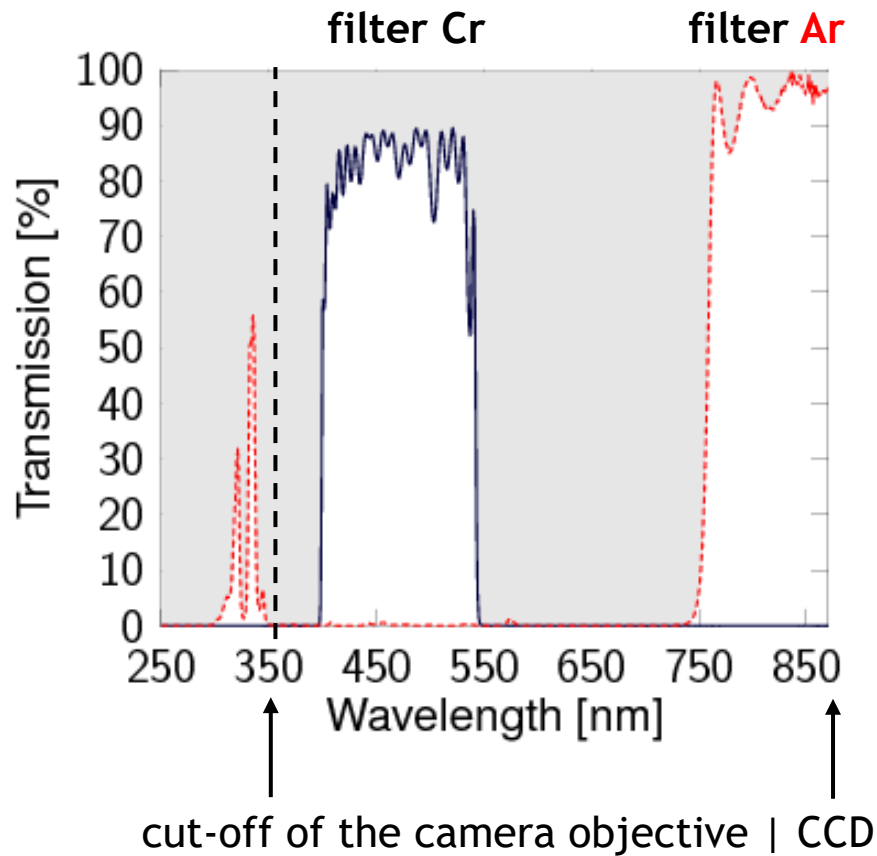
M. Hala et al., IEEE Trans. Pl. Sci., 38 (2010)

OES diagnostics – from the target to the substrate



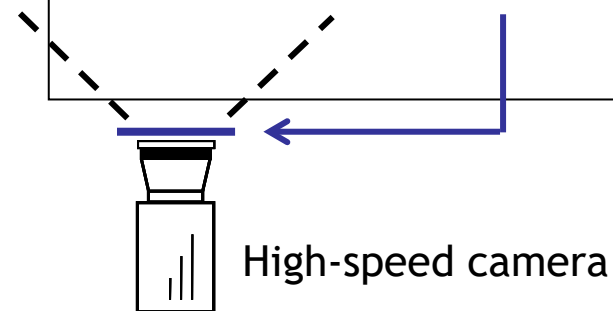
HIPIMS: Optical filters for species-resolved imaging

Filter performance and application



Introduction of custom-made band-pass interference filters

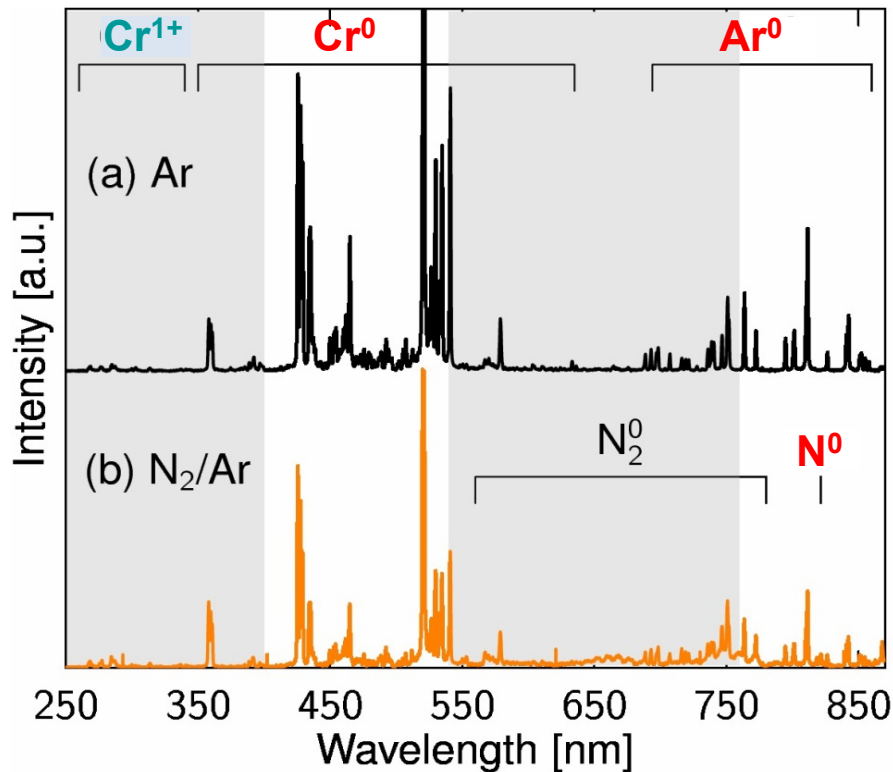
- high-transmission regions:
- 400 to 540 nm - filter Cr
- above 750 nm - filter Ar



M. Hala et al., IEEE Trans. plasm. sci. (2010)

HIPIMS with a Cr target: Discharges in Ar, N₂, and in Ar/N₂ mixtures

5-cm magnetron $p = 4 \text{ Pa (30 mTorr)}$
 $U_c = -2000 \text{ V}$ OES at $d = 3 \text{ cm}$

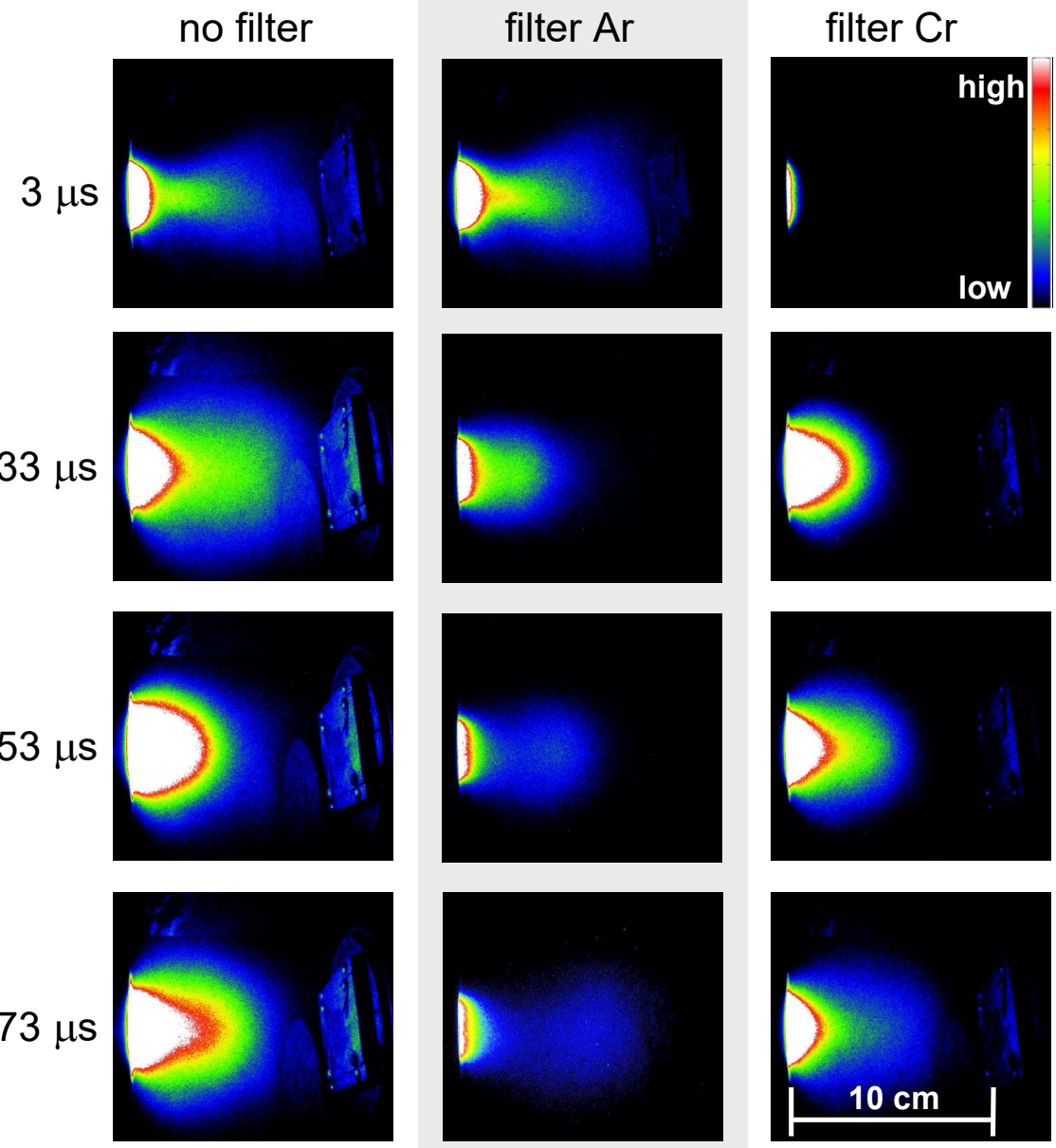


Sputtering of Cr

Two spectral regions of interest selected

- neutral chromium emission lines
- neutral gas emission lines and bands

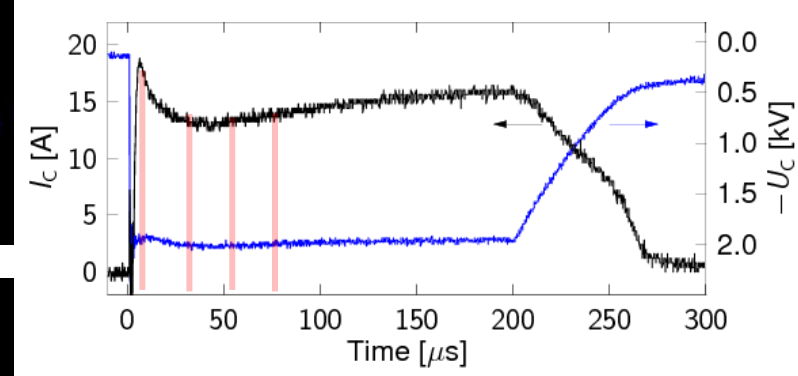
Dynamics of the HiPIMS discharge in Ar



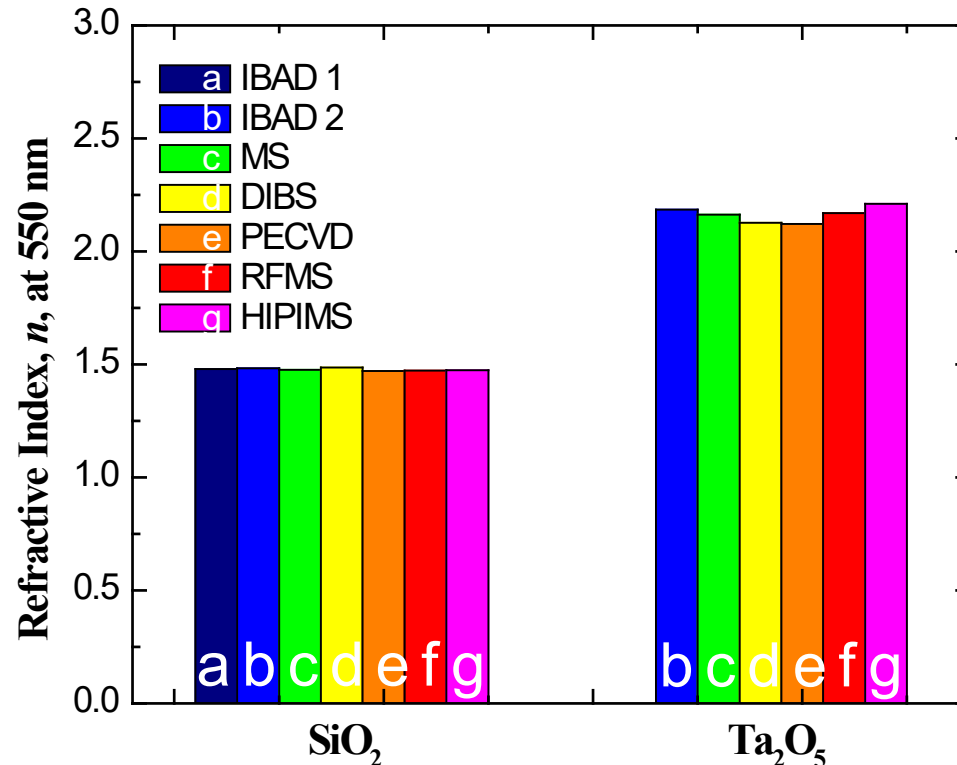
Ignition phase
 Electron avalanches and
 working-gas ion generation

Metal-dominated phase
 Self-sputtering process
 Plasma rich in sputtered Cr
 expands outwards the target

Current and voltage waveforms



Comparison of n_{550} values



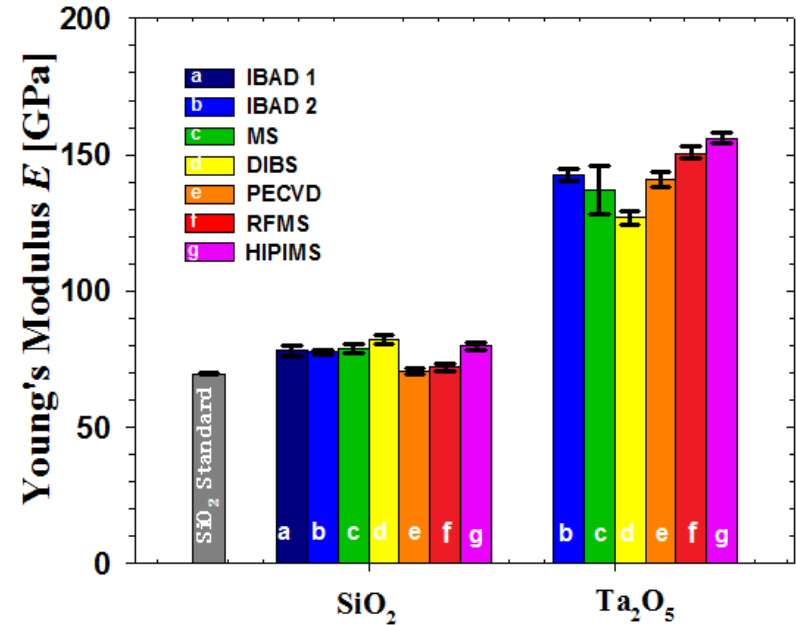
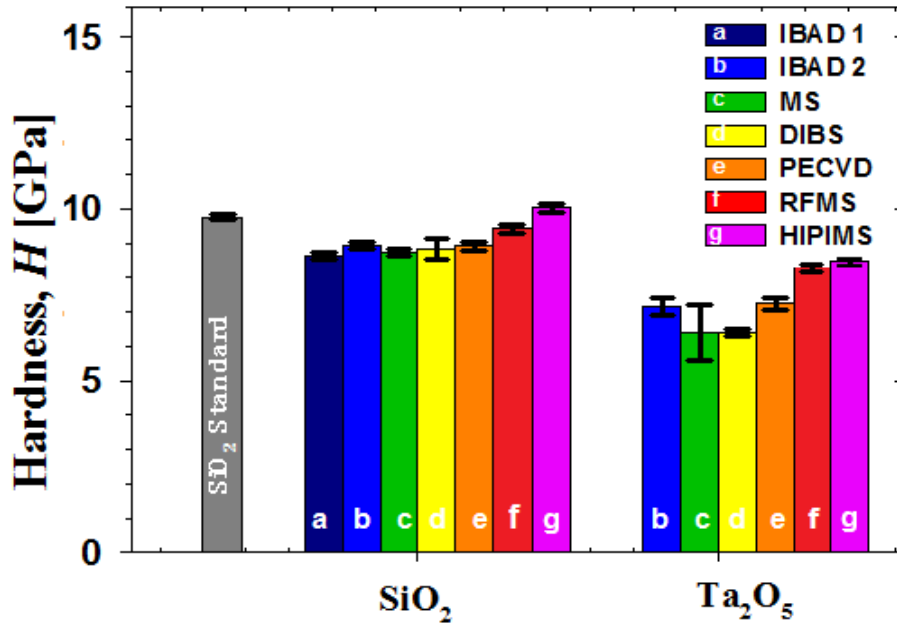
Comparative study:

Pre-characterized substrates – c-Si, FS
 Coating thickness: 1 μm
 Characteristics suitable for high-end
 optical filters

HiPIMS vs other techniques:

Comparison with J.E. Klemberg-Sapieha
 et al., Appl. Opt., 43 (2004) 2670

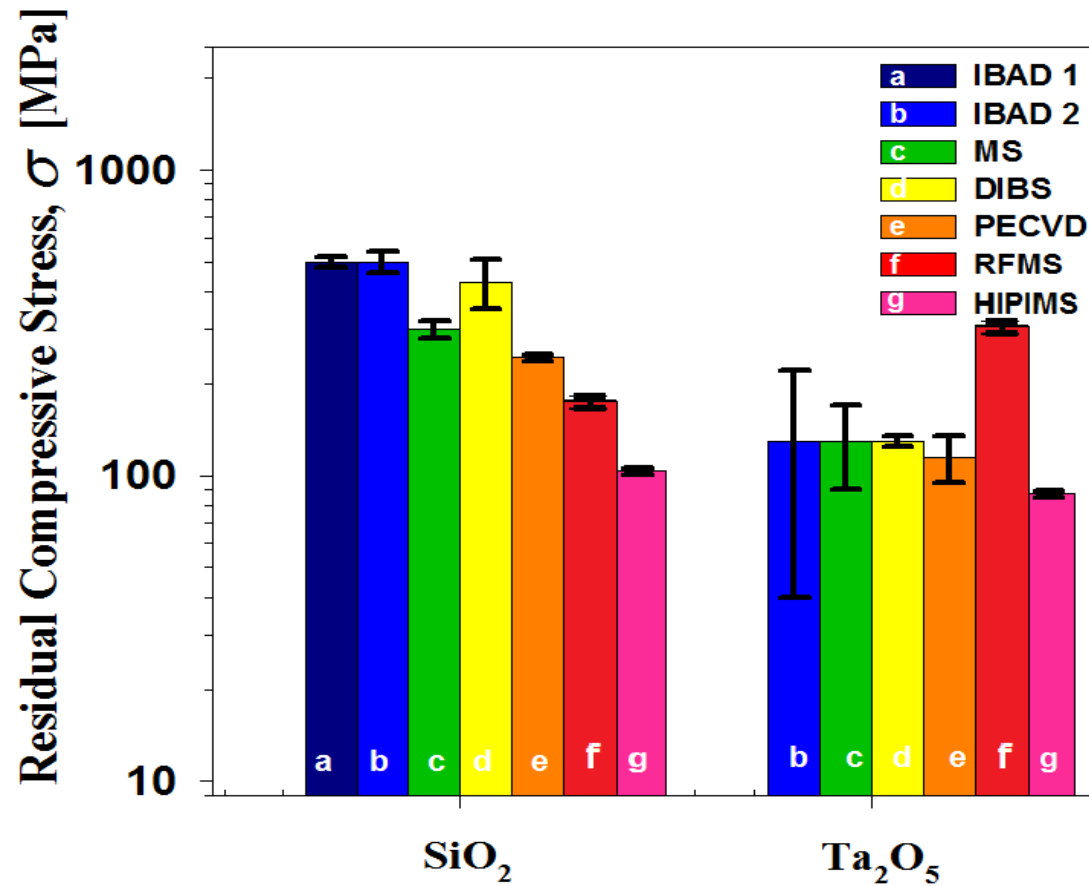
Hardness and Young's modulus



HIPIMS vs other techniques:

Comparison with J.E. Klemberg-Sapieha et al., Appl. Opt., 43 (2004) 2670

Residual stress

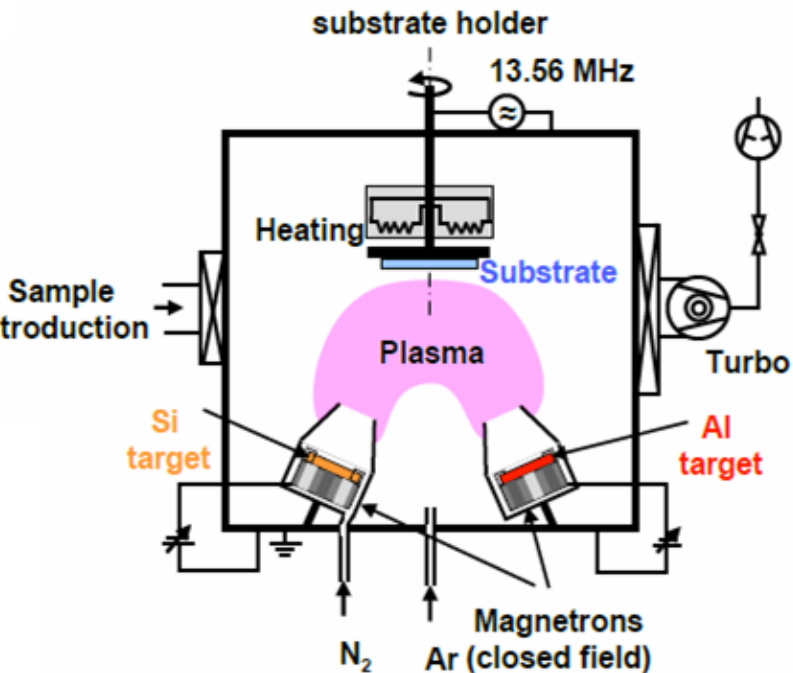


HiPIMS vs other techniques:

Comparison with: J.E. Klemberg-Sapieha et al., Appl. Opt., 43 (2004) 2670



Nanocomposite Al-Si-N films



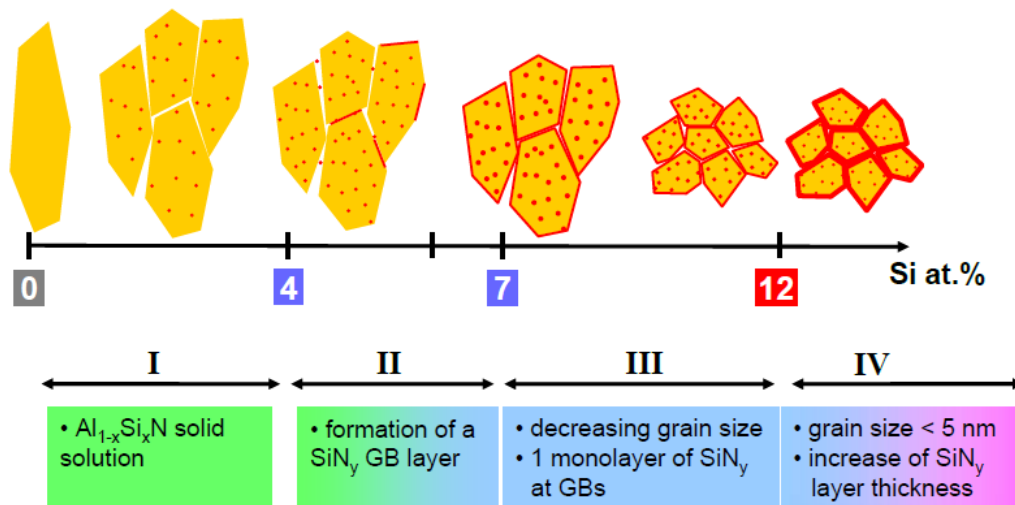
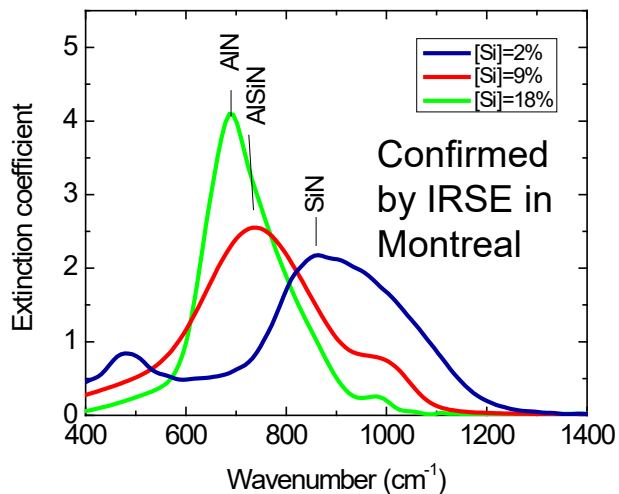
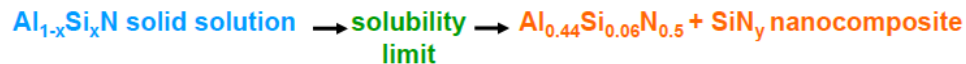
Reactive UBM sputtering from Al and Si targets

Pressure: ~0.3 Pa
 Substrate Temp: 200°C
 Deposition rate: ~250 to 650 nm/h
 Thickness: ~1-2 μm

AlN to Al-Si-N with up to 23 at.% Si

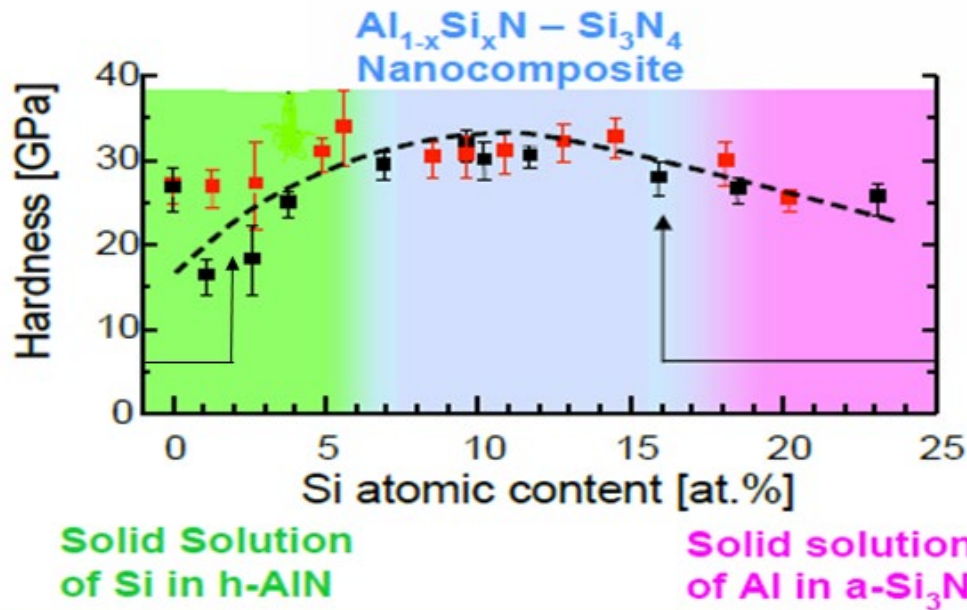
Formation of nanocomposite at [Si] > 6 at.%
 $\text{Al}_{0.88}\text{Si}_{0.12}\text{N}$ with Si_3N_4

Structural evolution of Al-Si-N films

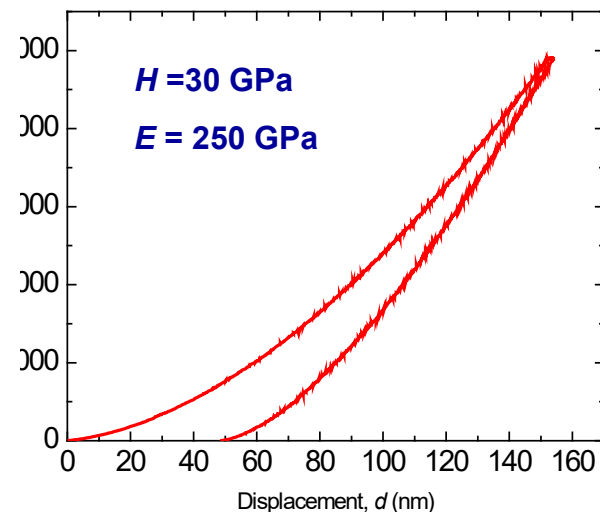




Mechanical properties of Al-Si-N



Al-Si-N with 9 at.% of Si deposited at 200 °C



Hardness of Al-Si-N depends on composition:

- Solid solution hardening
- Nanocomposite, small grain size. but structural similarities of AlN and Si₃N₄:
→ no sharp interfaces?
- Approaching the hardness of Si₃N₄

H/E - elastic strain to failure

$H/E = 0.12$

H^3/E^2 - resistance

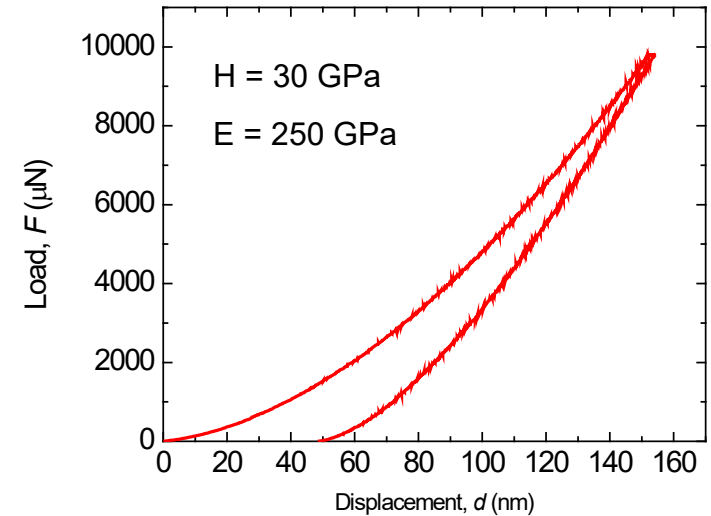
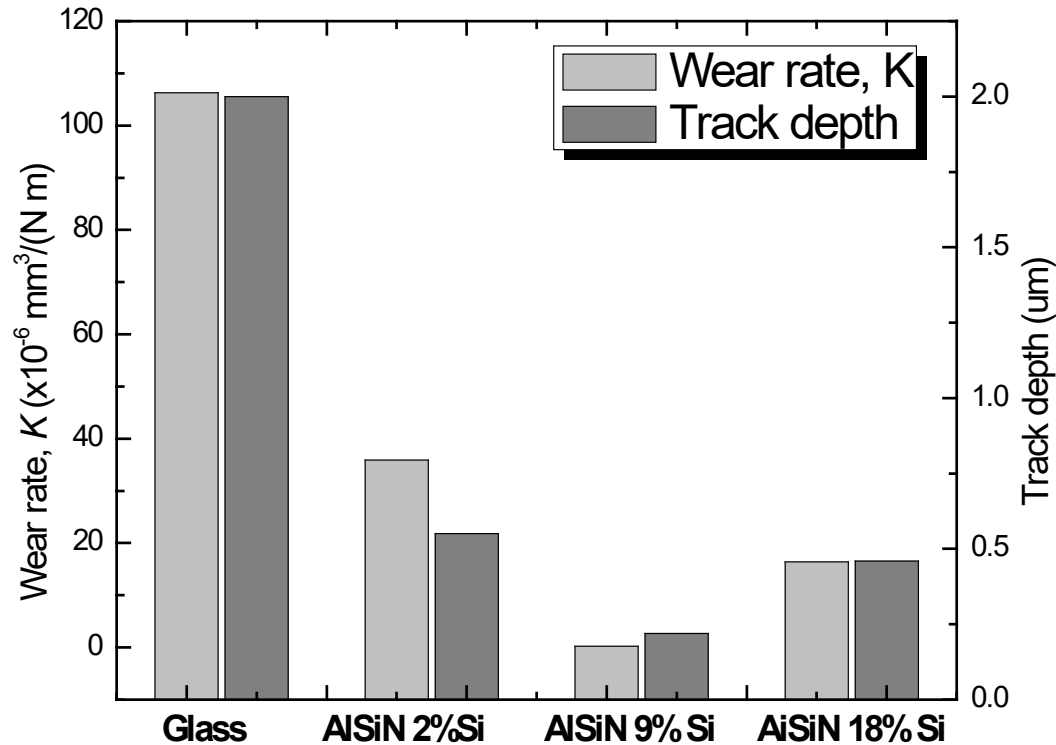
to plastic deformation

$H^3/E^2 = 0.43 \text{ GPa}$

$R \sim 80\%$

A.Péllisson, M. Parlinska-Wojtan, H.- J. Hug, J. Patscheider,
Surf. Coat. Technol. 202 (2007) 884–889

Wear resistance of Al-Si-N films



Al-Si-N: 9 at.% of Si

$$H/E = 0.12$$

$$H^3/E^2 = 0.43 \text{ GPa}$$

$$R \sim 80\%$$

Thermo-elastic characteristics of films and coatings

Thermal expansion coefficient & Poisson's ratio

Two substrate method: Thermo-elastic constants of the films were obtained from the $\sigma - T$ plots

Total $\sigma(T)$ in the film:

$$\sigma(T) = \sigma_i + (\alpha_s - \alpha_f) \left(\frac{E_f}{1 - \nu_f} \right) (T - T_d)$$

Assumption: E_f and α_f - independent of T

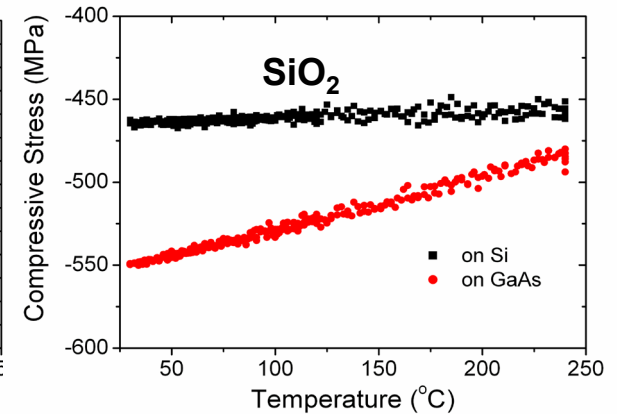
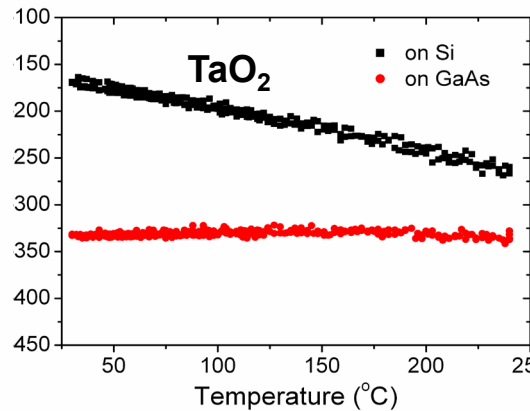
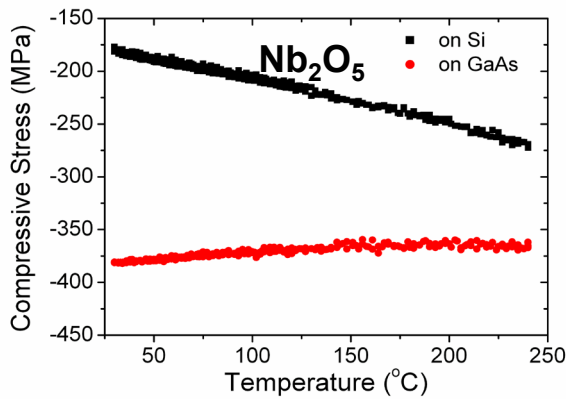
σ_i - independent of substrate

$$\left(\frac{d\sigma}{dT} \right)_{s1} = \frac{E_f}{1 - \nu_f} (\alpha_{s1} - \alpha_f) \quad \Rightarrow \quad \alpha_{film} = \frac{\alpha_{s2} \left(\frac{d\sigma}{dT} \right)_{s1} - \alpha_{s1} \left(\frac{d\sigma}{dT} \right)_{s2}}{\left(\frac{d\sigma}{dT} \right)_{s1} - \left(\frac{d\sigma}{dT} \right)_{s2}}$$

$$\nu_{film} \Rightarrow \nu_f = \left(\frac{1}{E_r} - \frac{1 - \nu_i^2}{E_i} \right) \frac{d\sigma}{dT} \frac{1}{\alpha_s - \alpha_f} - 1$$

Coefficient of thermal expansion & Poisson's ratio

σ - T plots : Nb_2O_5 , Ta_2O_5 and SiO_2 prepared by DIBS



Temperature range : 30-240 °C

Heating and cooling cycles (3 x) 1.5 °C/min in N_2 ambient

Substrate: c-Si, GaAs

CTE : $\alpha_{\text{Si}} = 2.6 \times 10^{-6} \text{ }^\circ\text{C}^{-1}$ and $\alpha_{\text{GaAs}} = 5.12 \times 10^{-6} \text{ }^\circ\text{C}^{-1}$

$$\alpha_{\text{film}} = \frac{\alpha_{s2} \left(\frac{d\sigma}{dT} \right)_{s1} - \alpha_{s1} \left(\frac{d\sigma}{dT} \right)_{s2}}{\left(\frac{d\sigma}{dT} \right)_{s1} - \left(\frac{d\sigma}{dT} \right)_{s2}}$$

Results were used to calculate:

- Coefficient of thermal expansion, CTE
- Poisson's ratio, ν_f

$$\nu_f = \left(\frac{1}{E_r} - \frac{1 - \nu_i^2}{E_i} \right) \frac{d\sigma}{dT} \frac{1}{\alpha_s - \alpha_f} - 1$$

Results – Comparison with published data

Film Material	$E_f/(1-n_f)$ (GPa)	E_f (GPa)	CTE $\times 10^{-6}$ ($^{\circ}\text{C}^{-1}$)	ν_{ϕ}	References
Nb_2O_5	139	130	4.9	0.22	This work
	–	–	1.52	–	[33]
	–	60	5.8	0.20	[34]
	–	–	-2.0	–	[35]
	–	125	–	0.23	[39]
Ta_2O_5	143	136	4.4	0.27	This work
	1549	–	2.45	–	[17]
	–	–	2.3 to 5.6	–	[36] [37] [38]
	1549	–	2.42	–	[1] [36]
	–	–	6.72	–	[38]
SiO_2	93	87	2.1	0.11	This work
	3257	–	0.38	–	[17]
	–	86	3.10	–	[21]
	–	75	0.55	0.16	[34]
	–	72	–	0.17	[39]

1. Thien et al OC **198** 2001.
17. Lee et al RSI **72**(4) 2001.
21. Thielsch et al AO **41**(16)2002.
33. Thien et al JMO **47**(10) 2000.
34. Chen et al JAP 101, 2004.
35. Choosuwan et al, JAP **91**, 2002.
36. Weyant et al, J. Am. Ceram. Soc. **88**, 2005.
- 38 al J. Mater Sci. **41**, 2006.
39. Chudoba et al Surface Coat. Technol. **127**, 2000.

Development of passive thin films

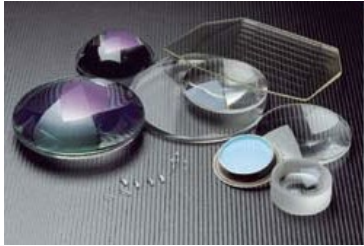
Optical coatings:

- Choice of the fabrication technique
- New technologies

Gas and vapor diffusion barriers:

- Thin films on plastics

Applications of optical coatings on plastics



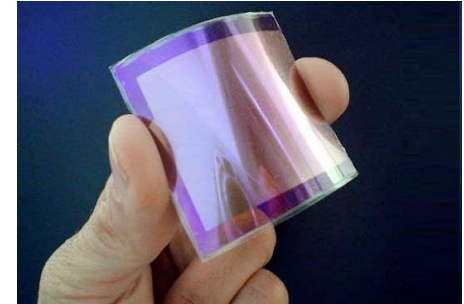
lenses
optical components



flexible electronics



displays



flexible solar cells



optical security devices



aerospace



automotive

Why plastics?

- **Cost**
- **Flexibility**
- **High strength-to-weight ratio**
- **Lightweight**
- **Safety**
- **Roll based processing**

Problem: Coating-substrate compatibility

Properties of selected optical plastics

Polymer	n [@550nm]	ρ [g/cm ³]	WA [%]	CTE [$\mu\text{m}/\text{m}^\circ\text{C}$]	ST [$^\circ\text{C}$]	H (DSI) [GPa]	E [GPa]
PC	1.58	1.20	0.15	68-70	122-132	0.2;118*-122*	2.1-2.3
PMMA	1.49	1.17-1.19	0.30-0.45	52-60	71-91	0.2;63*-93*	1.7-3.0
PET	1.66	1.40	0.05	59	80-100	130*	3.8
PTFE	1.35	2.17	0.03	86	260-290	58*	0.5
FEP	1.34	2.10	0.01	140	60-204	25*	0.4
PVDF	1.42	1.78	0.03	140	68-170	75*	1.8
PS	1.59	1.04	0.1	90	80	110*	2.4
PEN			<0.05		155	0.2	5.0
COP	1.53	1.01	<0.01	60-70	125		
COC	1.53	1.02	<0.01	60-70	75-170	184*	3.1
Fused silica	1.46	2.20		0.40		9.5	110
Glass	1.52	2.18		0.75		7.2	68
Diamond	2.42	3.52		1.80		98	980

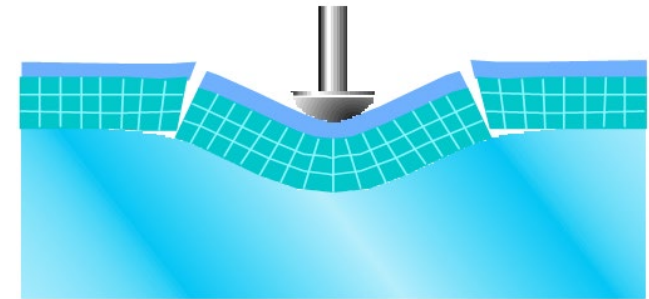
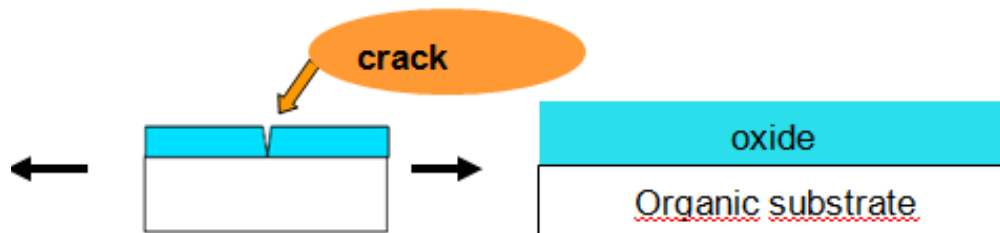
n_{550} refractive, ρ density, WA water absorption, CTE coefficient of thermal expansion @20°C, ST service temperature, H (DSI) depth sensing indentation hardness; *Rockwell hardness, E elastic modulus.

Inorganic optical films on plastic substrates

Problem: Significant mismatch between the mechanical properties of inorganic layers (e.g., anti-reflective (AR) coatings) and plastics substrates (e.g., for ophthalmic applications) may lead to pre-mature failure including cracking, delamination and other adverse effects.

Mechanical sollicitation → deformation of substrate

Strain to failure of oxides < ~ 2 %



Need:

- Tailor mechanical properties of AR layers: make them "deformable" (less brittle)
- Good adhesion (at all interfaces)
- "Perfect" transparency
- Good durability (vs. "crazing", scratches, stress cracking...)
- Environmental stability (UV, humidity, temperature...)

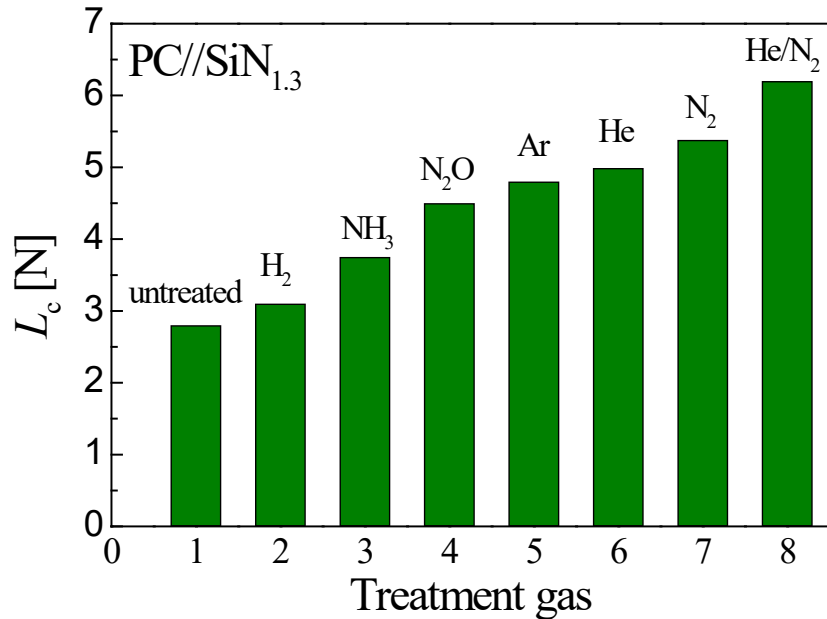
Methods to improve adhesion of coatings to polymeric surface

Plasma effects to improve adhesion

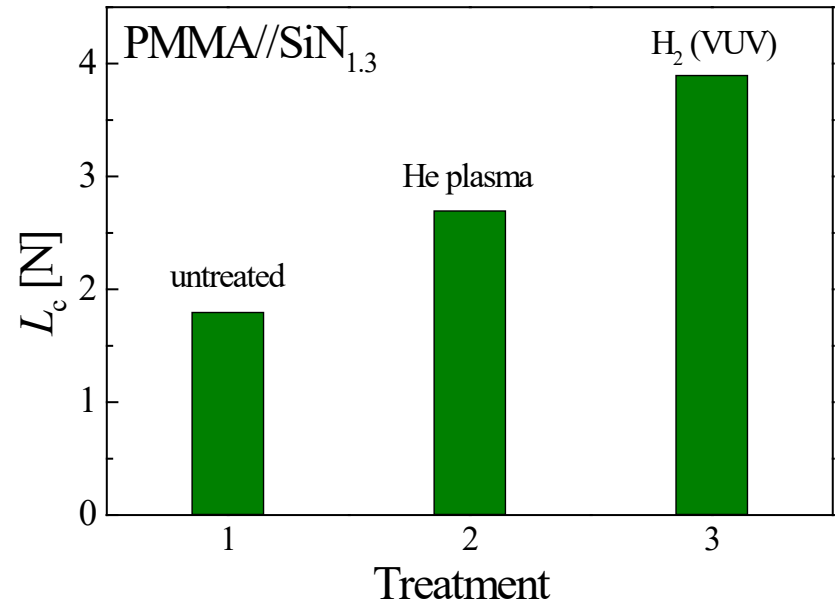
- Wet chemical treatment
- Mechanical treatment
- Exposure to flames
- UV treatment
- Ion beams
- Corona treatment
- **Low pressure plasma treatment**

1. **Surface cleaning**
(removal of organic contamination from the surfaces)
2. **Ablation**
(removal of Weak Boundary Layer, WBL)
3. **Surface crosslinking:**
CASING – Crosslinking via Activated Species of Intermediate Gases
(creation of free radicals on polymer surfaces via ion bombardment, VUV photons)
4. **Surface chemistry modification**
(incorporation of chemical functionalities on polymer surfaces)
5. **Surface electric charge**
6. **Deposition of intermediate layers**
7. **Atomic interface mixing**

Adhesion of Si_3N_4 films on plastics: Case study of PC and PMMA

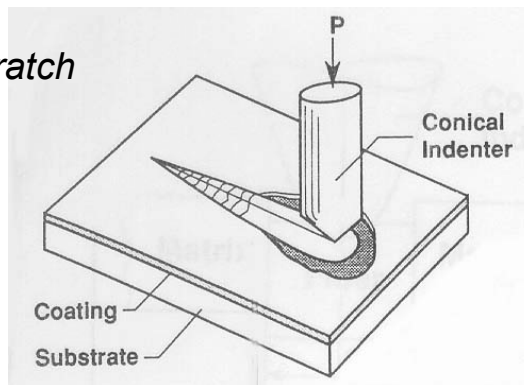


MW plasma pre-treatment in different gases



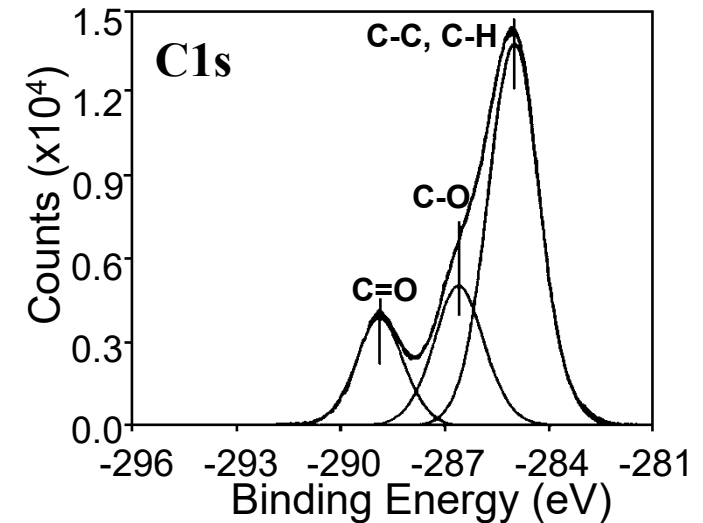
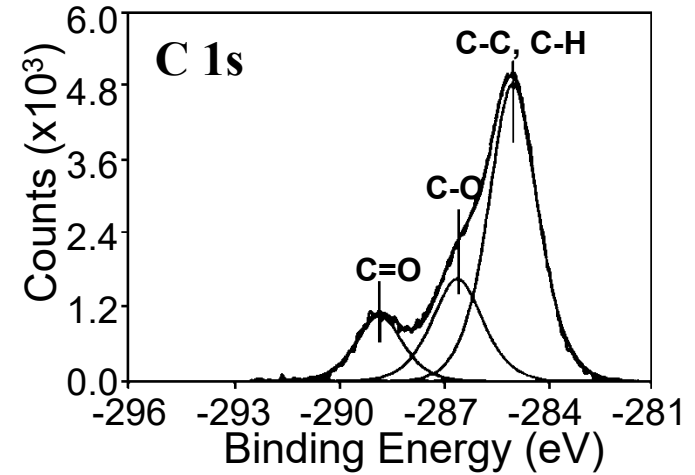
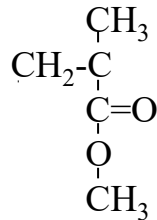
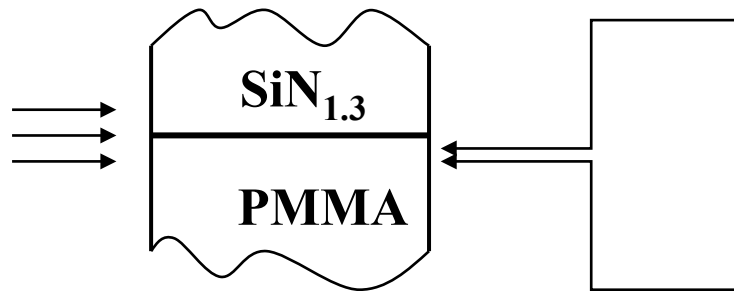
Pretreatment by He plasma or VUV radiation

Micro-scratch test



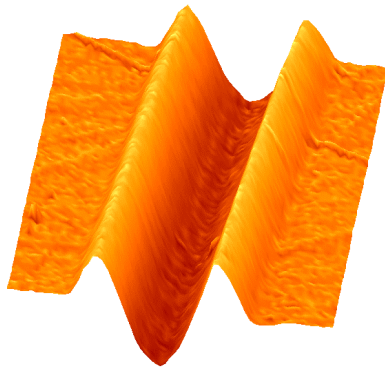
Martinu and Klemberg-Sapieha: "Optical coatings on plastics", in "Optical Interference Coatings", Springer 2003

PMMA/SiN_{1.3} interface

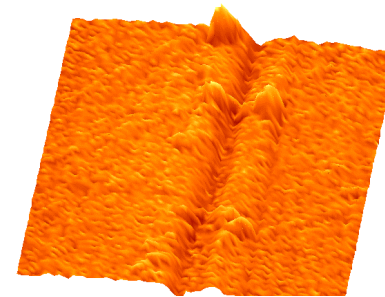
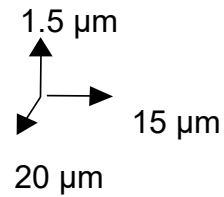


Klemberg-Sapieha et al., MRS Proc. 1998

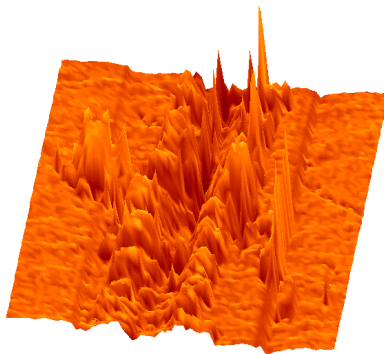
AFM images of scratch track profiles



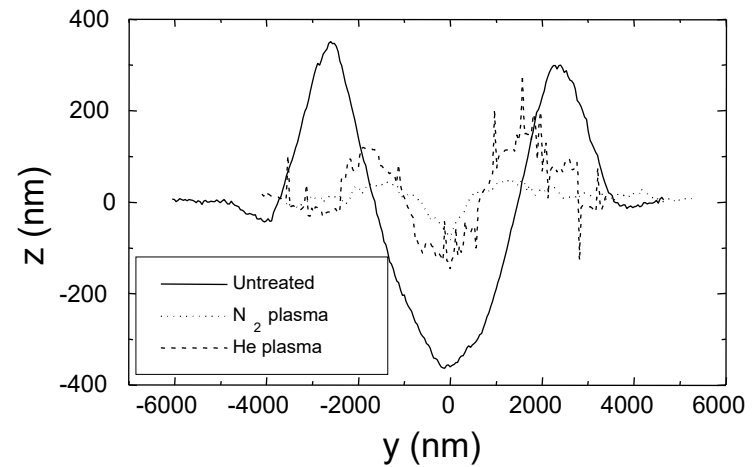
Untreated PC



PC/ N_2

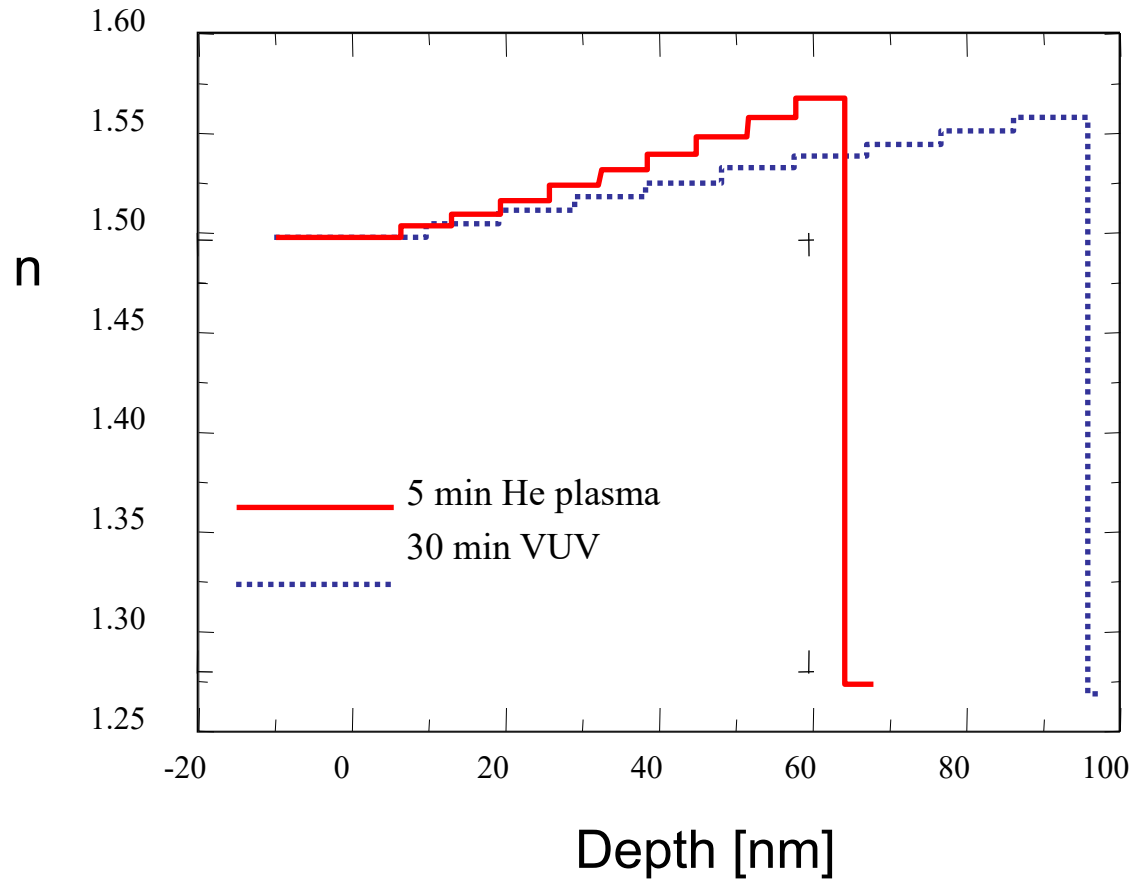


PC/He



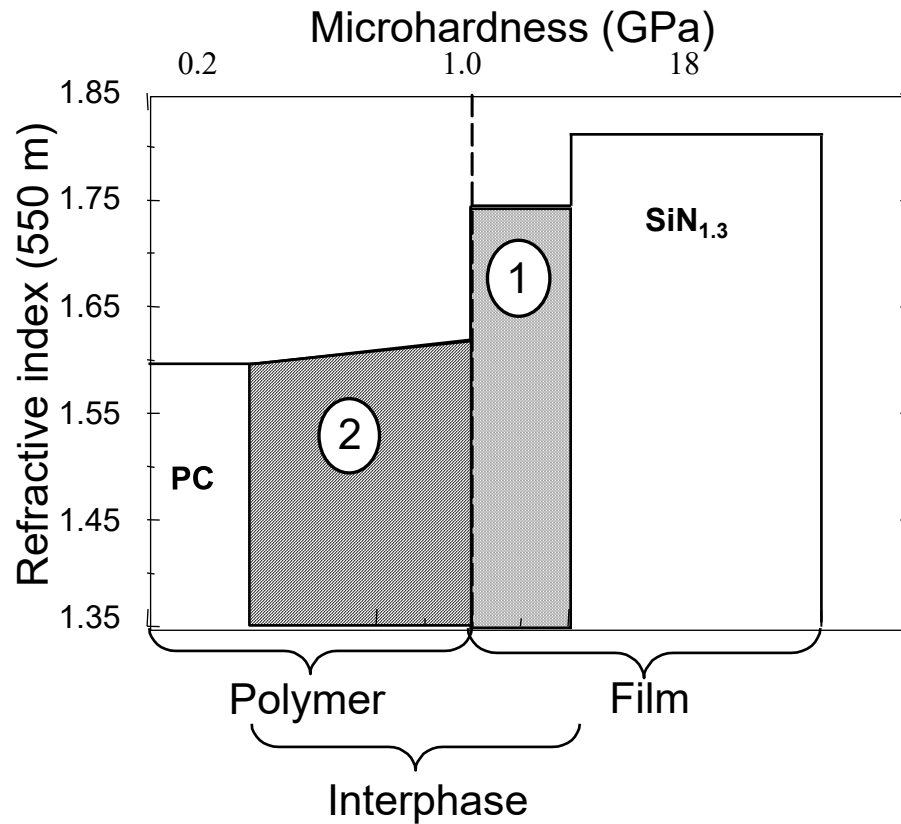
S. Dahl et al., Thin Solid Films, 1999

Refractive index depth profile for PMMA - spectroellipsometry



J. E. Klemberg-Sapieha et al, TSF 1998

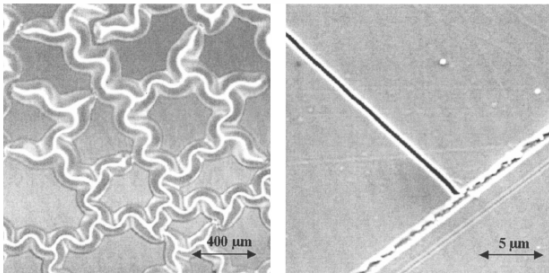
Interphase



J.E. Klemberg-Sapieha et al., SVC Proc., 2000

Challenges in coating plastics

Properties of selected plastics and coatings

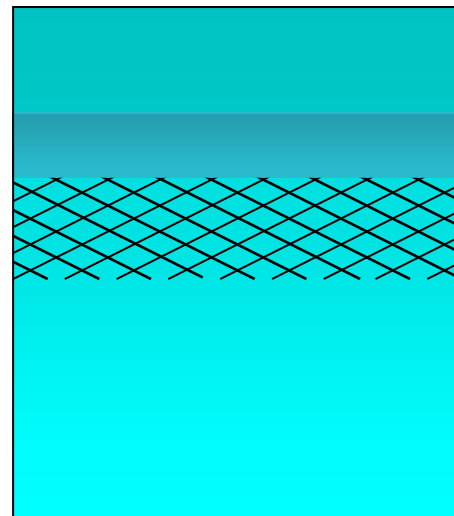


buckling of a coating tensile-stress cracking

U. Schulz, Appl. Opt., 2006

Polymer	ρ [g/cm ³]	CTE [µm/m°C]	H [GPa]	E [GPa]
PC	1.20	70	0.2	2.0
PMMA	1.18	60	0.2	1.8
PET	1.40	59	0.3	3.8
COP Zeonor	1.01	70		
SiO ₂	1.98	2.1	9.5	85
Ta ₂ O ₅	8.20	4.4	7.0	135
Nb ₂ O ₅	4.50	4.9	6.0	125

Solution:
Tailoring the
interfacial region

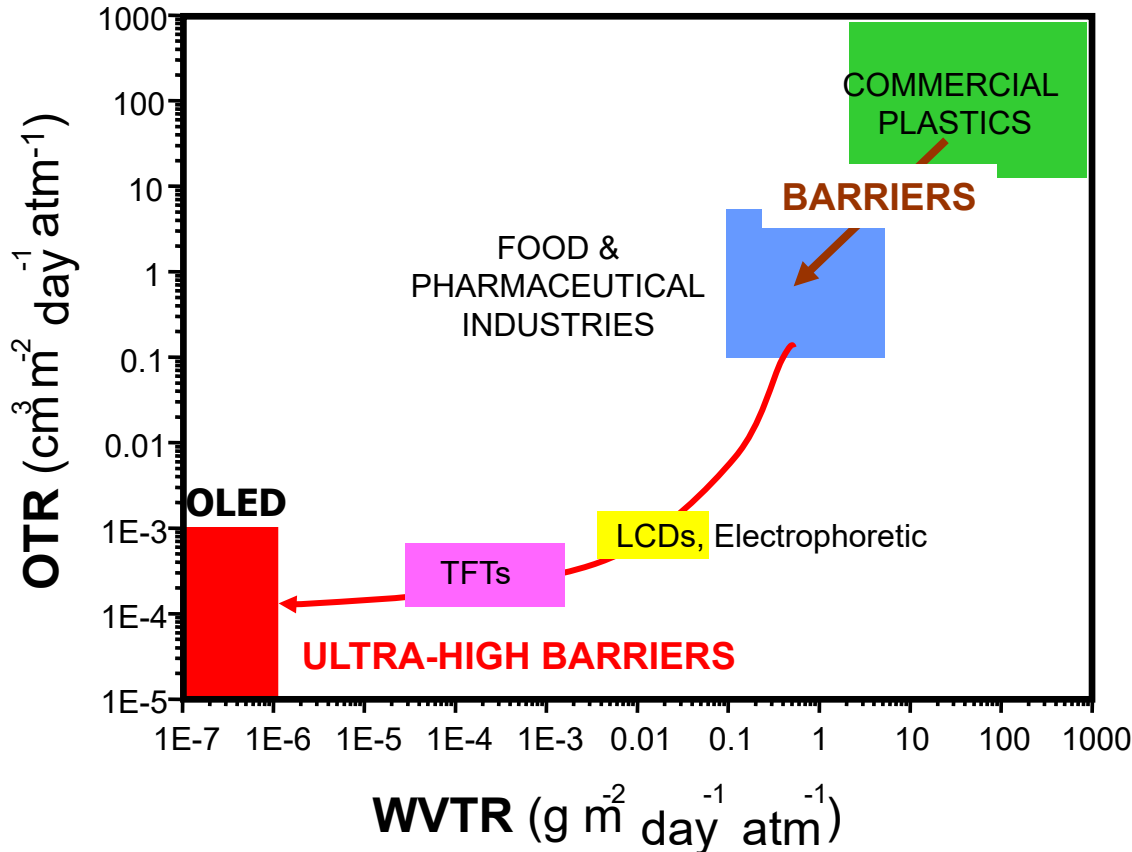


Coating
 Covalent bonding } Graded interfacial
 Crosslinked layer } region
 "interphase"
 Polymer

Martinu and Klemberg-Sapieha, in Opt. Interference Coatings, Springer, 2003

Permeation barriers on polymer substrates

OTR and WVTR requirements for different applications and the barrier performance provided by available materials.



Barrier requirements

Food & Pharmaceutical Industries:

OTR = 0.1- 1 $\text{cm}^3/\text{m}^2 \text{ day atm}$

WVTR = 0.1- 1 $\text{g}/\text{m}^2 \text{ day atm}$

BIF ~ 100 – 1000

Barrier requirements

Organic Electronics:

OTR < $10^{-3} \text{ cm}^3/\text{m}^2 \text{ day atm}$

WVTR < $10^{-6} \text{ g}/\text{m}^2 \text{ day atm}$

BIF > 10^5 for oxygen

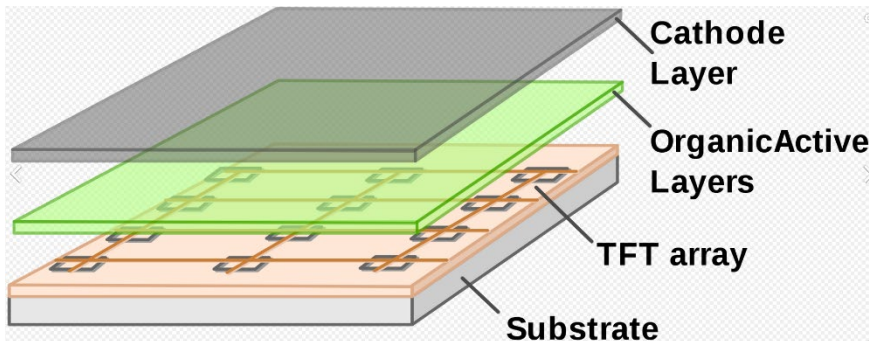
BIF > 10^7 for water

$$\text{Barrier Improvement Factor (BIF)} = \frac{\text{Permeation (bare substrate)}}{\text{Permeation (coated film)}}$$

OLED and AMOLED

AMOLED (active-matrix organic light-emitting diode) is a display device technology used in smartwatches, mobile devices, laptops, and televisions. OLED describes a specific type of thin-film-display technology in which organic compounds form the electroluminescent material, and active matrix refers to the technology behind the addressing of pixels.

As of 2008, AMOLED technology has been used in mobile phones, media players and digital cameras, and continued to make progress toward low-power, low-cost and large-size (for example, 40-inch or 100-centimeter) applications

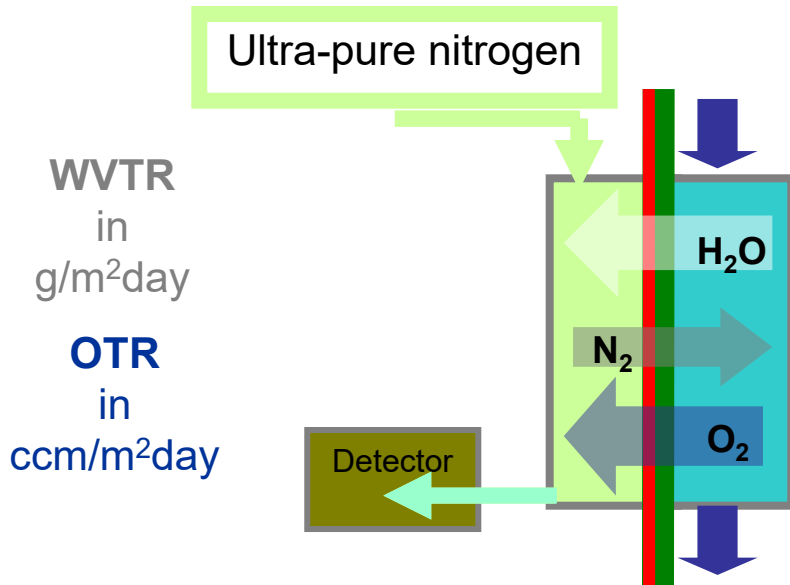


Flexible displays and flexible touch screens continue to grow; it is expected that flexible, curved and foldable displays will have **over \$75 billion revenue in 2027**.

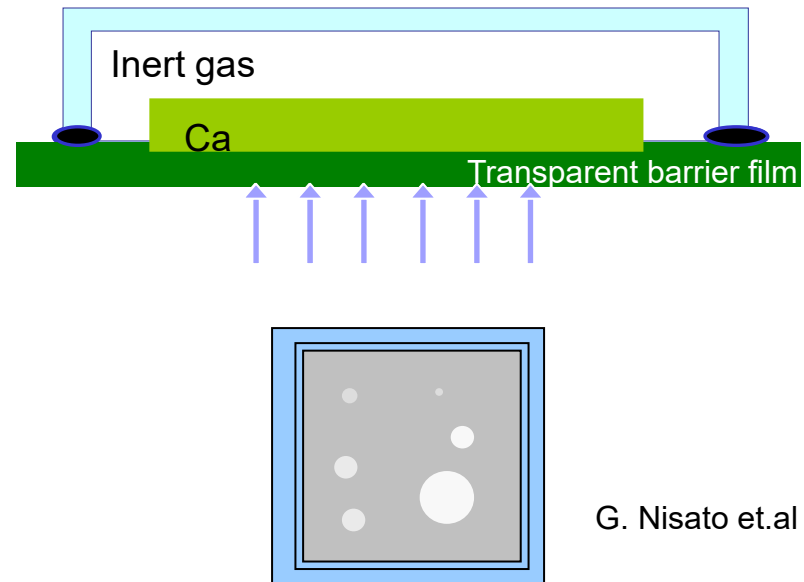
Jennifer Colegrove, Touch Display Research, private communication, May 2019

WVTR and OTR tests

Standard "MOCON" test



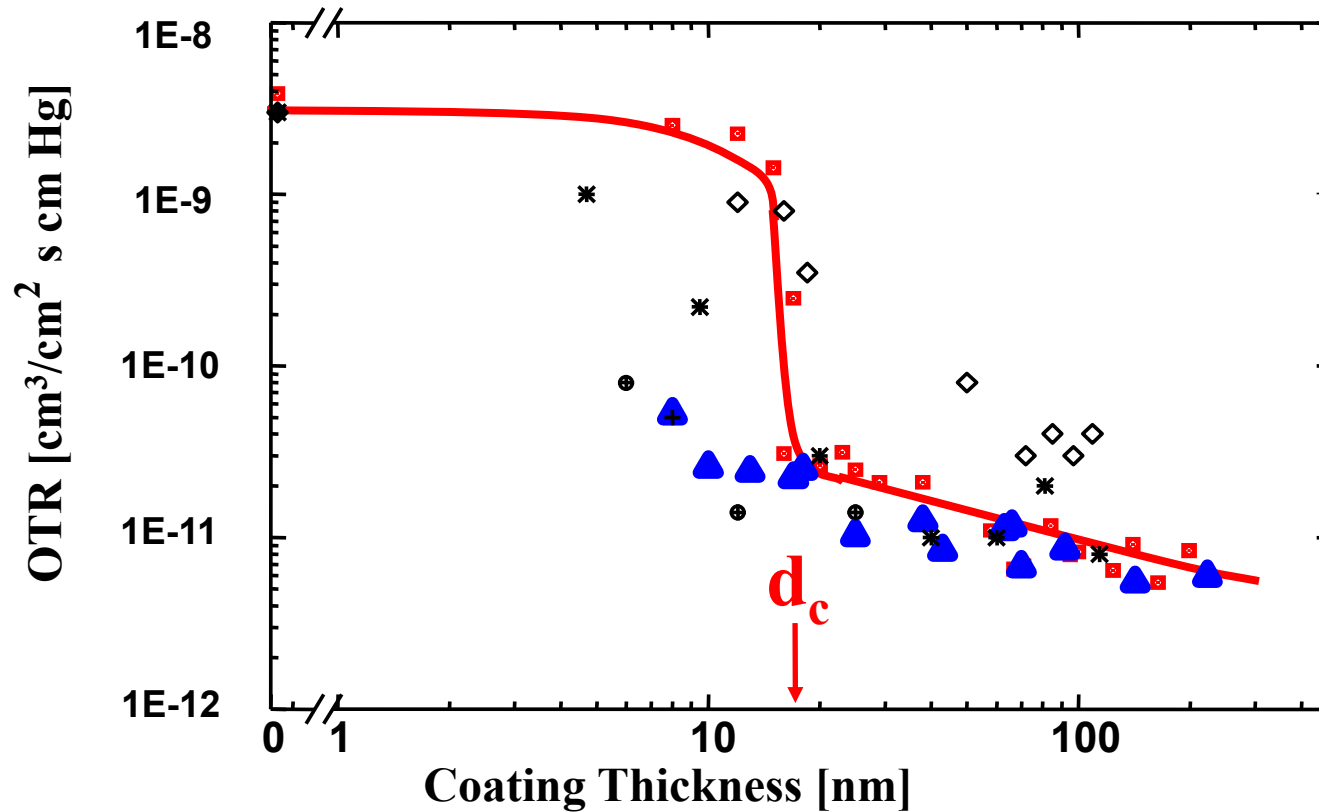
Ca test



- Standard "Mocon" test
- Calcium test
- QMS measurements (vacuum)
- OLED lifetime test
- Others

Critical thickness, d_c

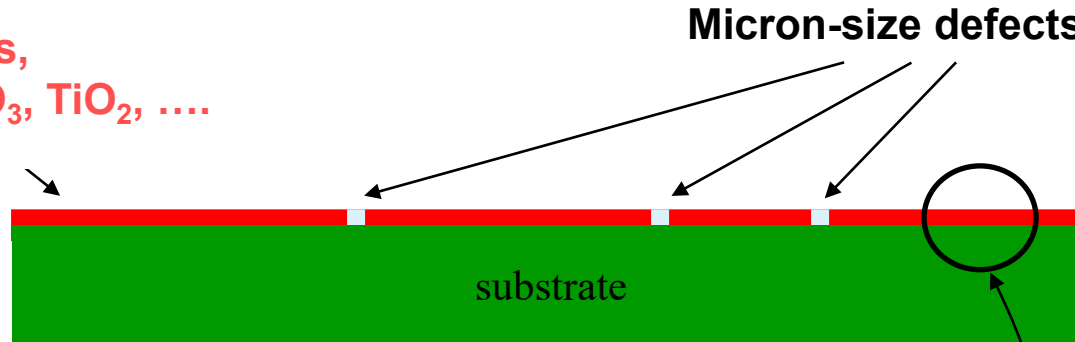
- ◇ T. G. Krug (PVD) SiO₂
- * Nelson & Chatham (PECVD)
- Izu at al (PECVD)
- Montreal
- SiO₂
- ▲ SiN



* From: H. Chatham, *Surface and Coatings Technology* 78 , 1 (1996).

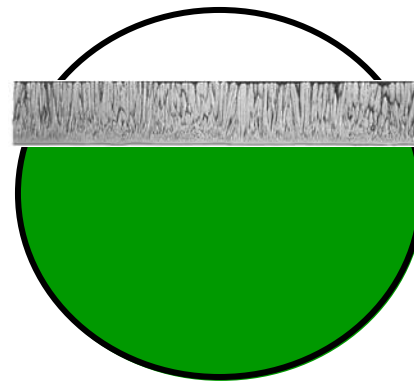
Defect-controlled permeation

Metal oxides, nitrides,
e.g. SiO_2 , Si_3N_4 , Al_2O_3 , TiO_2 ,

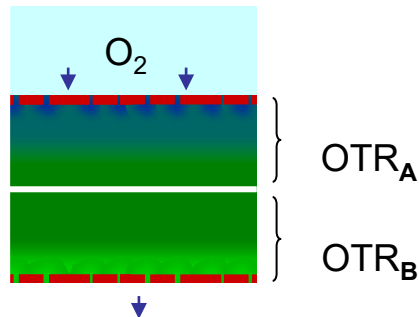
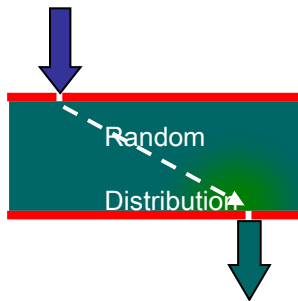


PET $E_a \sim 29$ kJ/mol

SiO_x $E_a > 80-300$ kJ/mol



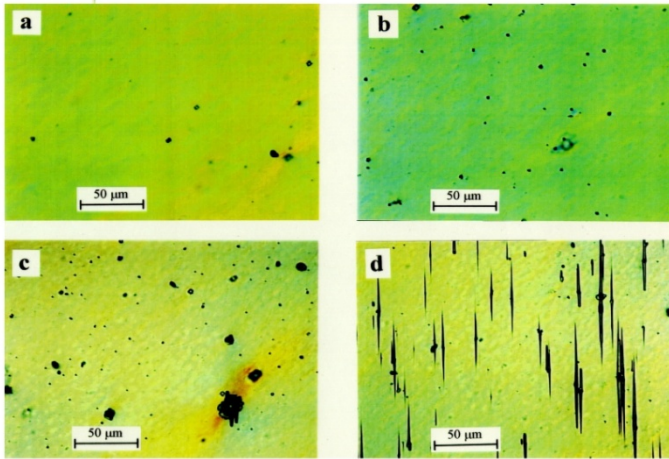
- Porosity;
- Columnar structure;
- Grain boundaries;
- Nano-cracks;
- Nano-breaches.



Permeation of gases through barrier-coated plastic films is controlled by the presence of **micron- and submicron size defects** in the otherwise impermeable coating !!!

Coating – substrates interphase

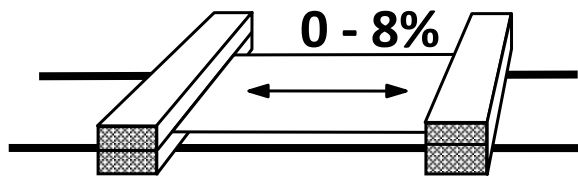
PECVD SiO₂ (200nm)/PET



Sample	Stretching	OTR cm ³ /m ² day
13 µm PET	0 %	159
	4 %	163
SiO ₂	0 %	0.3 - 1.1
	2 %	0.7 - 1.0
	3 %	2.2 - 3.3
	4 %	10.3 - 97
	4.8%	117
	5 %	137
	6 %	160
	8 %	160

← PVD
← PECVD

Films Stretching:

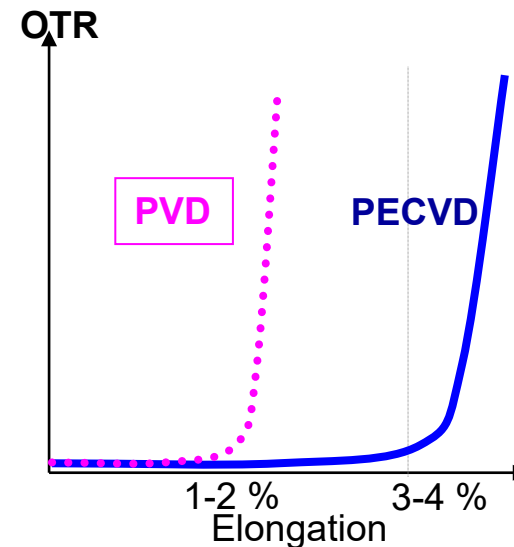


Test carried out using peel-tester 3M90, Instrumentors Inc.)

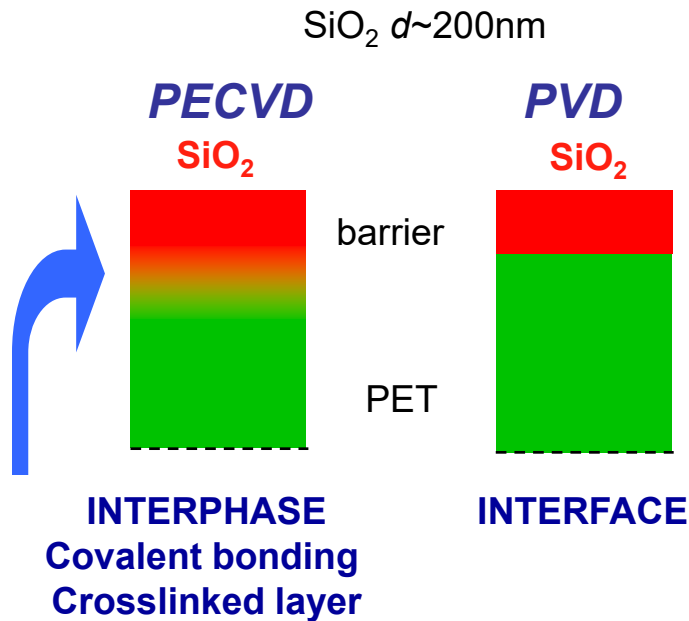
Stretching speed : 0.056 mm/s

Samples width : 9 cm or 2 cm.

G. Czeremuszkina et al., Proc. SVC 46th An. Tech. Conf. (2003)



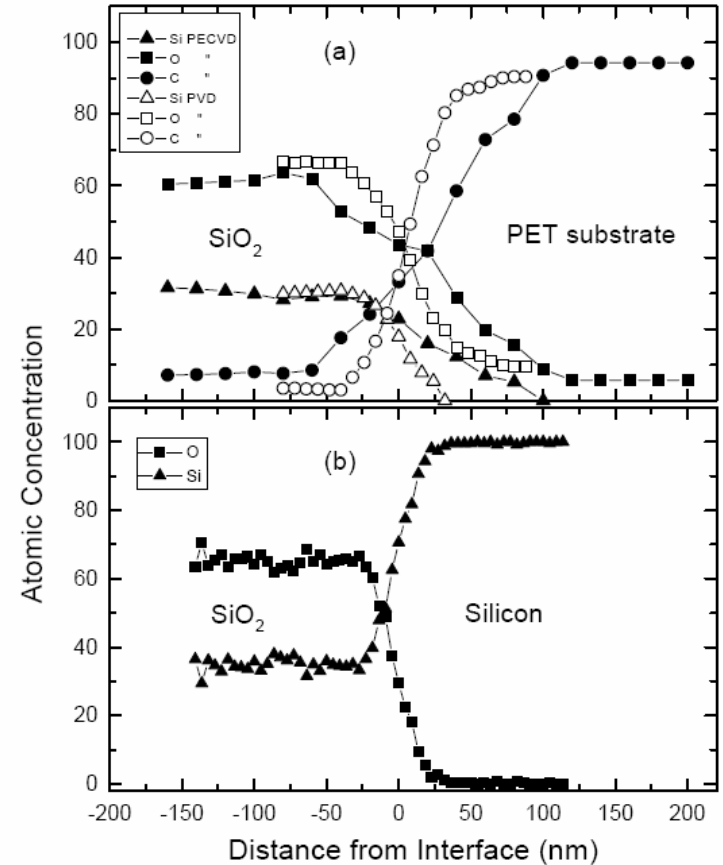
Interfacial region - Interphase



- * Thin coatings - thinner interphase 5 ~10 nm;
- * Depends on process parameters;
- * Interphase: complex structure:
Likely composed of:
 - A. Gradient transition layer (silica/substrate) with chemical bonding;
 - B. Modified substrate layer (UV, VUV, Ions);

PECVD

- Improved adhesion;
- Increased stretchability;
- Increased "bendability" of coated films.



Comparison of compositional depth profiles of the SiO₂/substrate by ERD:

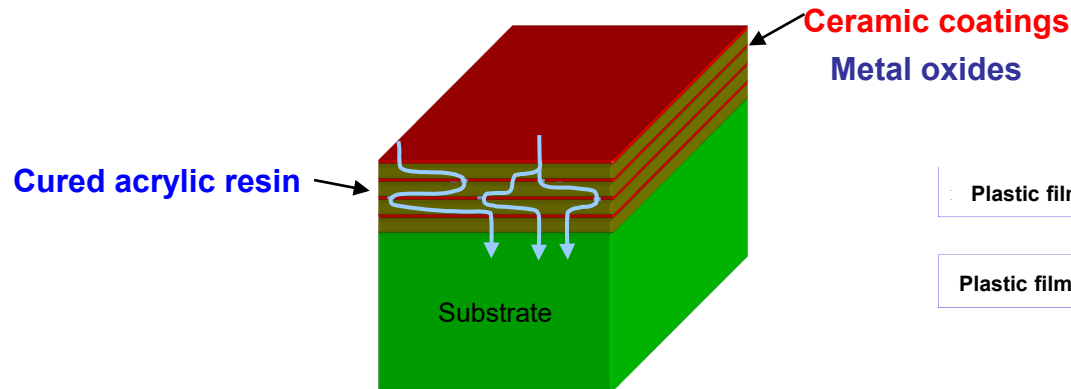
- (a) PECVD (320 nm) and PVD (120 nm);
- (b) Thermal CVD (200 nm) SiO₂ on c-Si

Da Silva-Sobrinho AS, Schüler N, Klemberg-Sapieha JE, Wertheimer MR, Andrews M, and Gujrathi SC J V S T, A 16 (1998) 3190.

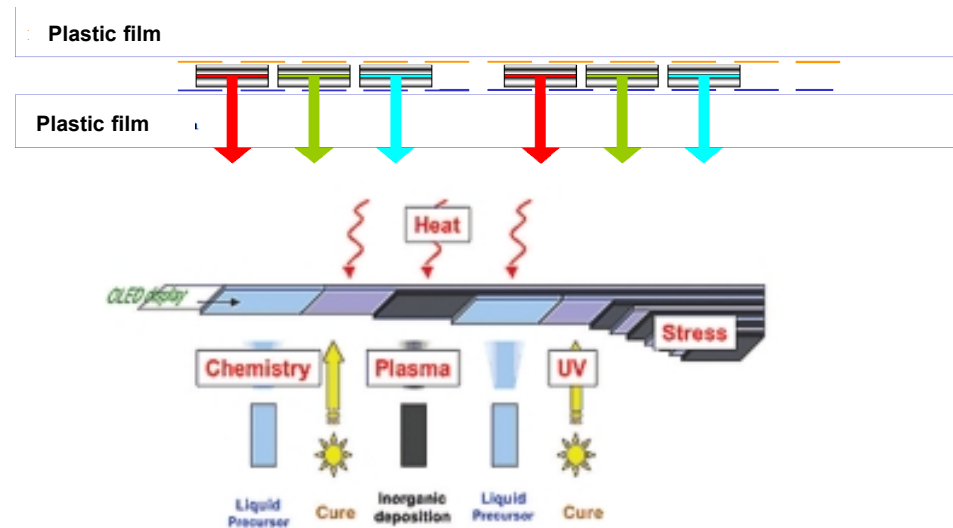
Ultra-high barriers

$$WVTR = 1 \cdot 10^{-6} \text{ g/m}^2\text{day atm}$$

corresponds to 0.006 monolayer per day !



Ultimate goal: encapsulation and flexible substrates for OLEDs



Deposition sequence of ultra barrier:

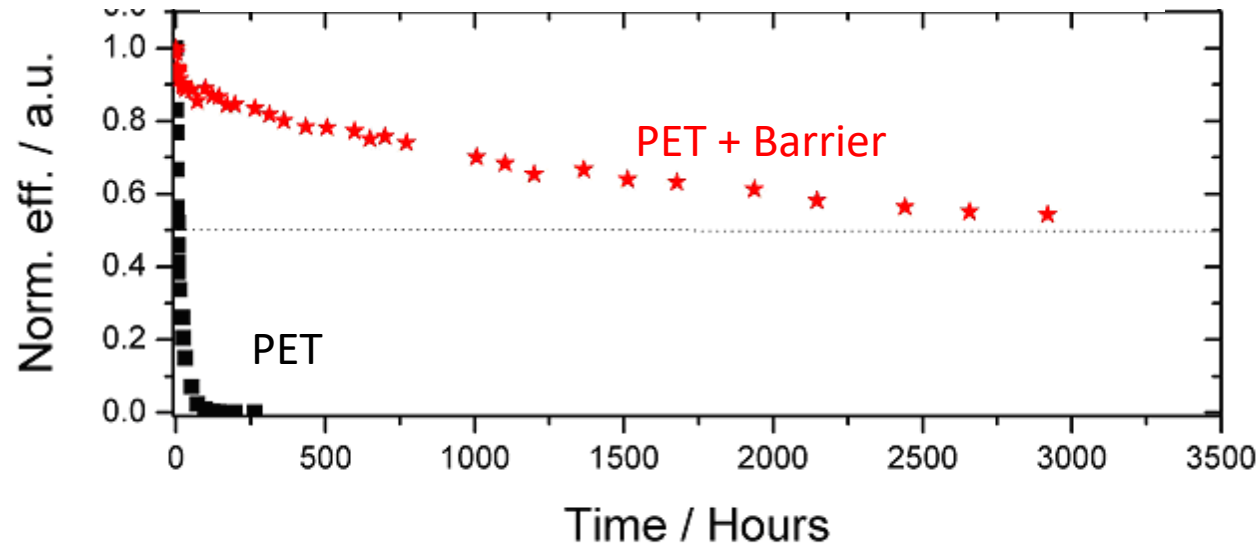
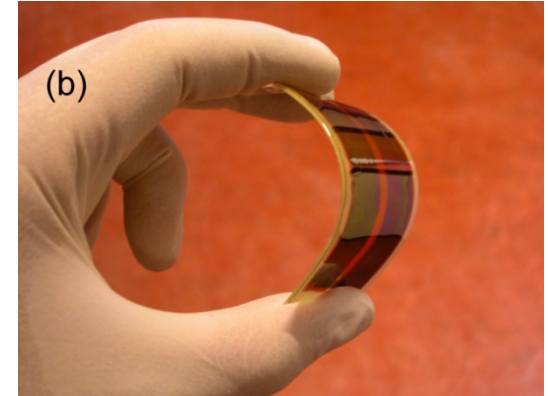
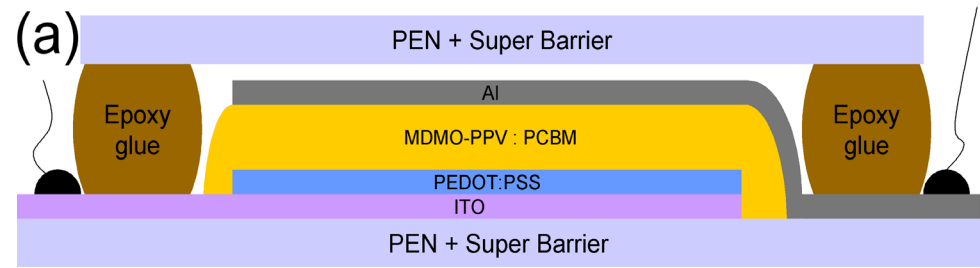
- Plasma surface activation
- Flash evaporate monomer
- UV cure
- Deposit inorganic layer
- Flash evaporate monomer
- UV cure
- Deposit inorganic layer

In line vacuum polymer deposition
(courtesy of Vitex System)

P. Martin, Vacuum Technology & Coating, 2009.

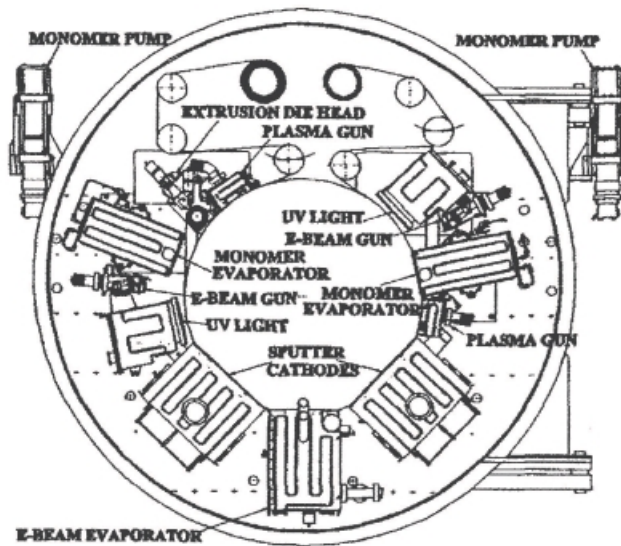
M.E. Gross et al., SVC, 2006.

Ultra-high barriers

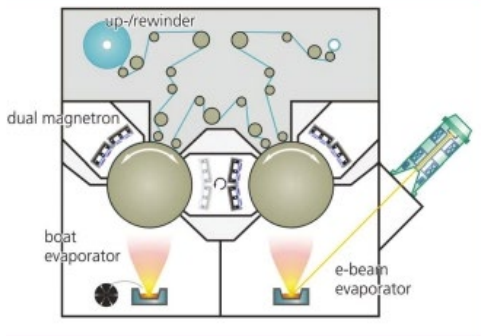


Flexible photovoltaic cell

Roll-to-roll technology for transparent barrier

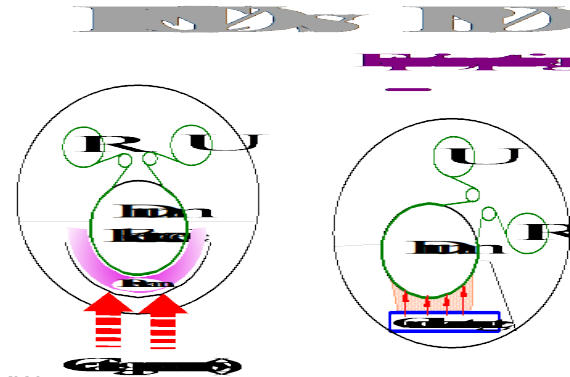


Schematic system which combine: plasma treatment, polymer evaporator, sputtering and e-beam evaporator around the central drum of web coater. M.E. Gross et al., SVC, 2006.



Pilot roll coater novel Flex 600.

N. Schiller et al., Vacuum Technology & Coating, 2009.



AC, RF, MW,
AC/RF, RF/MW

**INEXPENSIVE, FLEXIBLE,
HIGH QUALITY COLOR DISPLAY**



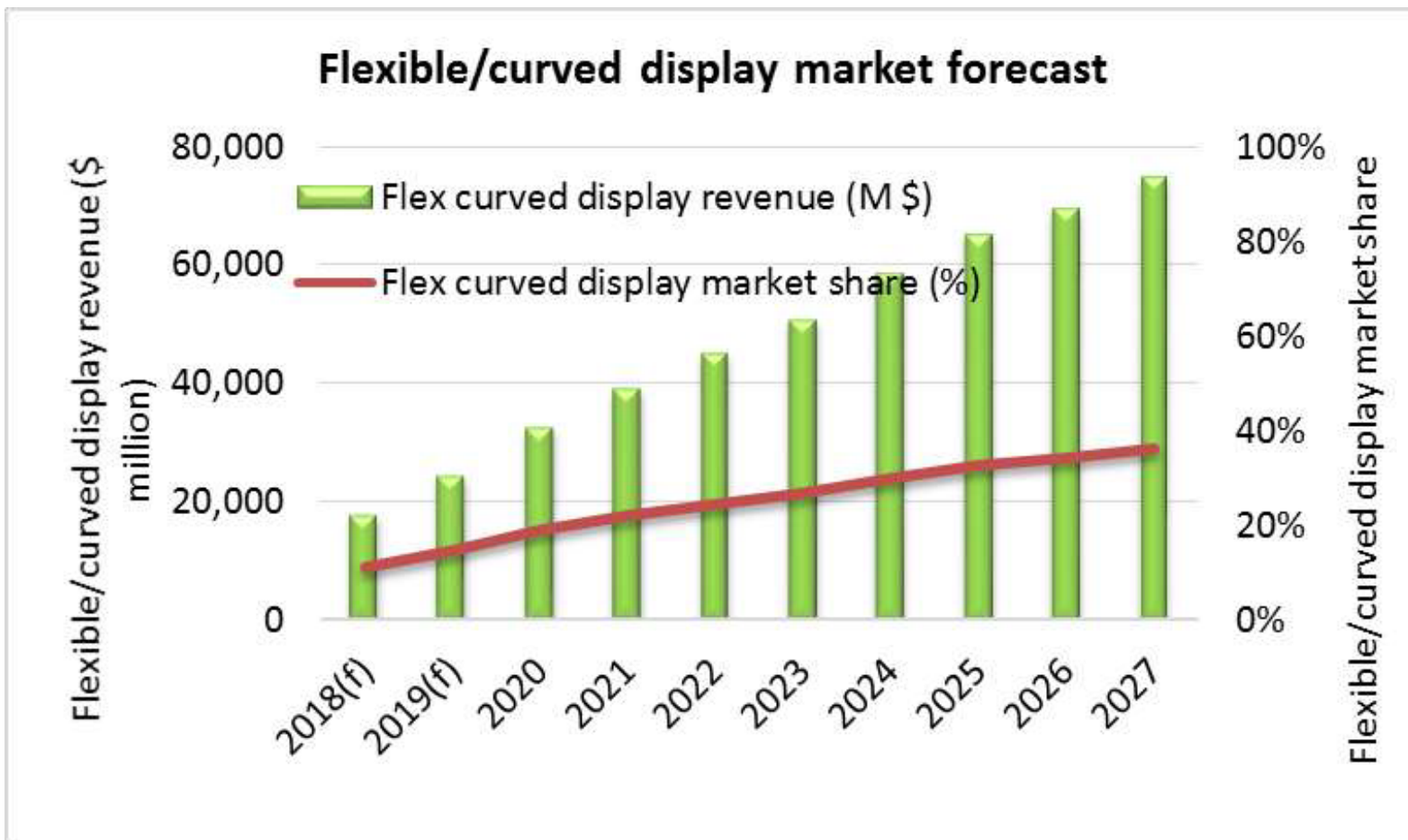
Ink jet printing,
Stamping Encapsulation

Roll to Roll processing

G. Czeremuszkín et al., SVC, 2003

Flexible, curved and foldable display market share

It is foreseen that flexible, curved and foldable display will have over \$75 billion revenue, which will be about 36% market share in 2027.



Jennifer Colegrove, Touch Display Research, private communication, May 2019



PHS 6317 Nanoengineering of thin films

Course schedule – Winter 2024

- 12 January Introduction – Scientific and technological challenges
- 19 Fabrication methods – Vacuum physics and vapor-phase techniques
- 26* Fabrication methods – Plasma processes and process optimization
- 2 February Fabrication methods - Plasma-surface interactions and diagnostics
- 9** Fabrication methods – Thermal/Plasma spray technologies
- 16* Optics of thin films 1, optical characterization, *Miniquiz1 (5%)*
- 23* Optics of thin films 2, design of optical filters
- 1*** March *Presentations – Emerging fabrication techniques (30%)*
- March 4-8 - Winter/Spring break**
- 15** Tribo-mechanical properties of films and coatings
- 22** Electrochemical properties – corrosion and tribo-corrosion (*filter-20%*)
- 5 April Functional films and coatings – Part 1, *Miniquiz 2 (5%)*
- 12 **Functional films and coatings – Part 2**
- 16 Life cycle analysis and environmental impact, **visits**
- 18*** *Presentations – Emerging applications of nanostructured films (40%)*

Deadlines:

Project #1 – Fabrication technique:

Choice of the subject: **26 January**

Abstract and references: **9 February**

Report and presentation: **1st March**

Projet #2 – Design of an optical filter:

Choice of the subject: **23 February**

Report: **22 March**

Projet #3 – Application of nanostructured thin films:

Choice of the subject: **16 February**

Abstract and references: **15 March**

Presentation: **18 April p.m.**

Report: **22 April at 23:59**

Project #3: Applications of nanostructured films and coatings

Thomas Sicotte and Alexandre Gamache - Cellules photovoltaïques à pérovskite

Alexandre Lussier - Fenêtres intelligentes thermochromiques

Mohamed Ammari - Thermal barrier coatings for aerospace gas turbine engine

Luc Montpetit - Passivation of CdZnTe for x-ray detectors

Veronika Cervenkova - Solar-thermal energy conversion - Transition metal nitrides

Émilien Martel - Electrochromic, photochromic and gasochromic coatings for consumer optics

Étienne Tremblay et Nathan Sasseville - Couches minces pour l'électronique organique – OLEDs

Thomas Lapointe - Photodétecteurs et leur conception/optimisation à l'aide des couches minces

Alexandre Carrière et Youssef Ben Mami - Électrodes transparentes pour la fabrication des cellules solaires

Arghavan Yazdanpanah Ardakani - Nanoengineering thin-films to produce hydrophobic coatings for aircraft surfaces

Mathieu Bruzzese – Oxidation-resistance barrier coatings for aerospace applications

Bastien Izacard – Atomic oxygen barrier coatings for satellites

Alexandre Fall - Carbon nanotubes for sodium-ion batteries

Alexandre Pinel - Couches minces d'hydroxyapatites pour les implants en biomedical

Christelle Abou Zeidan – Carbon nanotubes for flexible electronics