



PHS 6317 Nanoengineering of thin films

Course schedule – Winter 2024

- 12 January Introduction – Scientific and technological challenges
- 19 Fabrication methods – Vacuum physics and vapor-phase techniques
- 26* Fabrication methods – Plasma processes and process optimization
- 2 February **Fabrication methods - Plasma-surface interactions and diagnostics**
- 9** Fabrication methods – Thermal/Plasma spray technologies
- 16* Optics of thin films 1, optical characterization, *Miniquiz1 (5%)*
- 23* Optics of thin films 2, design of optical filters
- 1*** March *Presentations – Emerging fabrication techniques (30%)*
- March 4-8 - Winter/Spring break***
- 15** Tribomechanical properties of films and coatings
- 22** Electrochemical properties – corrosion and tribo-corrosion (*filter-20%*)
- 5 April Passive functional films and coatings, *Miniquiz 2 (5%)*
- 12 Active functional films and coatings
- 16 Life cycle analysis and environmental impact
- 19*** *Presentations – Emerging applications of nanostructured films (40%)*

Deadlines:

Project #1 – Fabrication technique:

Choice of the subject: **26 January**

Abstract and references: **9 February**

Report and presentation: **1st March**

Projet #2 – Design of an optical filter:

Choice of the subject: **23 February**

Report: **22 March**

Projet #3 – Application of nanostructured thin films:

Choice of the subject: **16 February**

Abstract and references: **15 March**

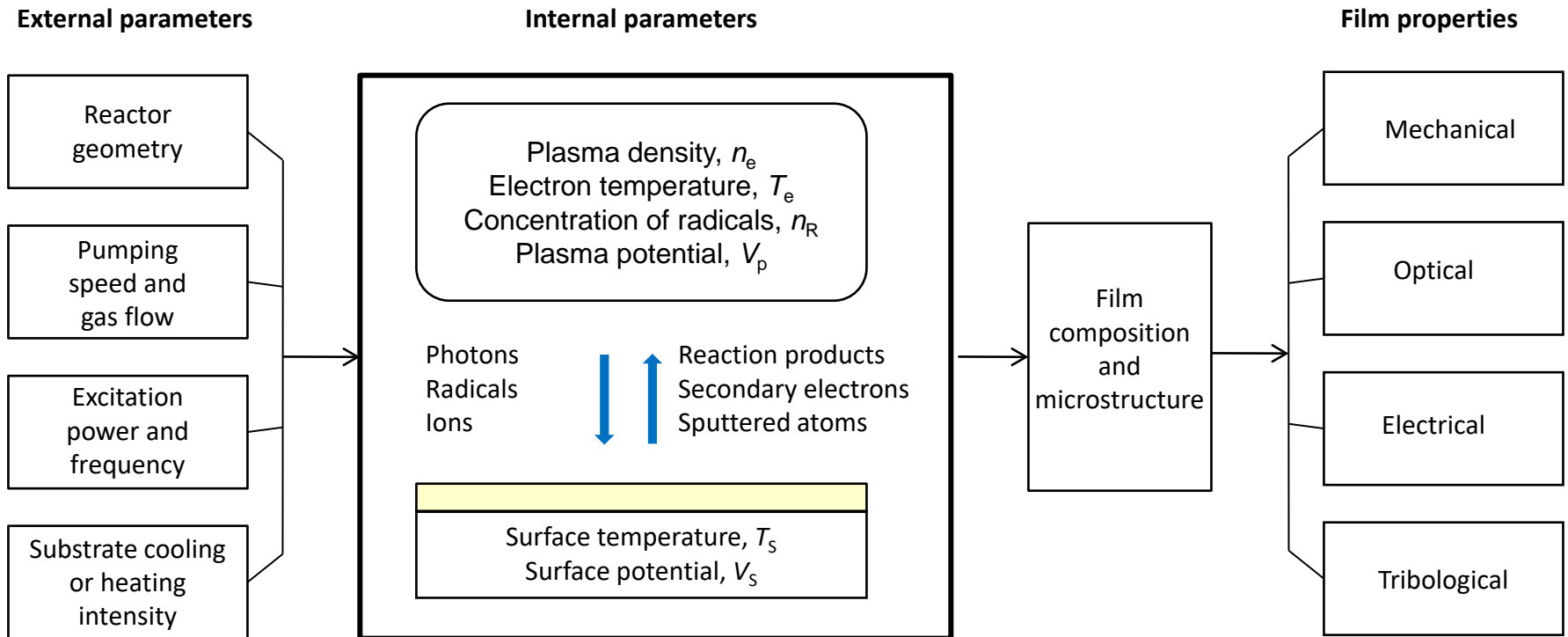
Report and presentation: **19 April**

Project #1: Techniques for the fabrication of nanostructured films and coatings

Mohamed Ammari – HiPIMS (High Power Impulse Magnetron Sputtering)
Veronika Cervenkova - Atomic layer deposition (ALD)
Emilien Martel – HVOF
Alexandre Lussier – DIBS
Gabriel Juteau - Organo-metallic MBE
Thomas Lapointe – Supersonic MBE
Luc Montpetit - Plasma-MBE
Alexandre Fall - Hollow cathode discharge for ALD
Arghavan Yazdanpanah Ardakani - PECVD
Alexandre Pinel – Reactive sputtering (pulsed DC, RF, HiPIMS)
Izacard Bastien – Cold spray
Christelle Abou Zeidan - Ultra-High Vacuum Chemical Vapor Deposition (UHVCVD)
Mathieu Bruzzese - Ion-beam assisted CVD

Etienne Tremblay-Nathan Sasseville – PIII
Alexandre Gamache-Thomas Sicotte – PLD
Alexandre Carrière-Yusef Ben Mami – Langmuir-Blodgett

Plasma system and process control



Today:

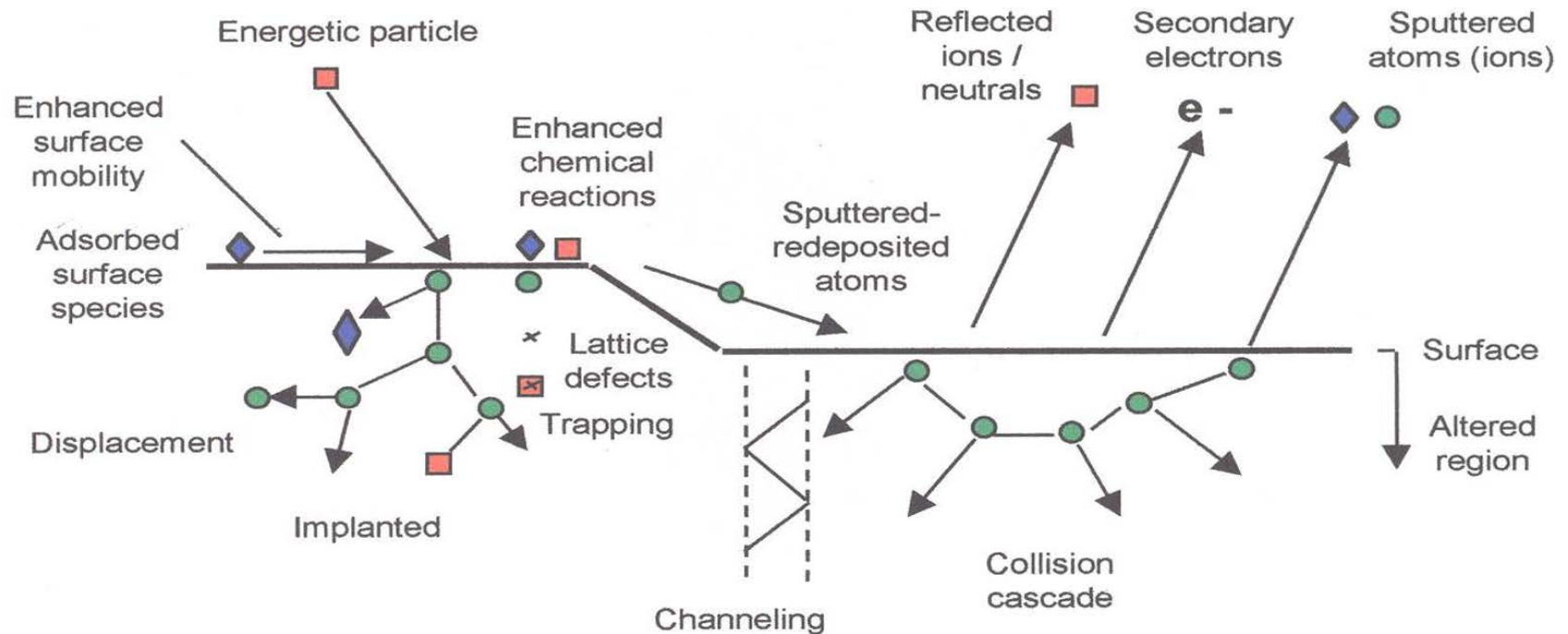
Reactive sputtering

Microstructural evolution during the film growth – Structure zone model

Plasma diagnostics

Plasma-surface interactions : Ions

Energetic ion bombardment effect at the surface:
sputtering, ion-assisted growth



Ion-surface interactions – Sticking probability

Ion beam originating from a plasma

Effects:

- reflection
- adsorption
- diffusion
- sputtering
- incorporation
- surface heating
- chemical reaction
- atom mixing
- change of topography (roughness)

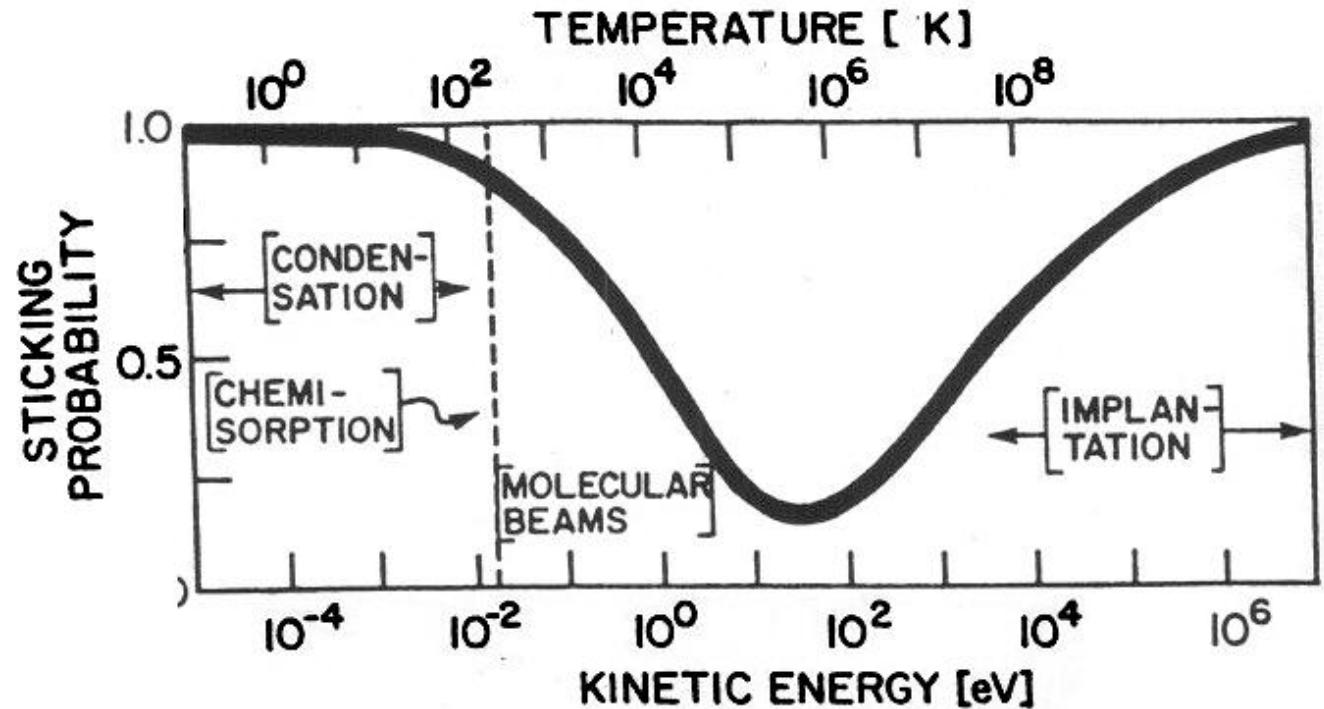


Figure 4-10 Particle-sticking probability as a function of energy. The dashed vertical line corresponds to room-temperature thermal energy. (From S. R. Kasi, H. Kang, C. S. Sass, and J. W. Rabalais, *Surface Science Reports* 10, Nos. 1/2, p. 1 (1989). Reprinted with the permission of Elsevier Science Publishers and Professor J. W. Rabalais.)

Sputtering

Basic effects:

- a) "knock-on"
- b) linear cascade
- c) thermal spike

E_{th} – threshold energy
 U_s – binding energy
 (heat of sublimation)
 2-5 eV

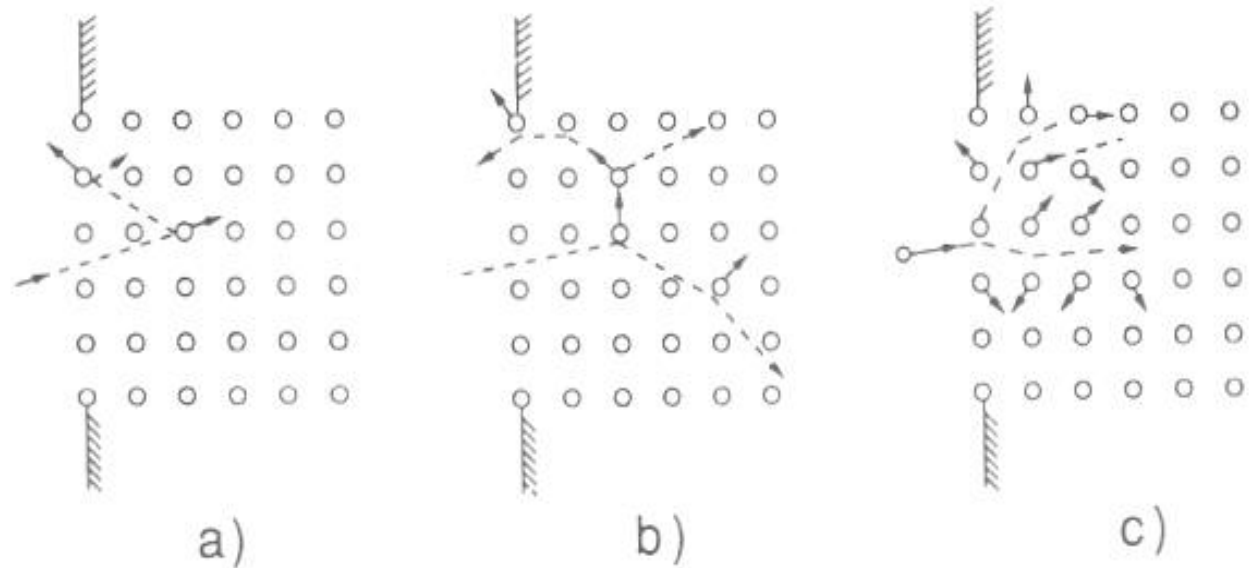


Figure 4-11 Three energy regimes of sputtering. (a) Single knock-on (low energy), (b) linear cascade, (c) spike (high energy). (After P. Sigmund.)



Linear cascade

Sputtering yield

$$S = \frac{3\alpha 4M_1M_2E}{4\pi^2(M_1 + M_2)^2U_s} \quad (E < 1 \text{ keV})$$

$$S = 0.042\alpha S_n(E)/U_s$$

α – efficiency of the mechanical momentum transfer

S_n – Stopping power: energy loss per unit length

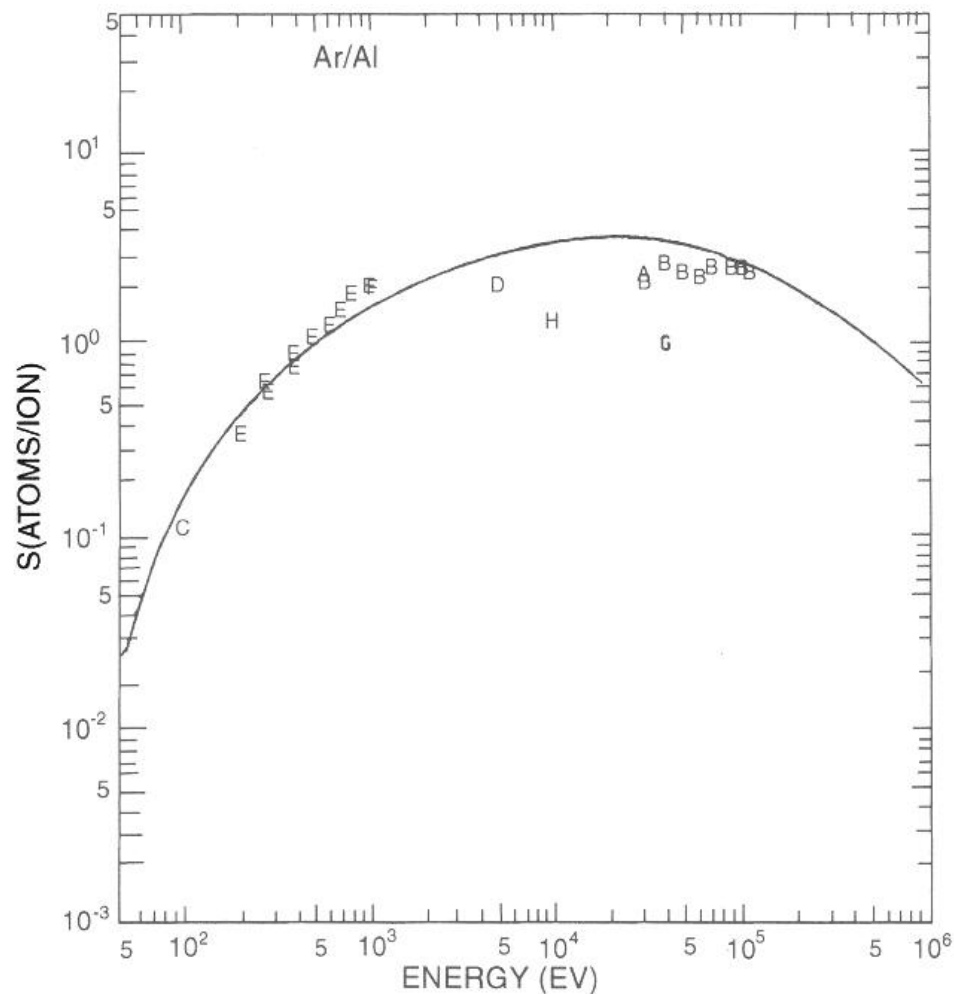


Figure 4-12 Sputter-yield values for Al as a function of energy. Letters on the plot refer to data from the following investigators: A. Yonts, Normand, and Harrison (1960); B. Fert, Colombie, and Fagot (1961); C. Laegreid and Wehner (1961); D. Robinson and Southern (1967); E. Weijnsfeld (1967); F. Oechsner (1973); G. Braun, Emmoth, and Buchta (1976); H. Okajima (1981). (From N. Matsunami, *et al.*, *AT. Data. Nucl. Data Tables* 31, 1 (1984). Reprinted with the permission of Academic Press, Inc.)

Table 4-2

Sputtering Yield Data for Metals (Atoms/Ion) and Semiconductors (Molecules/Ion)

Sputtering gas energy (keV) →	He 0.5	Ne 0.5	Ar 0.5	Kr 0.5	Xe 0.5	Ar 1.0	Ar threshold voltage (eV)
Ag	0.20	1.77	3.12	3.27	3.32	3.8	15
Al	0.16	0.73	1.05	0.96	0.82	1.0	13
Au	0.07	1.08	2.40	3.06	3.01	3.6	20
C	0.07	—	0.12	0.13	0.17		
Co	0.13	0.90	1.22	1.08	1.08		25
Cu	0.24	1.80	2.35	2.35	2.05	2.85	17
Fe	0.15	0.88	1.10	1.07	1.0	1.3	20
Ge	0.08	0.68	1.1	1.12	1.04		25
Mo	0.03	0.48	0.80	0.87	0.87	1.13	24
Ni	0.16	1.10	1.45	1.30	1.22	2.2	21
Pt	0.03	0.63	1.40	1.82	1.93		25
Si	0.13	0.48	0.50	0.50	0.42	0.6	
Ta	0.01	0.28	0.57	0.87	0.88		26
Ti	0.07	0.43	0.51	0.48	0.43		20
W	0.01	0.28	0.57	0.91	1.01		33
GaAs		0.10	0.83			1.52	20–25
InP			1.00			1.4	25
GaP			0.87				36
SiC		0.13	0.40				17
InSb			0.50				

From Refs. 4 and 6. Compound semiconductor data for normal ion incidence (Ref. 11).

Sputtering yield

S = number of atoms
per incident particle



Effet of the fabrication conditions on sputtering

Deposition rate

$$\dot{G} \left(\frac{\text{cm}}{\text{s}} \right) \approx \frac{\bar{P}_d \langle x_{th} \rangle}{g\rho(1 + \gamma_e)E'}$$

P_d – power density

x_{th} – thermalisation length of the sputtered atoms

g – anode-cathode distance

ρ – density

γ_e – Townsend coefficient

E – sputtering energy

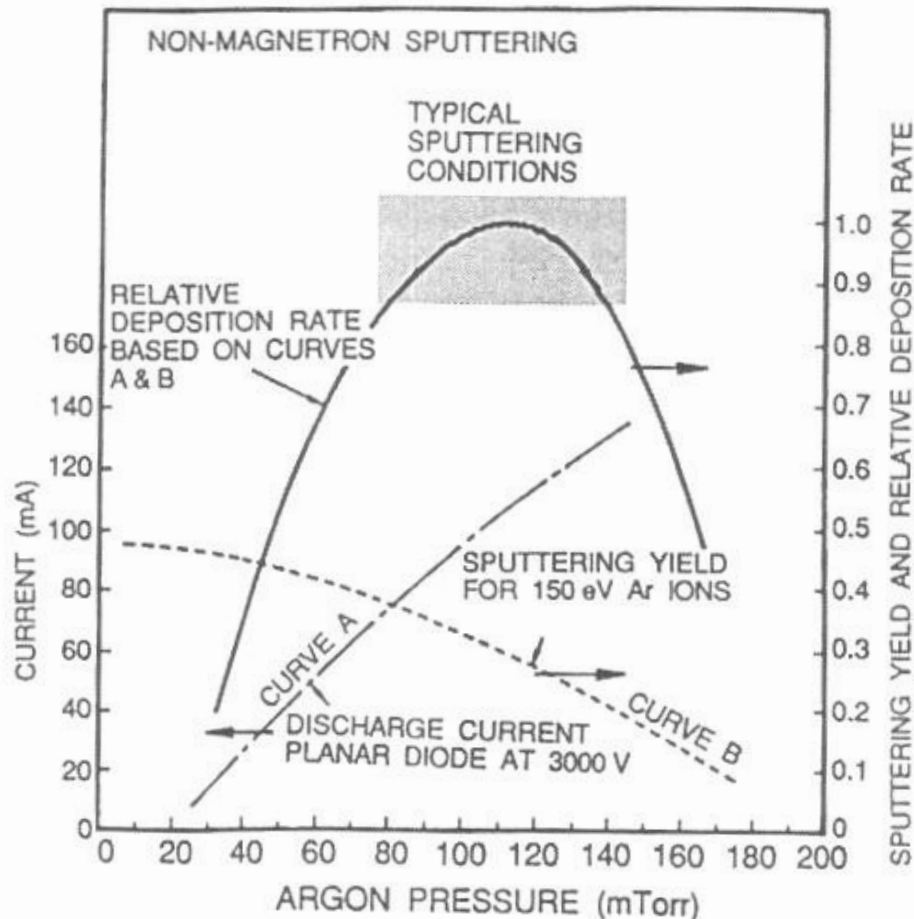


Figure 5-2 Influence of working pressure and current on film deposition rates in nonmagnetron sputtering. (From Ref. 3.)

DC and RF systems (capacitive coupling) - Sputtering

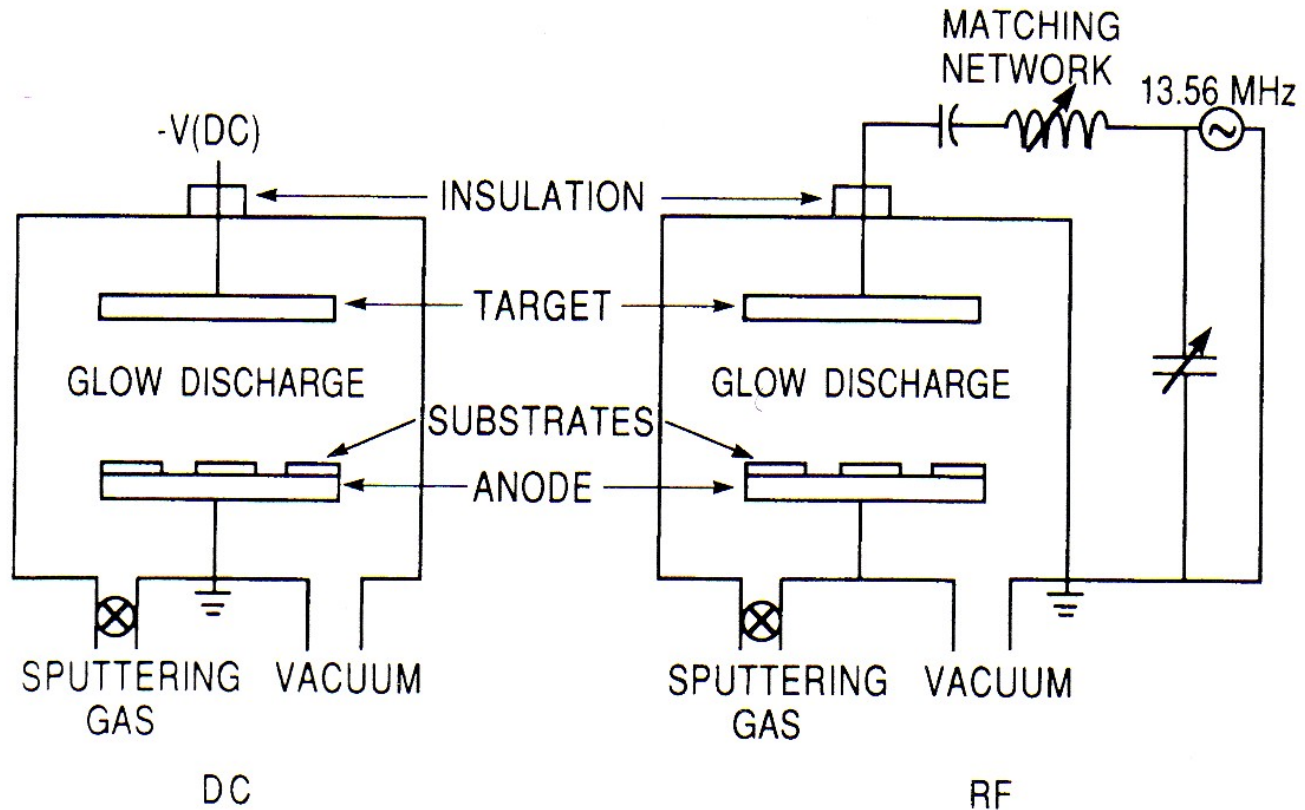


Figure 4-1 Schematics of simplified sputtering systems: (a) DC, (b) RF.



Reactive sputtering

Hysteresis effect

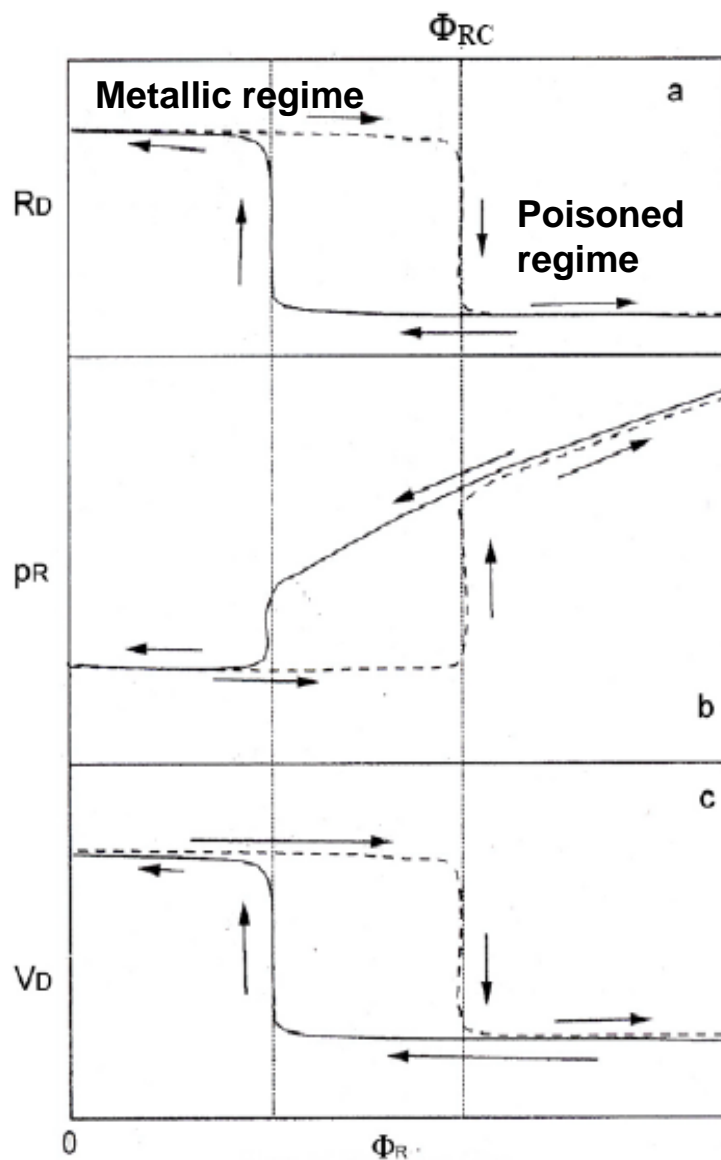
Φ_R : reactive gas flow

1. Oxides (oxygen) — Al_2O_3 , In_2O_3 , SnO_2 , SiO_2 , Ta_2O_5 .
2. Nitrides (nitrogen, ammonia) — TaN , TiN , AlN , Si_3N_4 , CN
3. Carbides (methane, acetylene, propane) — TiC , WC , SiC .
4. Sulfides (H_2S) — CdS , CuS , ZnS .
5. Oxycarbides and oxynitrides of Ti, Ta, Al, and Si.

Deposition rate: R_D

Reactive gas
partial pressure: p_R

Cathode voltage: V_D



Evolution of R_D (a), p_R (b) and V_D (c) as a function of the **reactive gas flow**.



Berg's model of reactive sputtering

Assumptions:

- a) Metal target – sputtering yield S_m
- b) Sputtering due to the inert gas
- c) Target compound - S_c
- d) Uniform current density at A_t
- e) Substrate surface - A_s
- f) Compound surface fraction - θ_t
- g) Compound surface fraction of the "substrate" - θ_s
- h) Sticking: α_t on the target (metal)
0 on the compound

Reactive gas flow toward all surfaces:

$$\Phi_r / N_A = P_R / (2\pi MRT)^{1/2}$$

S. Berg et al, Chapter A5.3 in *Handbook of Thin Film Process technology*, D.A. Glocker and S.I. Shah, eds., IoP, Bristol 1995

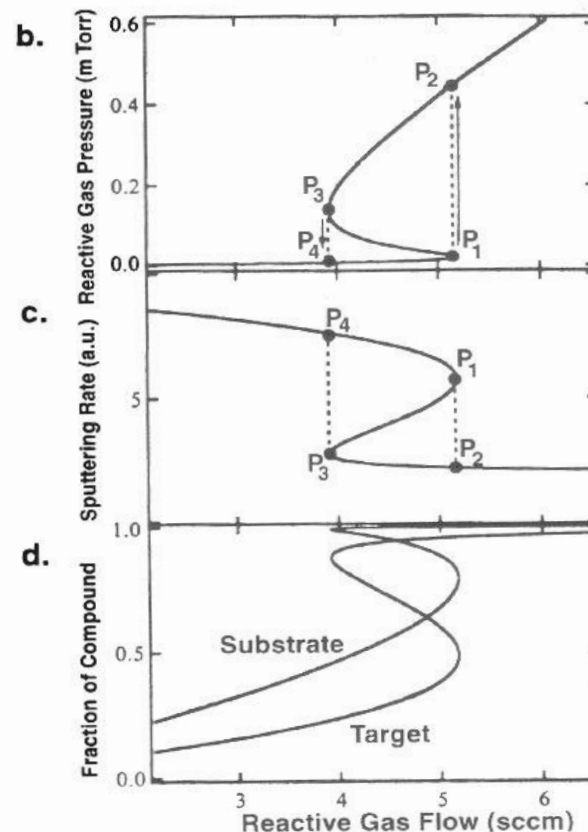
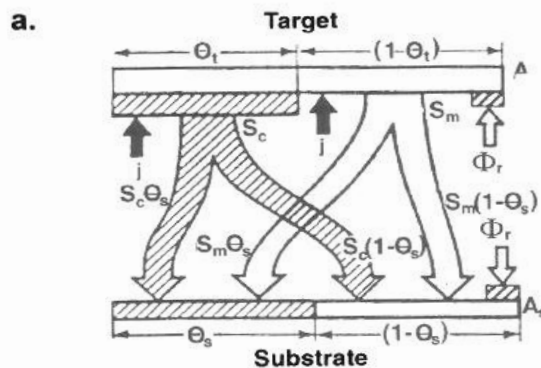


Figure 5-6 (a) Model of reactive sputtering. (b) Simulation of reactive gas pressure vs reactive gas flow. As Q increases, pressure values follow the path $P_1 \rightarrow P_2 \rightarrow P_3 \rightarrow P_4$, tracing out a hysteresis loop. (c) Simulated sputtering rate vs reactive gas flow rate. (d) Simulation of target and substrate composition as a function of reactive gas flow. (From S. Berg *et al.* in *Handbook of Thin Film Process Technology*, edited by D. A. Glocker and S. I. Shah, 1998. Reprinted with the permission of the Institute of Physics Publishing and the authors.)



Reactive sputtering effects

Target: Species formation rate =
 species sputtering rate:
 j Ar⁺ current density

$$\Phi_r \alpha_t (1 - \theta_t) A_t a = (j/q) \theta_t A_t S_c,$$

Target erosion rate:

$$R_t = (j/q) [S_c \theta_t + S_m (1 - \theta_t)] A_t$$

Equilibrium of the arrival rates :

1. Sputtering rate, deposition rate on the metal and on the substrate;

1

2

3

α_s – gas sticking coefficient

$$(j/q) [S_c \theta_t A_t] (1 - \theta_s) + \Phi_r \alpha_s (1 - \theta_s) A_s b = (j/q) [S_m (1 - \theta_t) A_t] \theta_s / b$$

2. Metal reaction with the reactive gas

3. Metal sputtered from the target

Gas phase equilibrium:

$$Q = Q_t + Q_s + Q_p,$$

Reaction on the target: $Q_t = \Phi_r \alpha_t (1 - \theta_t) A_t$

Reaction on the substrate: $Q_s = \Phi_r \alpha_s (1 - \theta_s) A_s$

Pumped flux, S – pumping speed: $Q_p = P_r S$

Effet of reactive gas on the deposition rate: stoichiometry and properties

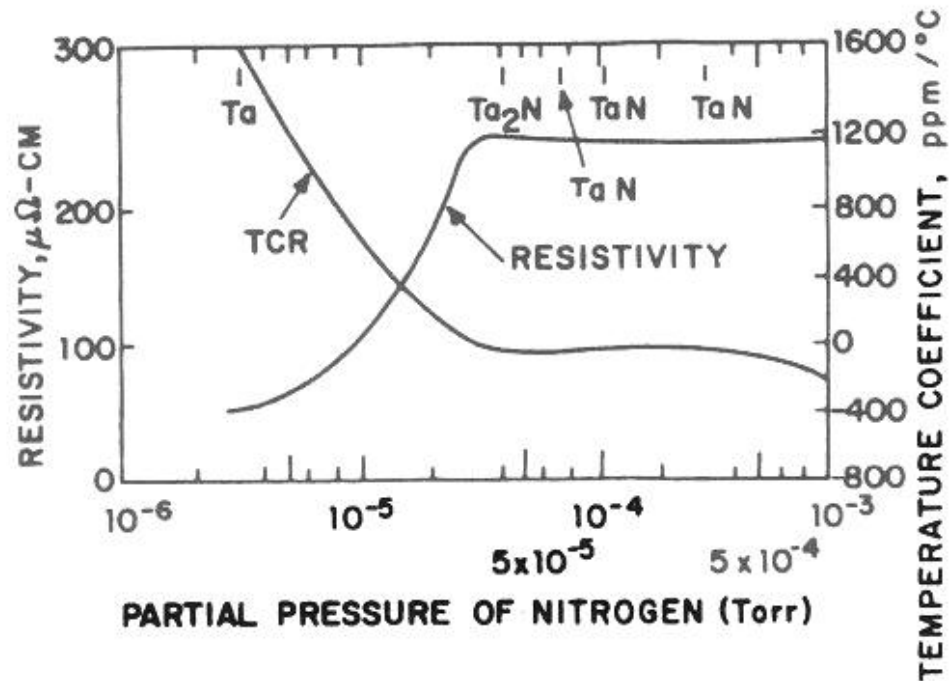
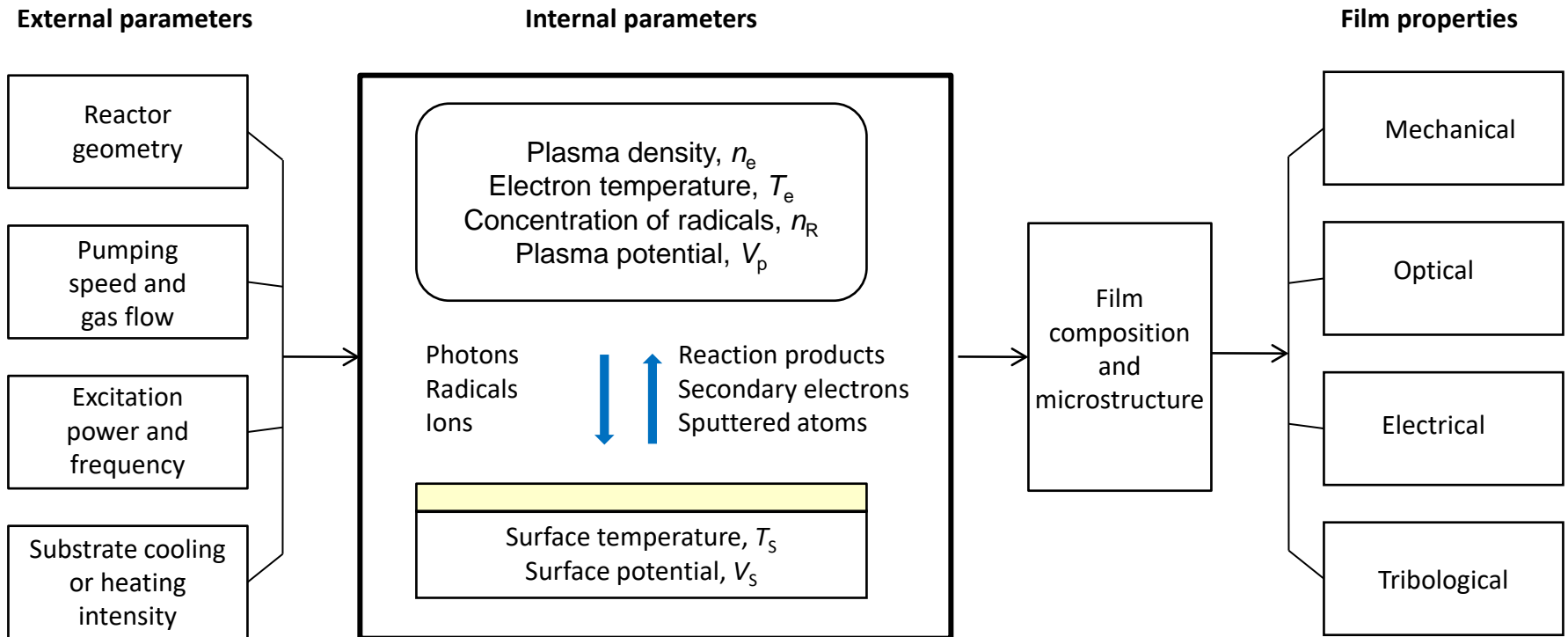


Figure 5-7 Influence of nitrogen on composition, electrical resistivity, and temperature coefficient of resistivity of reactively sputtered Ta films. (From Ref. 19.)

TaN – resistance in electric circuits;

DC sputtering at 3 - 5 kV, thermal coeff. of resistivity: $\rho = \rho_0(1 + \alpha T)$

Plasma system and process control



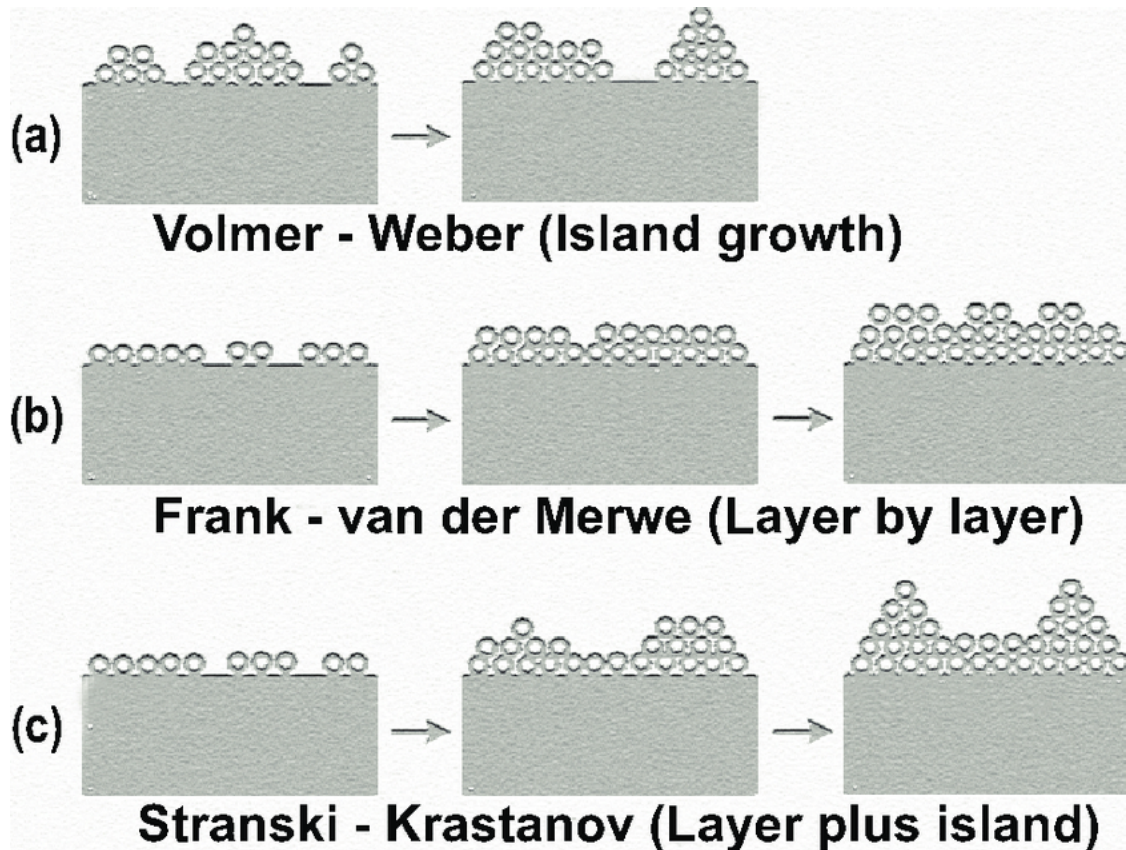
Today:

Reactive sputtering

Microstructural evolution during the film growth – Structure zone model

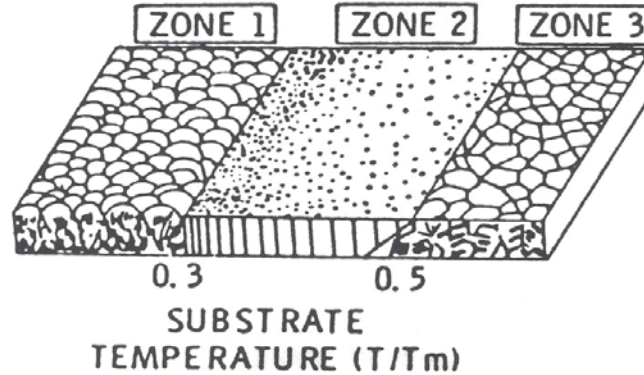
Plasma diagnostics

Thin film growth models

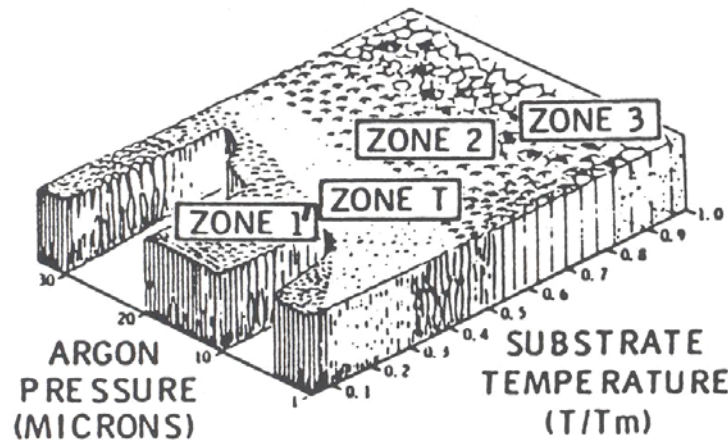




Structure zone model - SZM

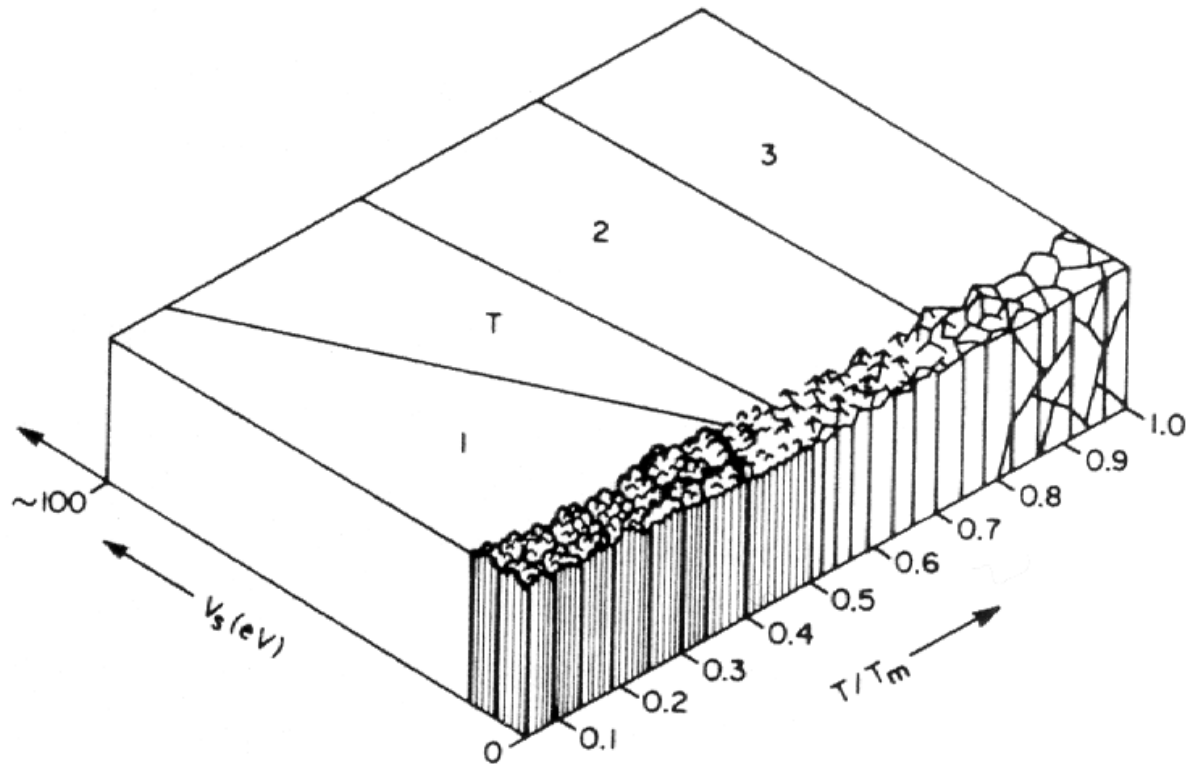


B.A. Movchan and A.V. Demchishin, *Fiz. Metal. Metalloved.*, 28 (1969) 653.



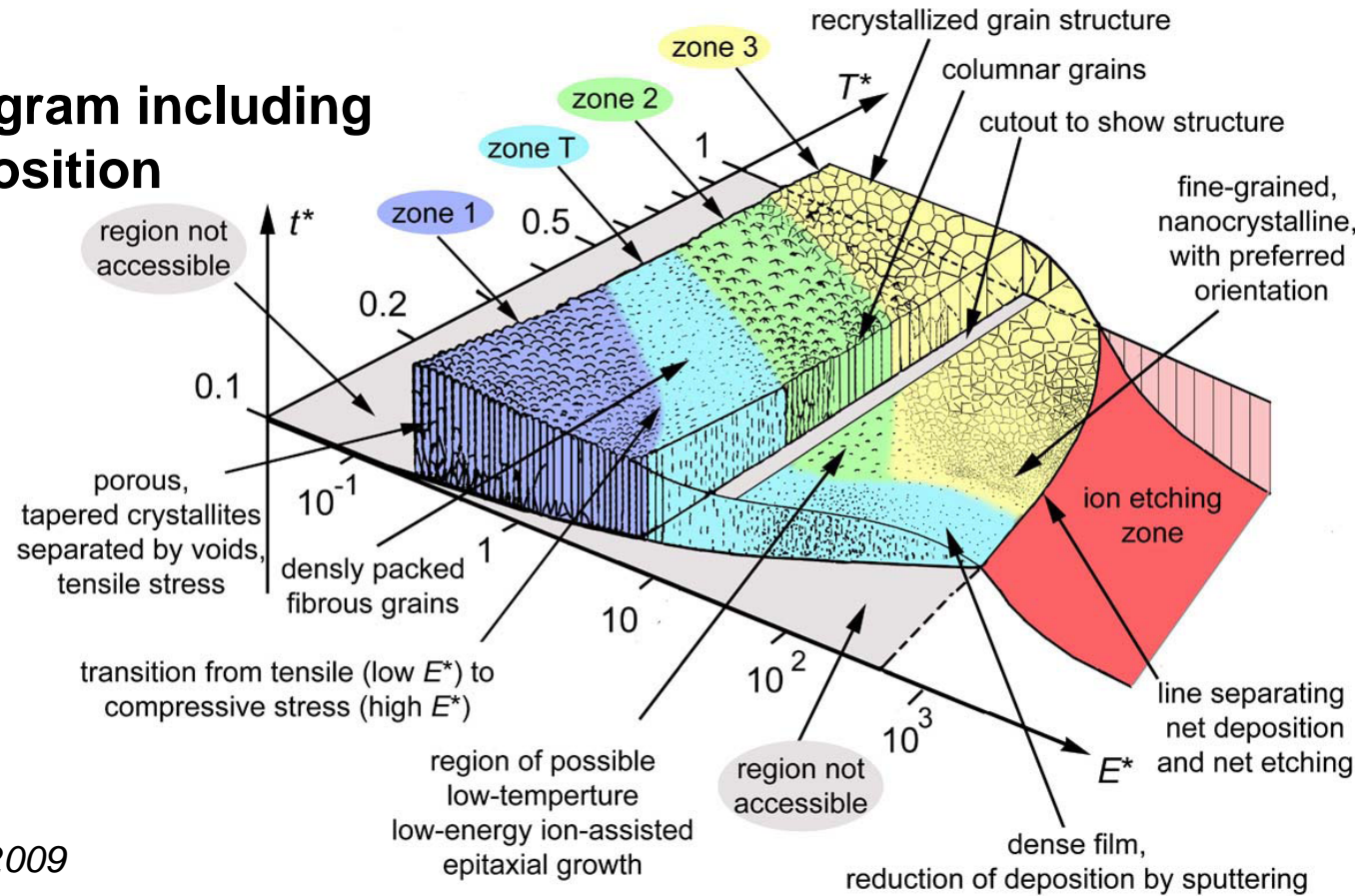
J.A. Thornton, *J. Vac. Sci. Technol.*, 11 (1974) 666.

Microstructural evolution according to the SZM



Messier, Giri, and Roy [Messier, 1984];

Structure zone diagram including plasma based deposition and ion etching



A. Anders, *Thin Solid Films*, 2009

- (I) The linear axis is replaced with a generalized temperature, which includes the homologous temperature plus a temperature shift caused by the *kinetic energy of particles arriving on the surface*.
- (II) The linear pressure axis is replaced with a logarithmic axis for a normalized energy, describing displacement and heating effects caused by the *kinetic energy of bombarding particles*.
- (III) The until now unlabeled z-axis is replaced with a net film thickness, which allows one to illustrate film structure, thickness reduction by densification/sputtering, and “negative thickness” (ion etching).

Growth control by the ion bombardment energetics

1. Ion bombardment effects

$E_p \sim E_i \cdot \Phi_i / \Phi_n$ - energy per deposited particle

$E_i < 1$ keV, IEDF, Φ_i ion flux, Φ_n flux of the condensing particles, SZM

Control of E_i and Φ_i / Φ_n :

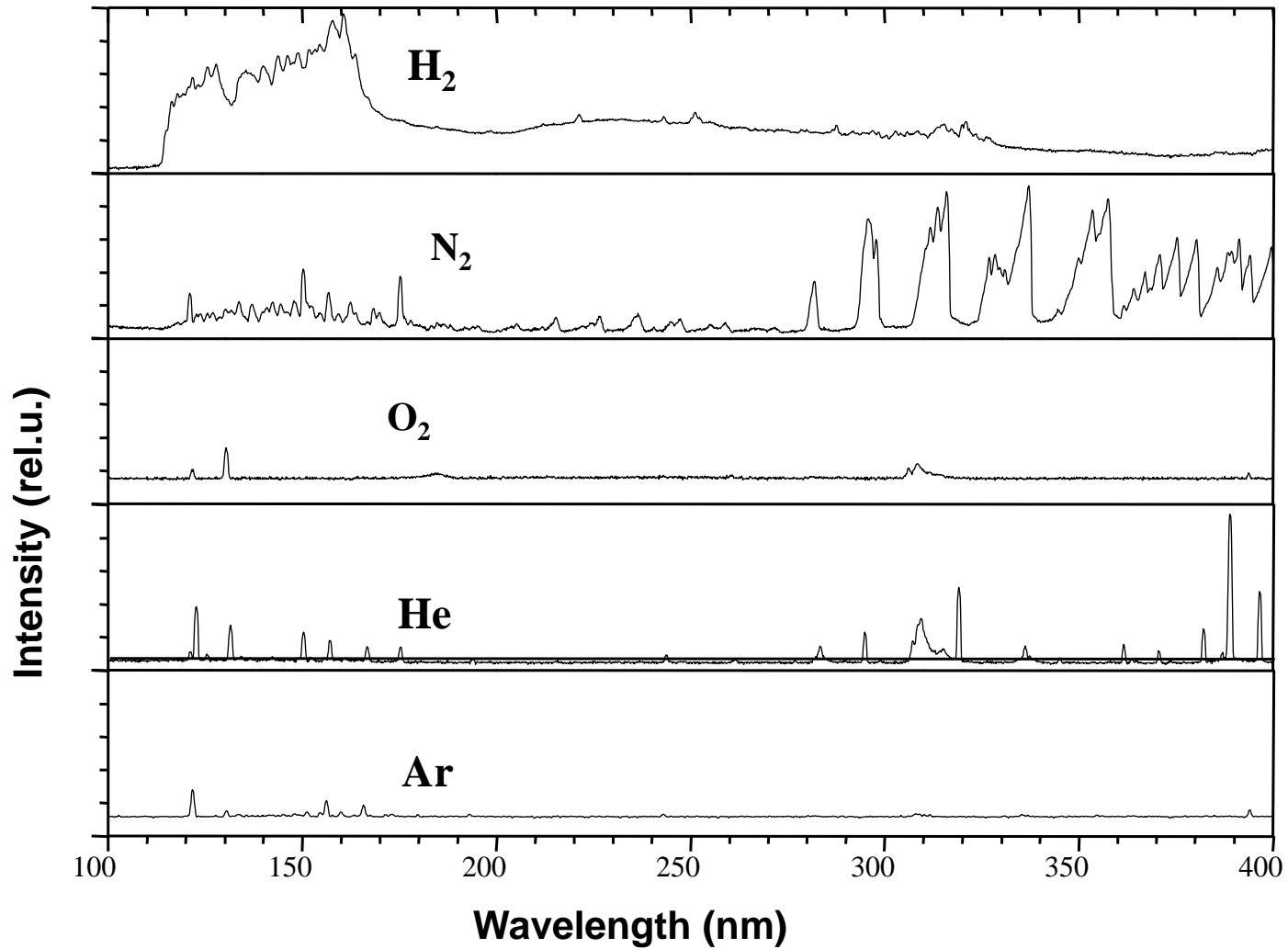
- Surface biasing
- Unbalanced magnetrons
- Gas phase ionization (plasma assistance)
- Ionization / biasing (IBAD, PA-EBE, ECR, PECVD, MW/RF)
- Pulsed plasma (HiPIMS)

$$\Phi_N = r_D \frac{\rho N_A}{m_A}$$

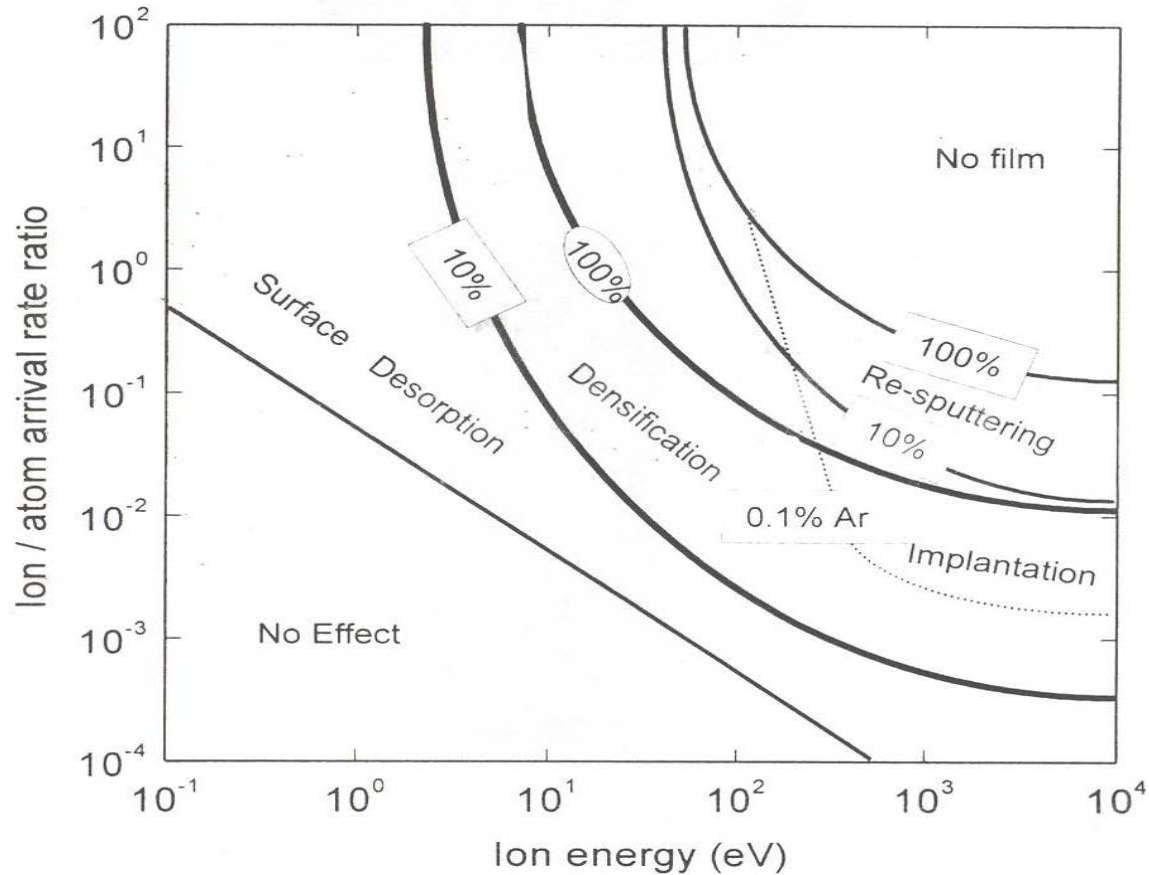
2. UV and VUV radiation

- Strong radiation below $\lambda = 200$ nm
- Polymer crosslinking, surface volatilization

Vacuum ultraviolet (VUV) spectra

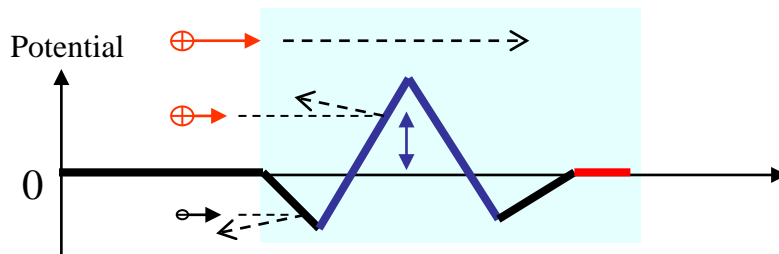
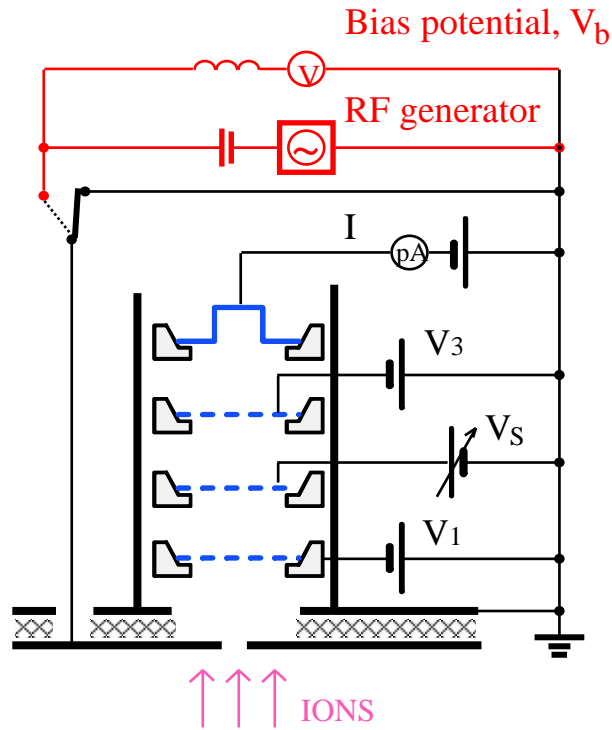


Critical ion energy and ion flux

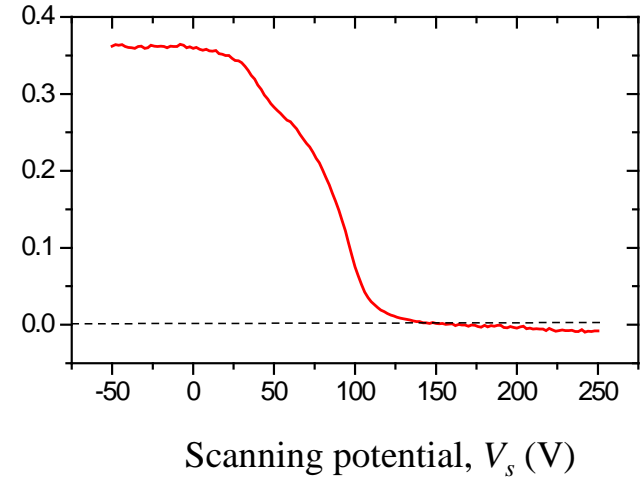


(After Ref. [Roy89], adapted from Ref.[Harper84] for IAD of metals).

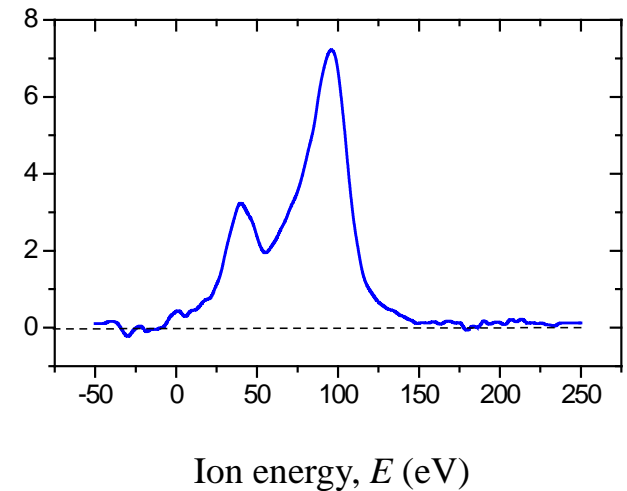
Multi-grid ion energy analyser



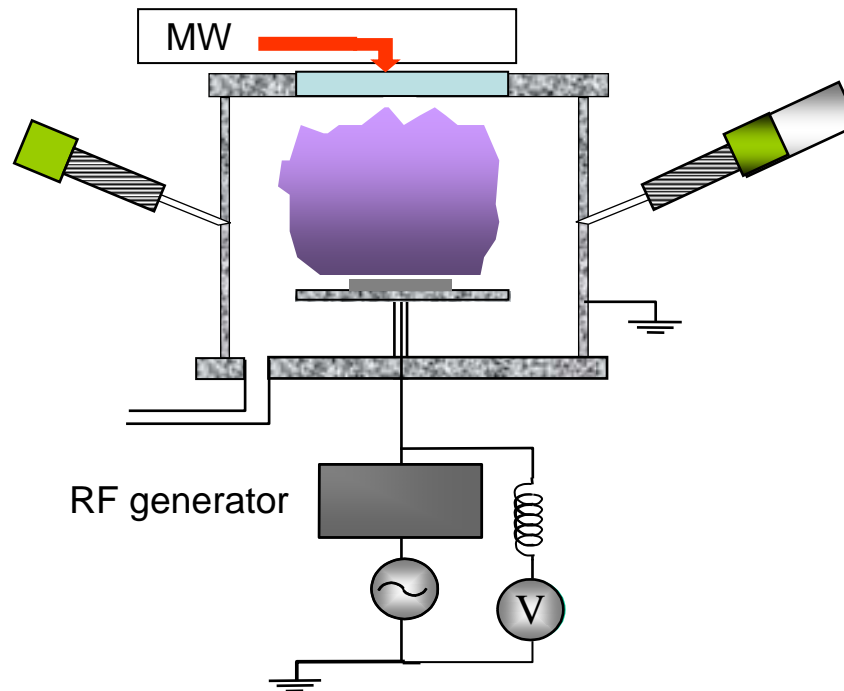
Collector
current, I
(μA)



IEDF, $f_i(E)$
(nA/V)

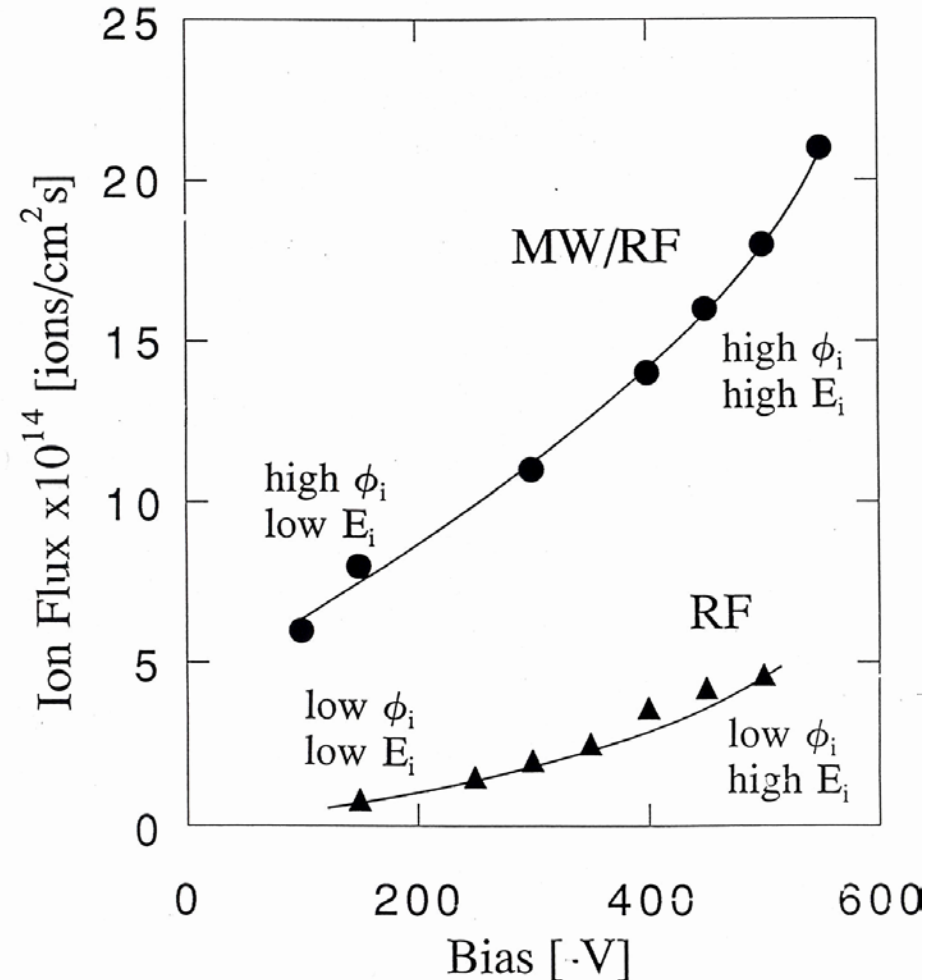


PECVD in the dual-frequency MW/RF discharge



- Principal microwave (2.45 GHz) plasma
- RF (13.56 MHz) radiofrequency applied to the substrate holder - V_B

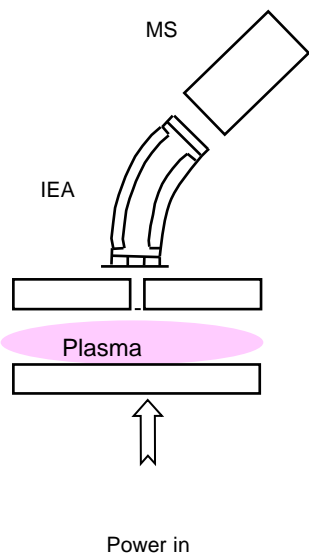
MW/RF discharge: Ion flux vs. bias voltage in CH₄



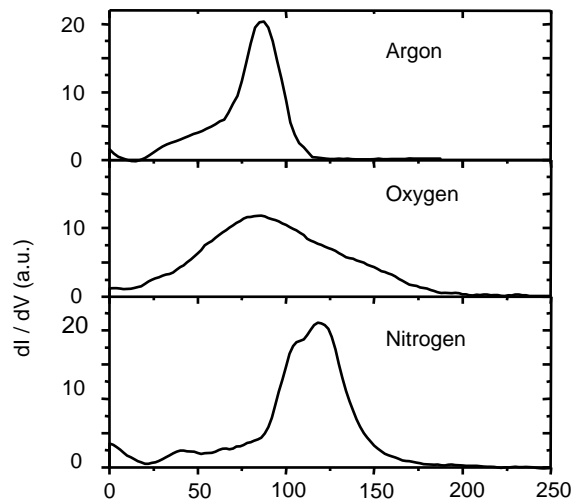
L. Martinu et al., *J. Vac. Sci. Technol. A*,
12 (1994) 1360



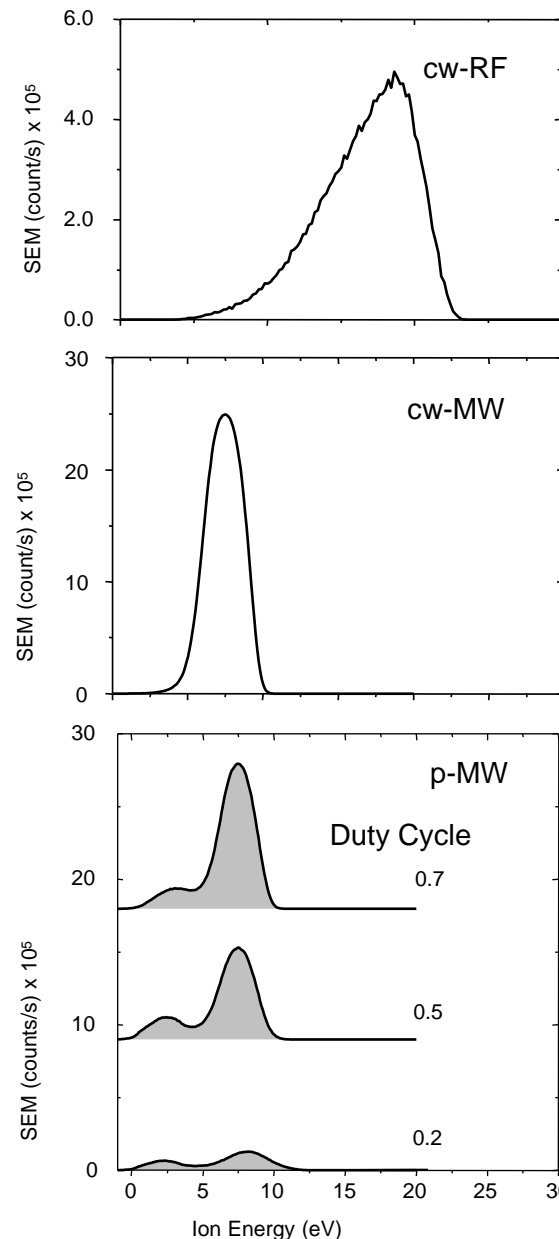
Ion energy distributions, IED



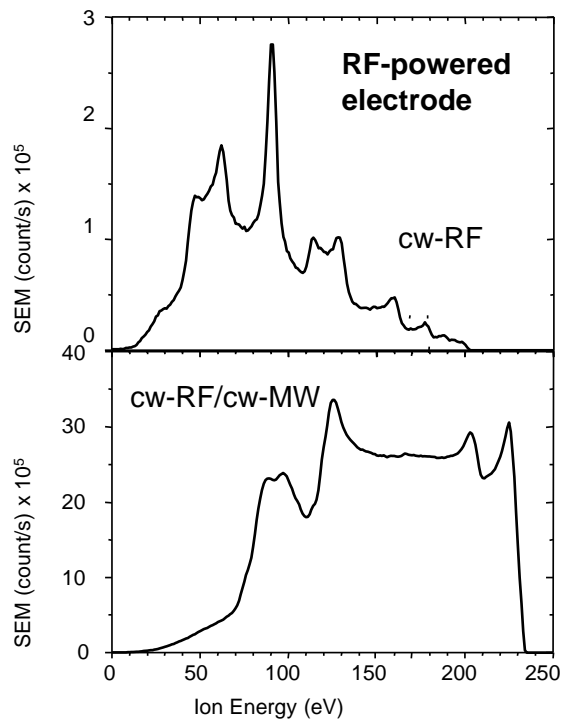
Ion assisted evaporation



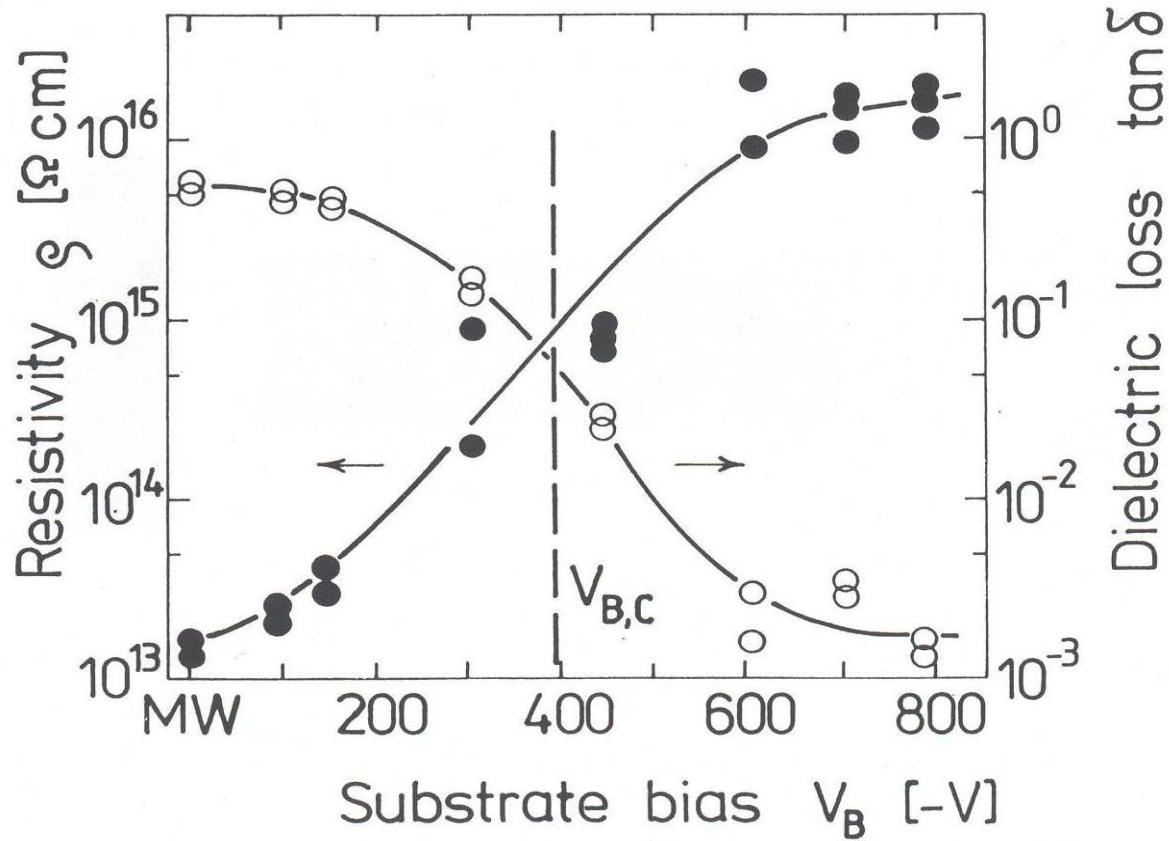
Grounded electrode



RF-powered electrode

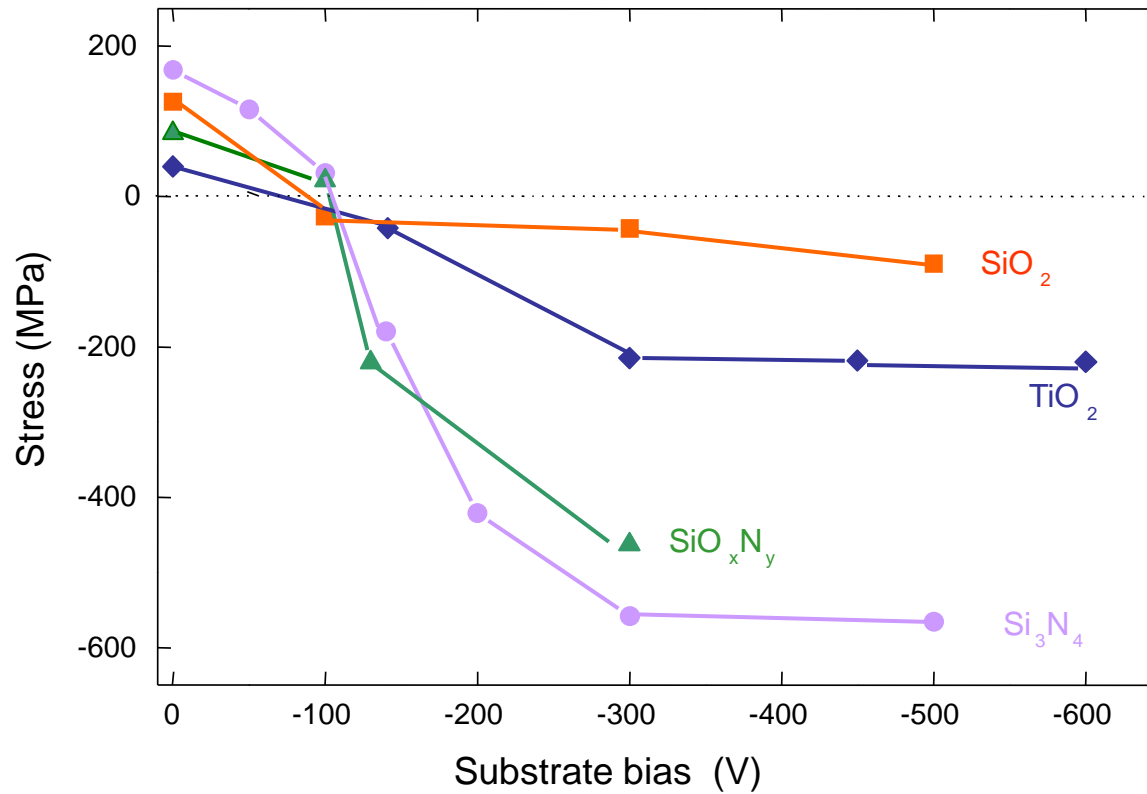


Effet of ion bombardment in Si_3N_4

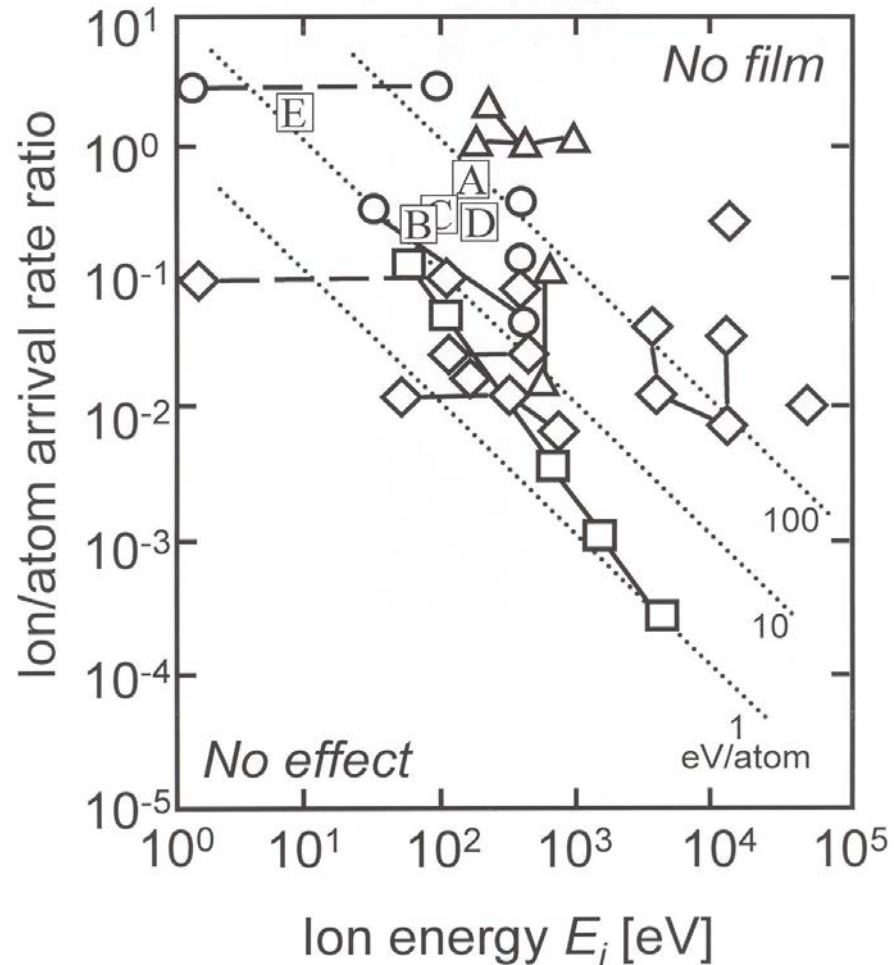


Critical ion energy - E_c

Mechanical stress in PECVD films



Critical ion energy and ion flux

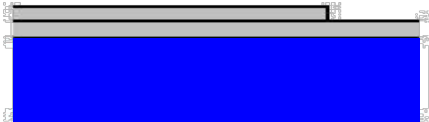


L. Martinu et al., *J. Vac. Sci. Technol. A*,
12 (1994) 1360

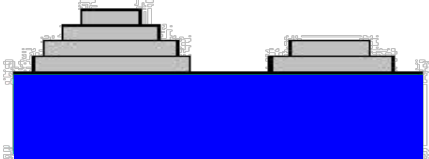
A: $\text{SiN}_{1.3}$; B: SiO_2 ; C: a-C:H; D: TiO_2 (MW/RF); E: TiO_2 (PICVD)
and different PVD dielectrics, metals and semiconductors

Ion bombardment and thin film growth

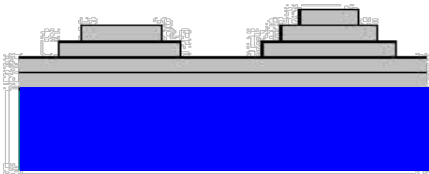
Layer-by-layer (Franck-van der Merwe)



Island (Vollmer-Weber)

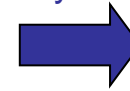


Mixed (Stranski-Krastanov)



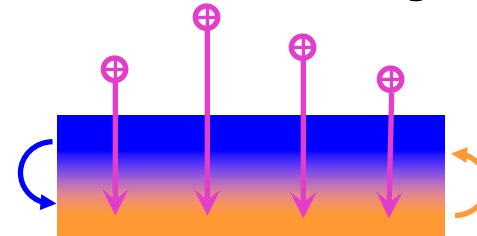
Surface effects

Enhanced surface mobility
Island dissolution
Surface defects
Surface activation



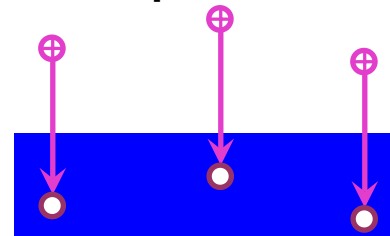
Homogeneous nucleation
Early coalescence
Surface morphology
Compound formation

Interface mixing



Subplantation

Lifshitz *et al.* PRL 62 (1989) 1290.

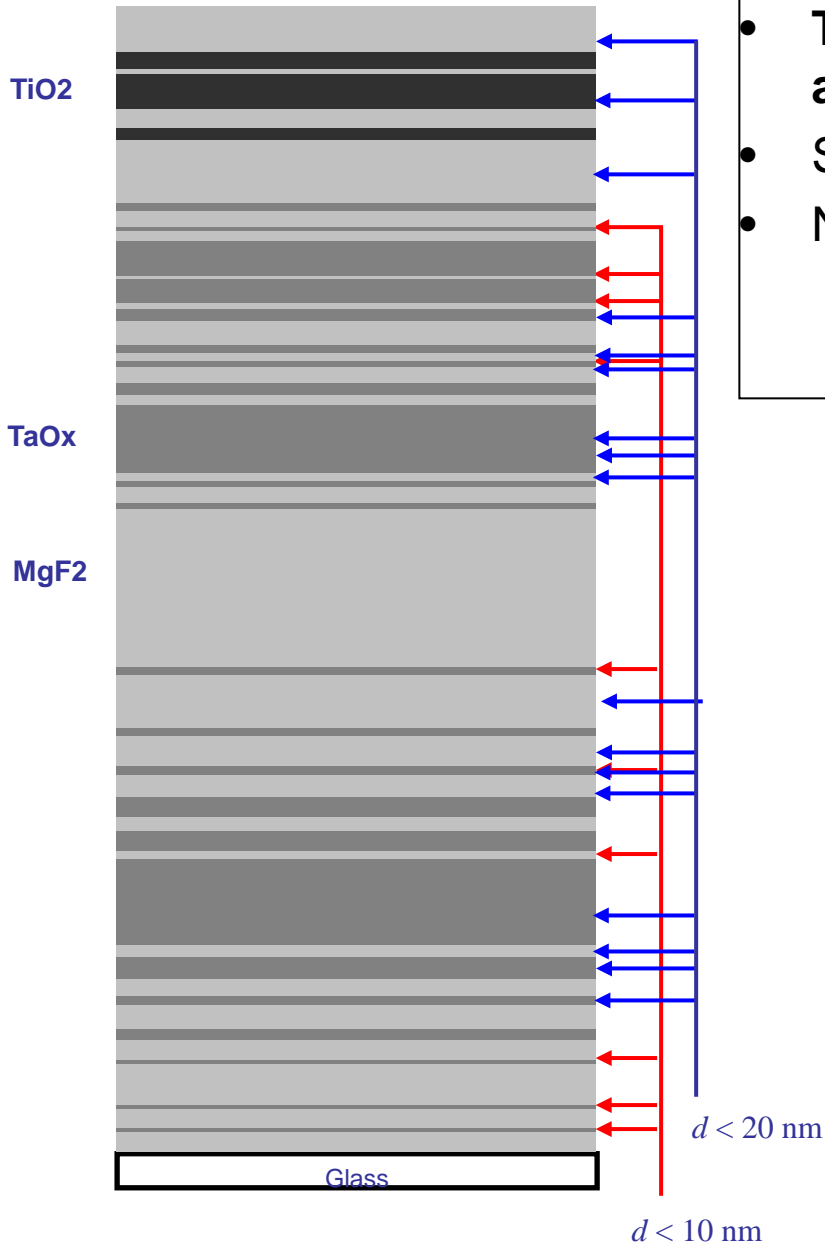


Growth below surface:

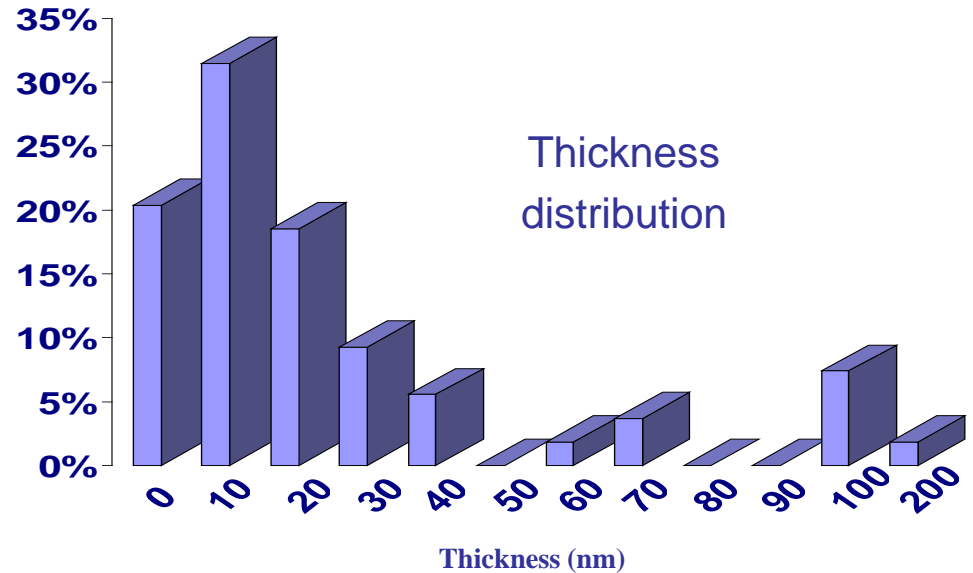
- Film-forming ions
- Film densification
- Stress formation

Ion bombardment effects in a plasma environment: sub-surface transport and its effects.

Complex optical interference filters



- Today's advanced optical interference filters are synthesized, not designed
- Synthesis techniques: Flip-Flop and Needle
- New challenges on films and processes:
 - Ultra-thin films with abrupt interfaces
 - Non quarter-wave films require control



- **53 layer broad-band AR coating** for photographic lens synthesized by Flip-Flop method
- Berlin '91 design contest winner: W. H. Southwell

Initial growth of TiO_2 on SiO_2 : *In situ* RTSE

Addition of TiCl_4 to O_2

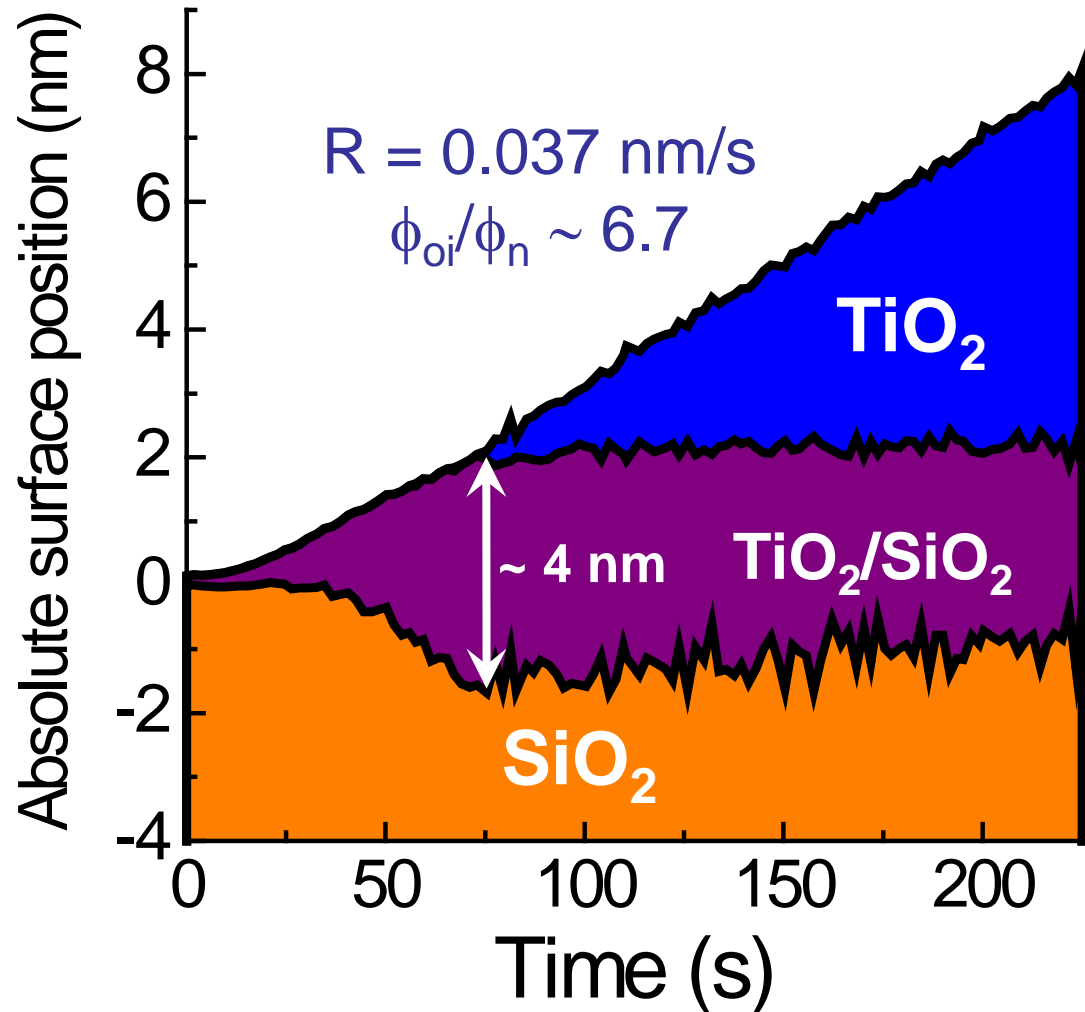
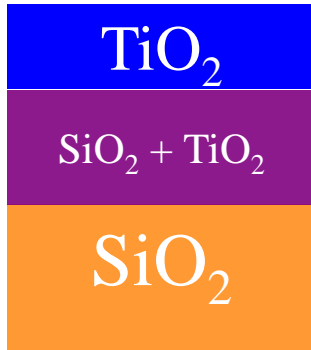
PECVD Deposition

$V_B = -450 \text{ V}$
in $\text{O}_2 + \text{TiCl}_4$
 $P_{\text{TiCl}_4}/P_{\text{O}_2} = 0.005$

Ion Bombardment

$E_{\text{max}} \sim 480 \text{ eV}$
 $E_m \sim 150 \text{ eV}$

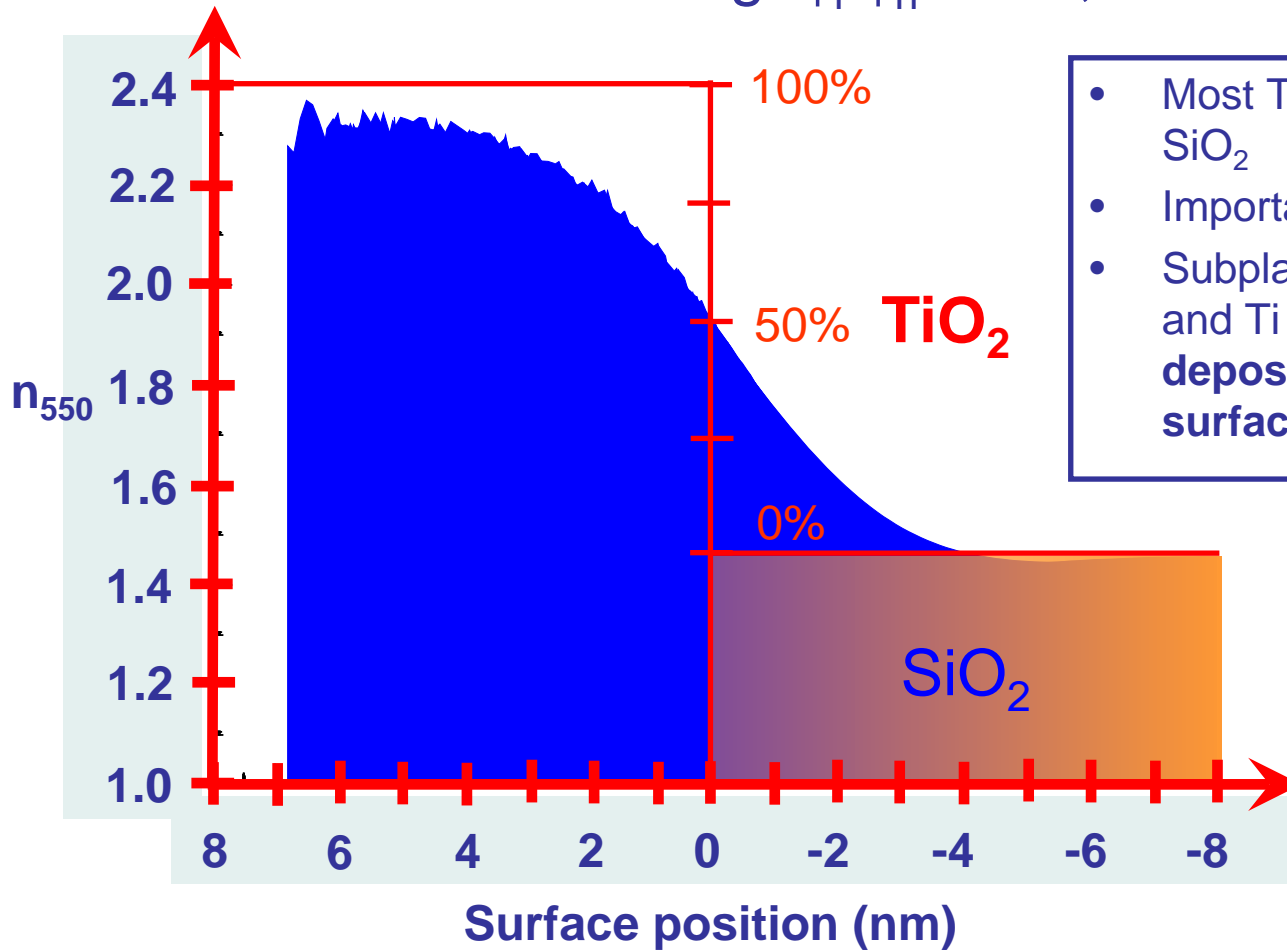
Optical model



- Interface broadening during initial growth => steady state thickness
- We want to understand interface formation and to control it!

Interface broadening: TRIDYN simulation

Interface Mixing: $\phi_i/\phi_n \sim 6.3$; $R = 0.04$ nm/s



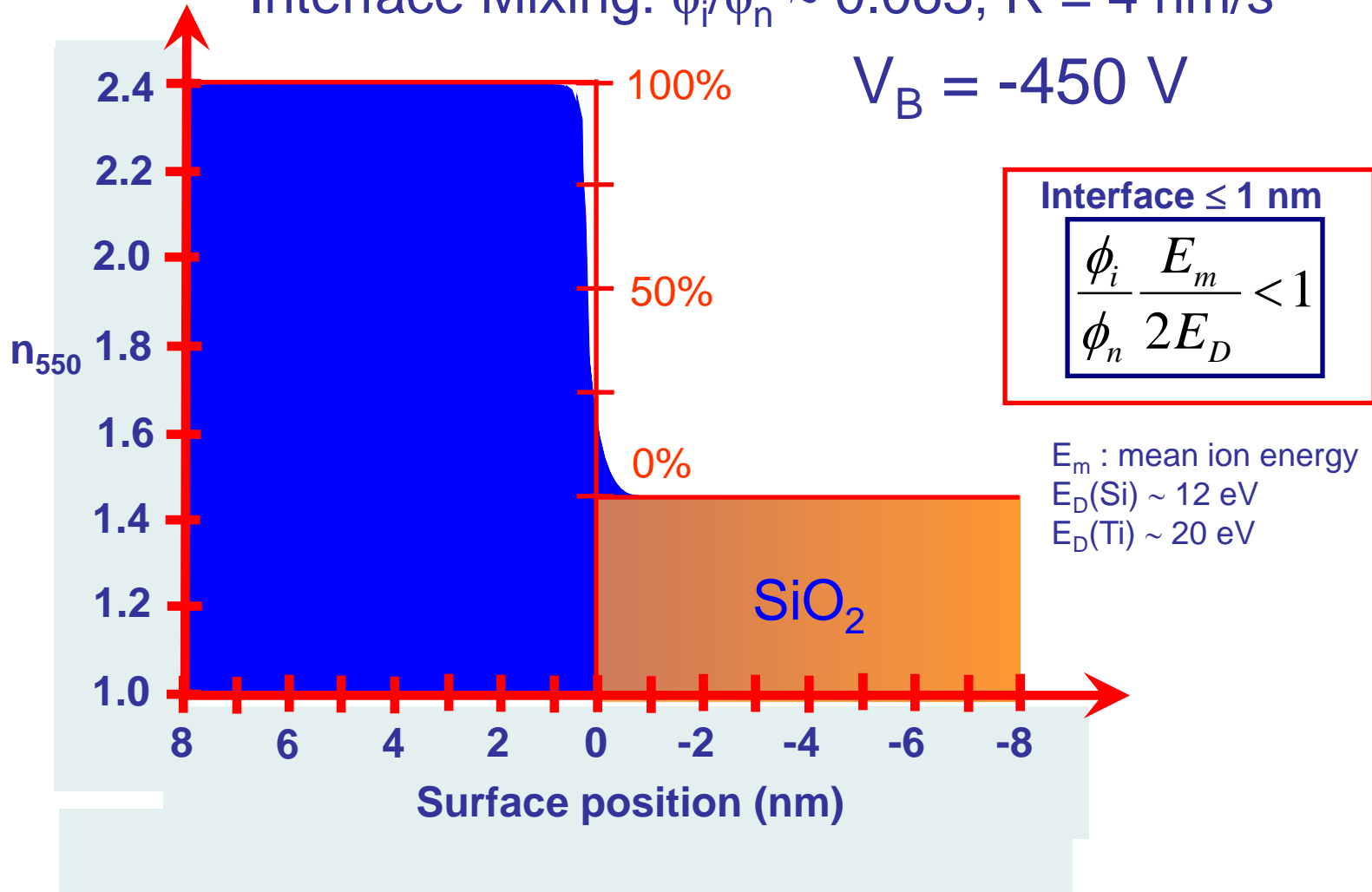
- Most Ti atoms are knocked into SiO_2
- Important ion mixing
- Subplantation of O from plasma and Ti from surface \Rightarrow film deposited below growth surface

We must increase Ti flux (r_D)!

Interface broadening: TRIDYN simulations

Interface Mixing: $\phi_i/\phi_n \sim 0.063$; $R = 4 \text{ nm/s}$

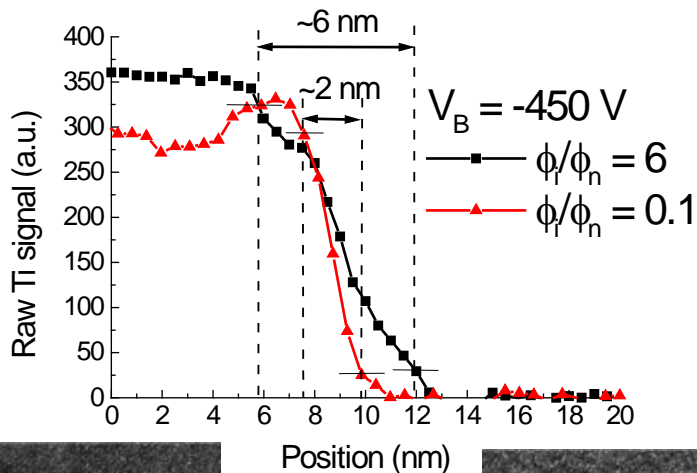
$V_B = -450 \text{ V}$



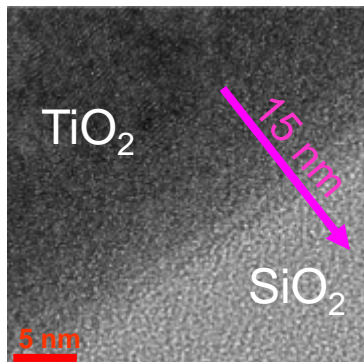


Interface broadening: HRTEM, comparison with simulation

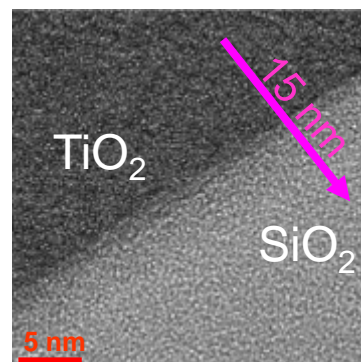
EELS
Ti signal



HRTEM

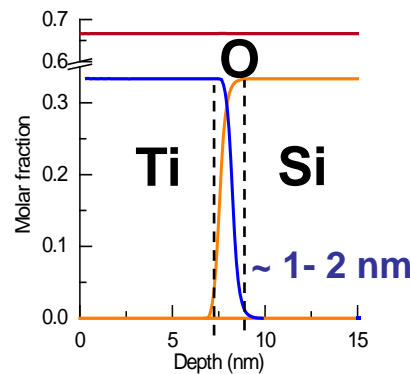
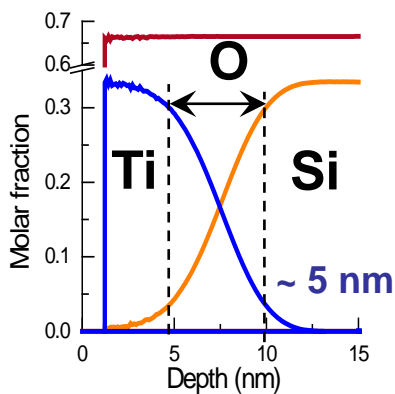


$\phi_i/\phi_n = 6$



$\phi_i/\phi_n = 0.1$

TRIDYN





Interface engineering of Si nitrides – MW/RF plasma

- **PECVD deposition system**

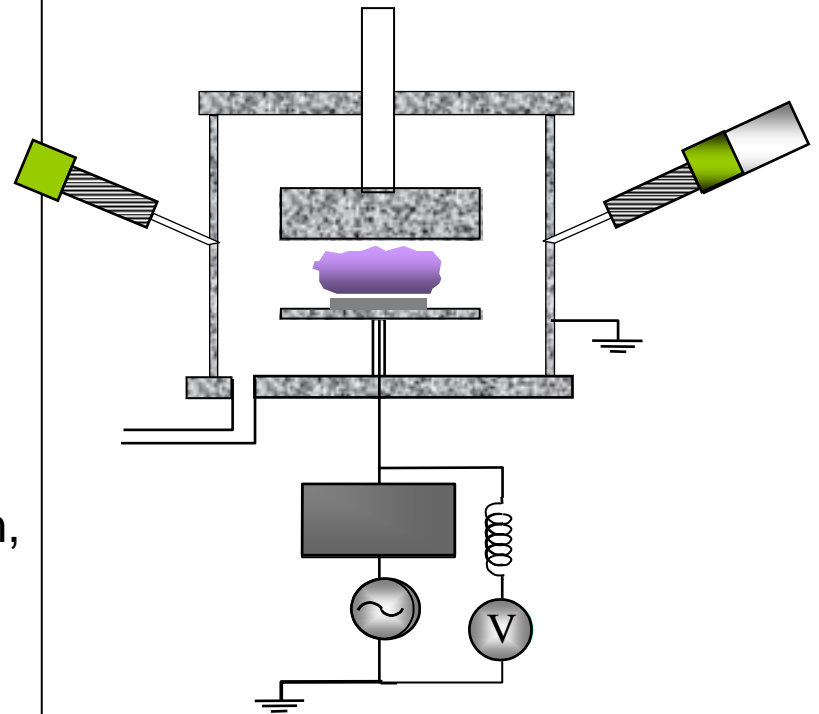
- Gas mixtures: SiH_4 , N_2 , Ar
- Pressure: 20-200 mTorr
- RF and MW power levels: ≈ 100 W
- Substrate bias: $\sim 0 - 800$ V

- ***In-situ* spectro-ellipsometry**

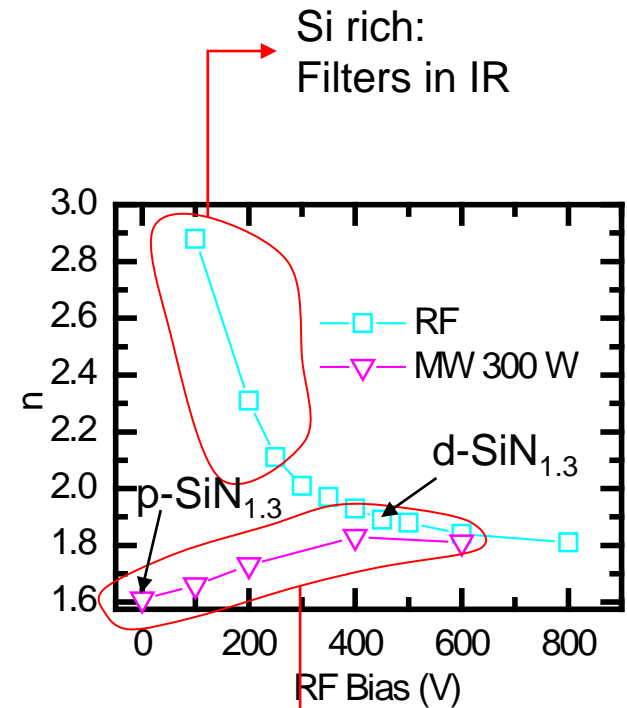
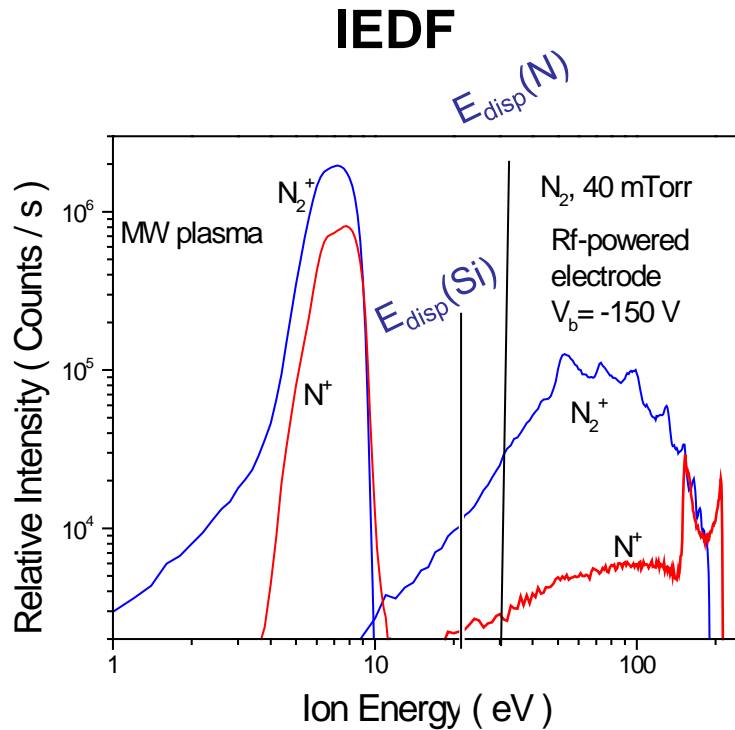
- Dynamic Monte Carlo simulations
- SRIM: www.srim.org
- A. Amassian, JAP, 2006

- ***Ex-situ* characterization:**

- UV-VIS-NIR-IR VASE: 260 nm – 33 μm , Spectrophotometry
- FTIR, XPS, XRD, AFM, ERD-TOF



Ion bombardment and properties of Si_3N_4



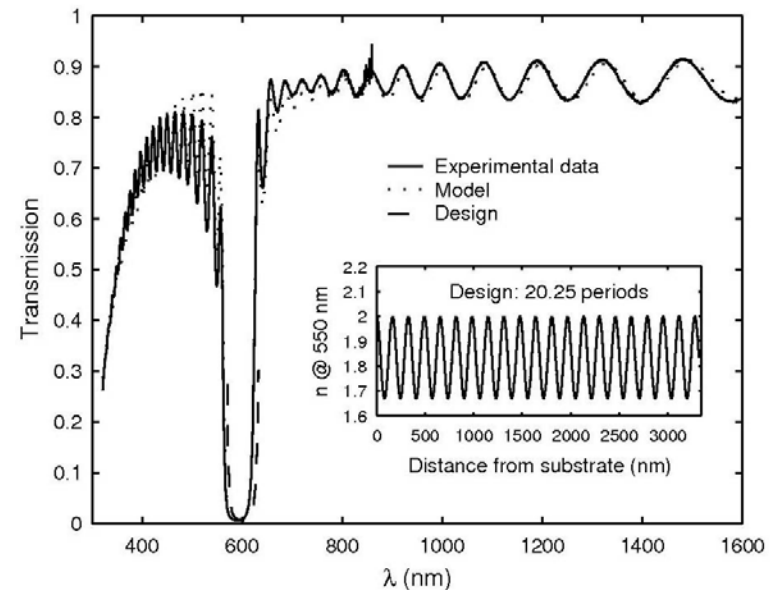
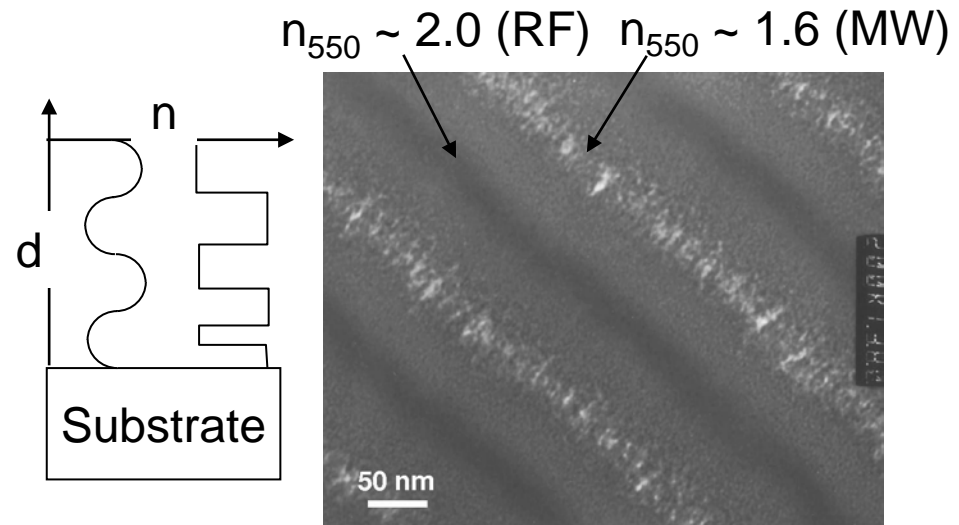
Energy per deposited particle: $E_p \approx E_i \times \phi_i / \phi_n$

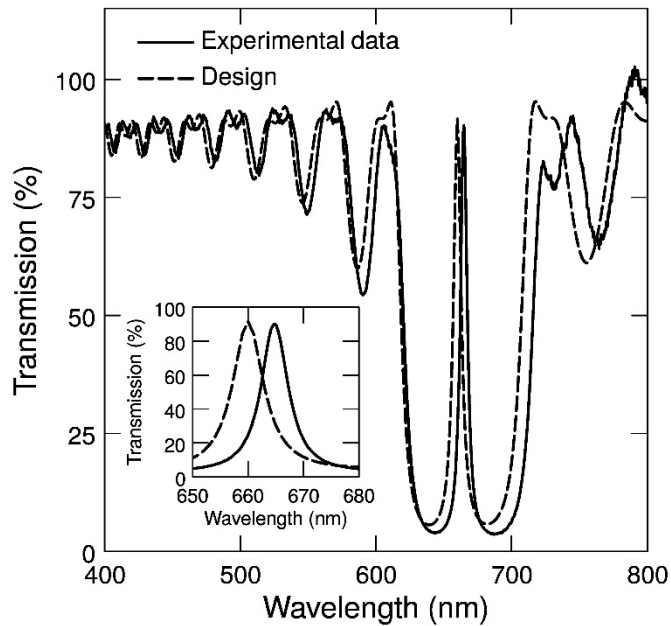
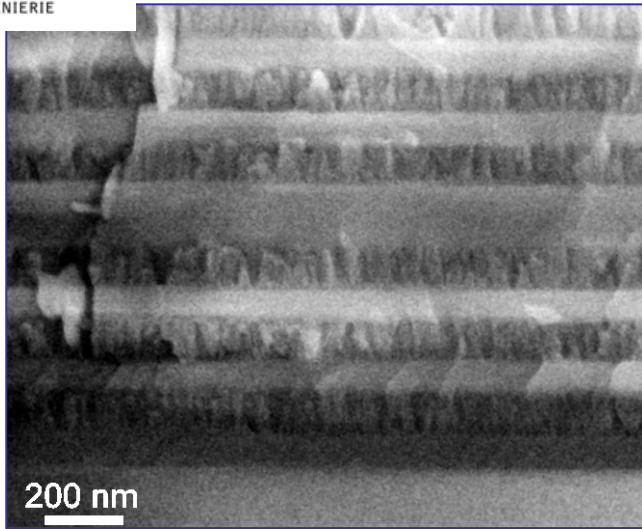
$$E_b(\text{Si}) \approx E_b(\text{N}) \sim 2 \text{ eV} < E_{\text{max}} (\text{MW}) < \left\{ \begin{array}{l} \text{Bulk displacement} \\ E_{\text{disp}}(\text{Si}) \sim 20 \text{ eV} \\ E_{\text{disp}}(\text{N}) \sim 28 \text{ eV} \end{array} \right\} \ll E_{\text{max}} (\text{RF})$$

L. Martinu, JVST A, 2000
A. Hallil et al, JVST A, 2000

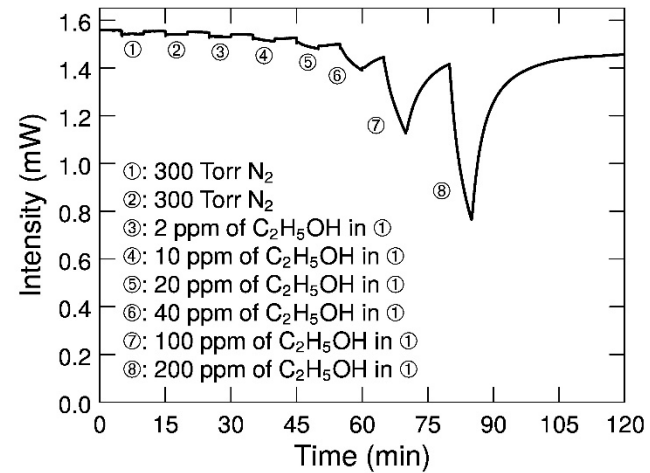
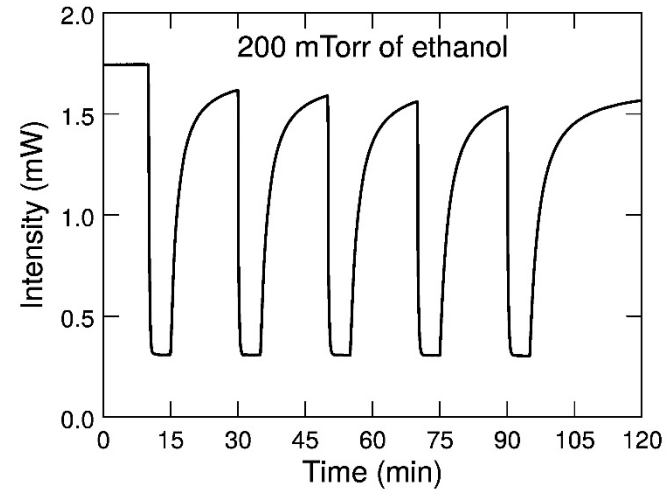
Single-material (Si_3N_4) rugate filter

- A single material is used to provide low, high and all intermediate refractive indices
- n dependent on the microstructure and porosity
- Microstructure and porosity dependent on ion bombardment energy, E_i , and incident flux, Φ_i
- Dual-mode RF/MW PECVD flexible enough to produce $\text{SiN}_{1.3}$ films with $n_{550} \sim 1.2 - 2.0$
- Graded-index optical filters have been fabricated

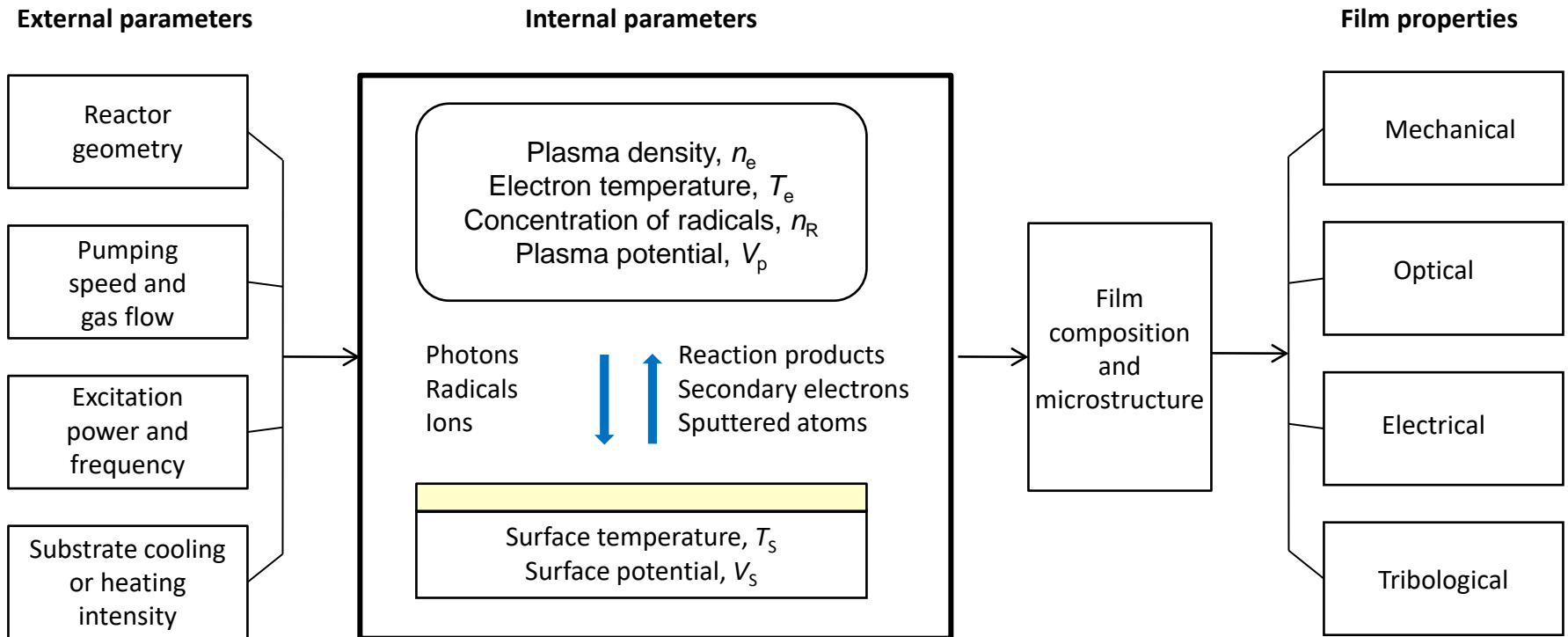




Fabry-Perot porous/dense OIF sensor



Plasma system and process control



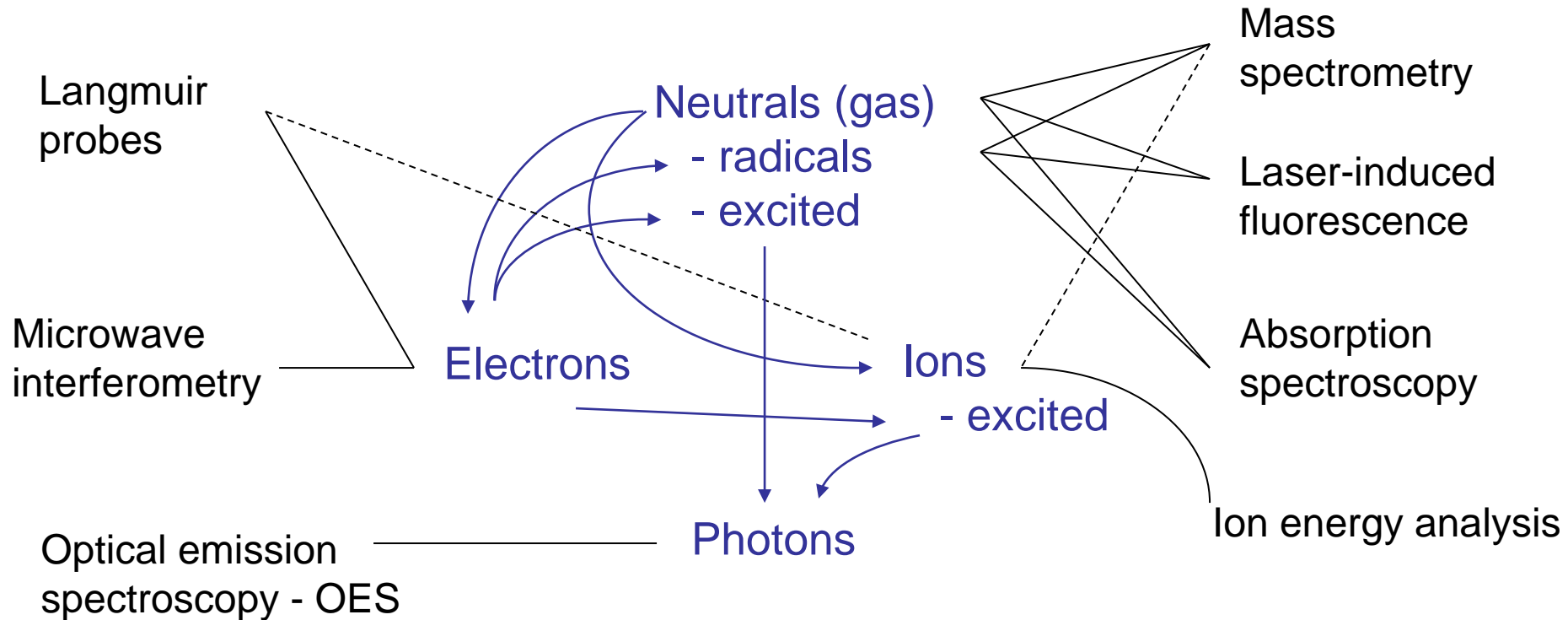
Today:

Reactive sputtering

Microstructural evolution during the film growth – Structure zone model

Plasma diagnostics

Plasma diagnostic techniques



Plasma diagnostic techniques provide information about the concentration and energy of the species

Diagnostic methods and their capabilities suitable for advanced analysis and control of the plasma processes.

a) Plasma bulk:

Diagnos- tics method	Measured parameters	Derived characteristics	Perturb the plasma	Time resolution	Space resolution	Cost	Contami- nation is a problem	Advantages	Shortcomings
Langmuir probes	I-V characteristics; Ion and electron currents	n_e, T_e, V_p, λ_D , EEDF	slightly	10^{-5} s	5 mm	\$ - \$\$	+++	Simple instrumentation	Complex interpretation
Mass- spectrometry	Mass-selective intensity	Concentrations of atoms, molecules and fragments	slightly	10^{-3} s	1 cm	\$\$ - \$\$\$	++	Many species, straightforward	Differential pumping, short lived species
Ion energy analysis	Ion current	IEDF	slightly	10^{-4} s	1 cm (0.1 mm)	\$	+++	Direct ion flux	No mass resolution
Optical emission spectroscopy	Spectrally resolved emission intensity,	Concentrations of atoms, molecules and fragments; Vibrational and rotational temp., partial info. on the EEDF	no	10^{-9} s	1 mm x 10 cm	\$\$-\$\$\$	+	Easy to set up	Indirect, convoluted interpretation
Absorption spectroscopy	Spectrally resolved absorption	Concentrations of atoms, molecules and fragments	no	10^{-9} s	1 mm x 10 cm	\$\$\$	+	Access to radical densities	Bulky, limited set of species
Laser induced fluorescence	Induced light intensity	Concentrations of atoms, molecules and fragments,	no	10^{-9} s	1 mm x 10 cm	\$\$\$	+	Access to radical densities	Bulky, limited set of species
Plasma impedance	Current, voltage, phase shift	Resistance, Capacitance, n_e	no	10^{-3} s	none	\$	-	Simple	Indirect, convoluted interpretation



b) In situ real time film growth monitoring :

Monitoring method	Measured parameters	Derived characteristics	Perturb the plasma	Time resolution	Precision in assessing thickness	Cost	Contamination problem	Advantages	Comments
Quartz crystal microbalance	Vibration frequency	Mass, d , r_D , density (indirect)	slight	1 s	1-5 nm	\$	-	Simple	Sensitive to heating and to electric fields
Interferometry	Light intensity in transmission or reflection	d , n , r_D	no	10^{-3} s	1-5 nm	\$ - \$\$	+	Simple	Single wavelength or multiwavelength; transparent films
Spectroscopic reflection / transmission	Spectrally resolved light intensity	d , n , r_D	no	10^{-3} s	1-5 nm	\$\$	+	Wide range of λ	Partially transparent films
Spectroscopic ellipsometry	Ellipsometric angles $\Psi(\lambda)$ and $\Delta(\lambda)$	d , n , k , r_D	no	10^{-1} s	0.2 nm	\$\$\$	+	Precise assessment of n and k in a wide range of λ	Costly, only for at least partially transparent films.
Resistivity	Current, Resistance	d	no	10^{-3} s	Depends on knowledge of the resistivity	\$	-	Simple	Only for conductors, affected by electric fields

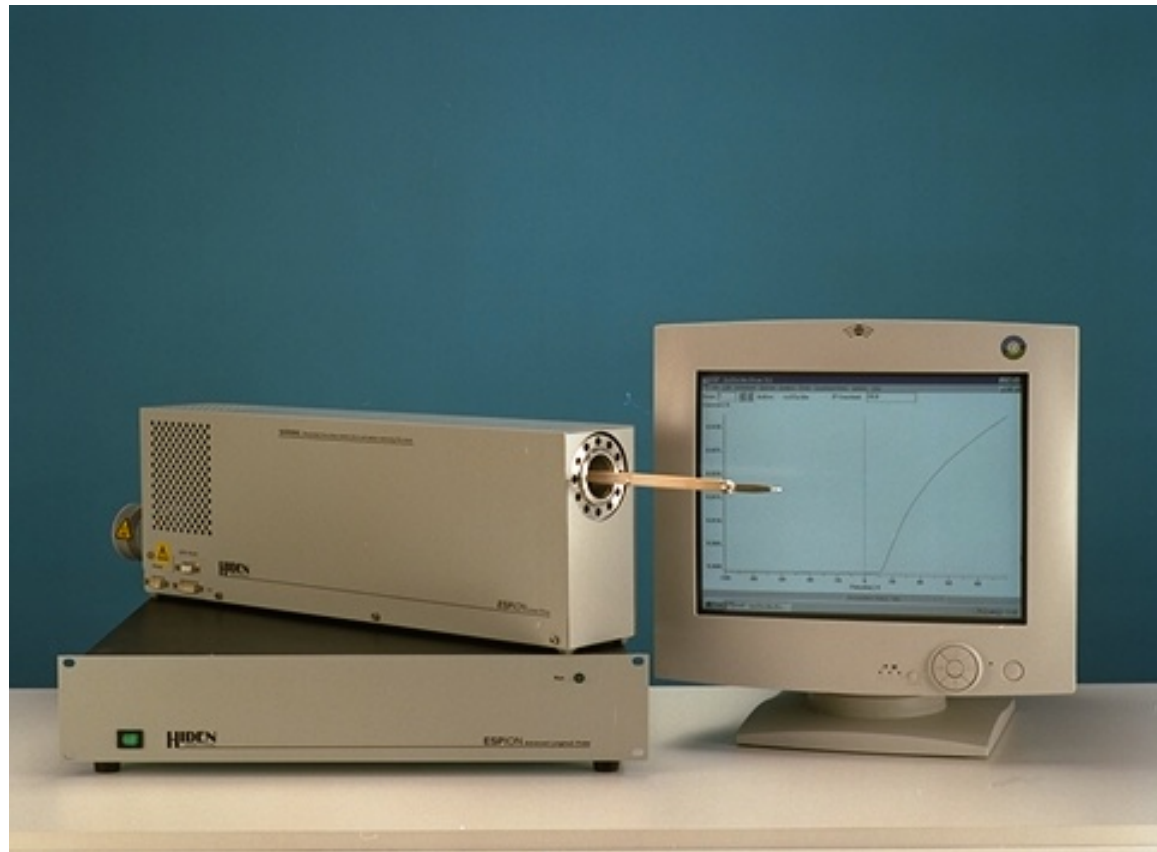


1. Langmuir probes (electrostatic): diagnostics of the main plasma characteristics:

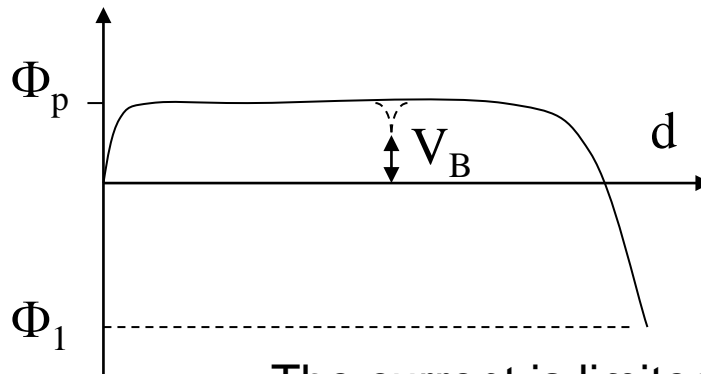
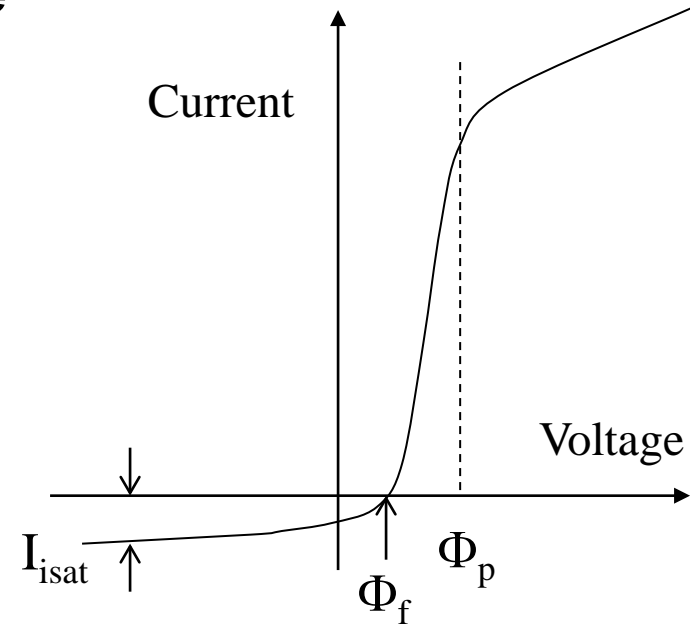
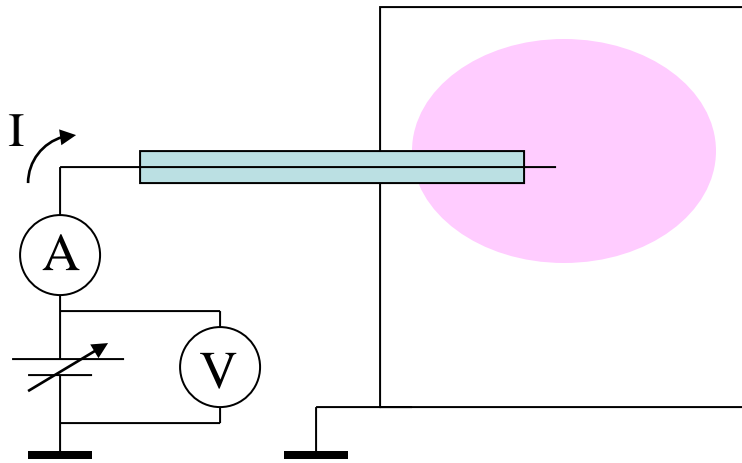
Simple probe – EEDF, n_e , V_p , V_f

Double probe - EEDF, n_e

Emissive probe - V_p

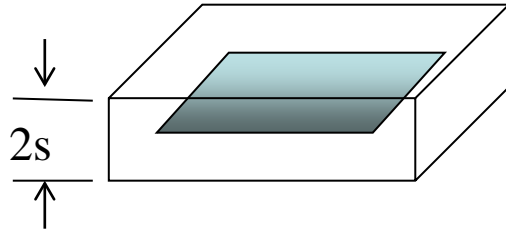


Single Langmuir probe

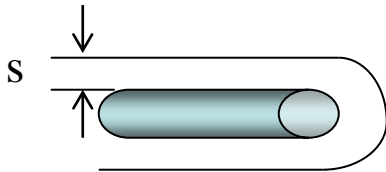


The current is limited by space charge

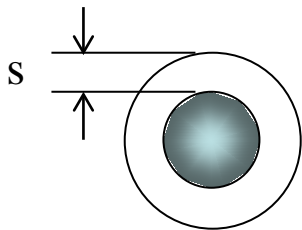
Collection surface is a function of the applied potential and of the probe geometry



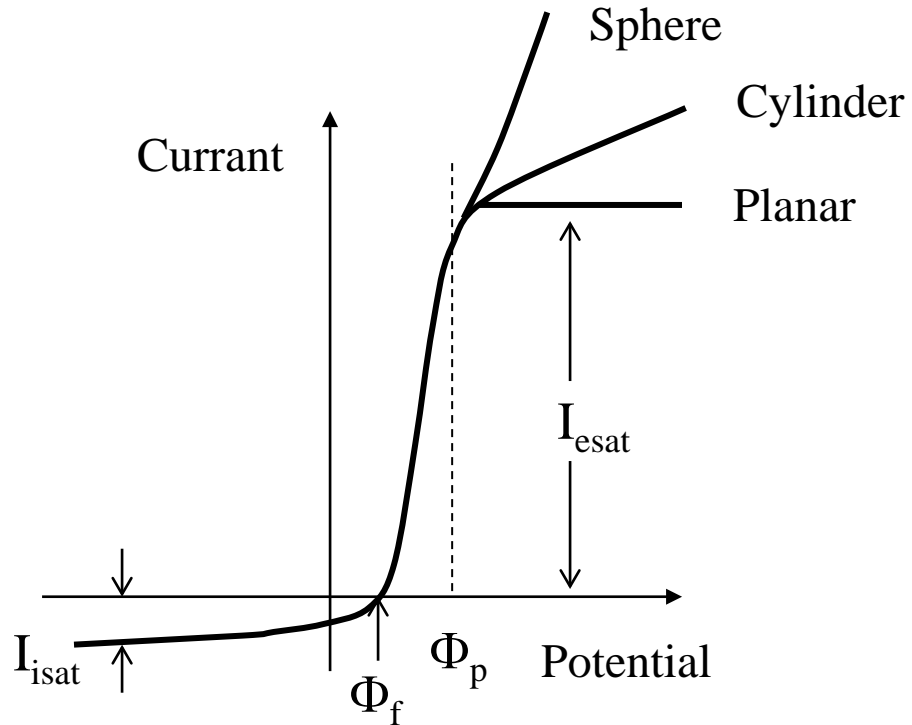
$$A \approx 2LW$$



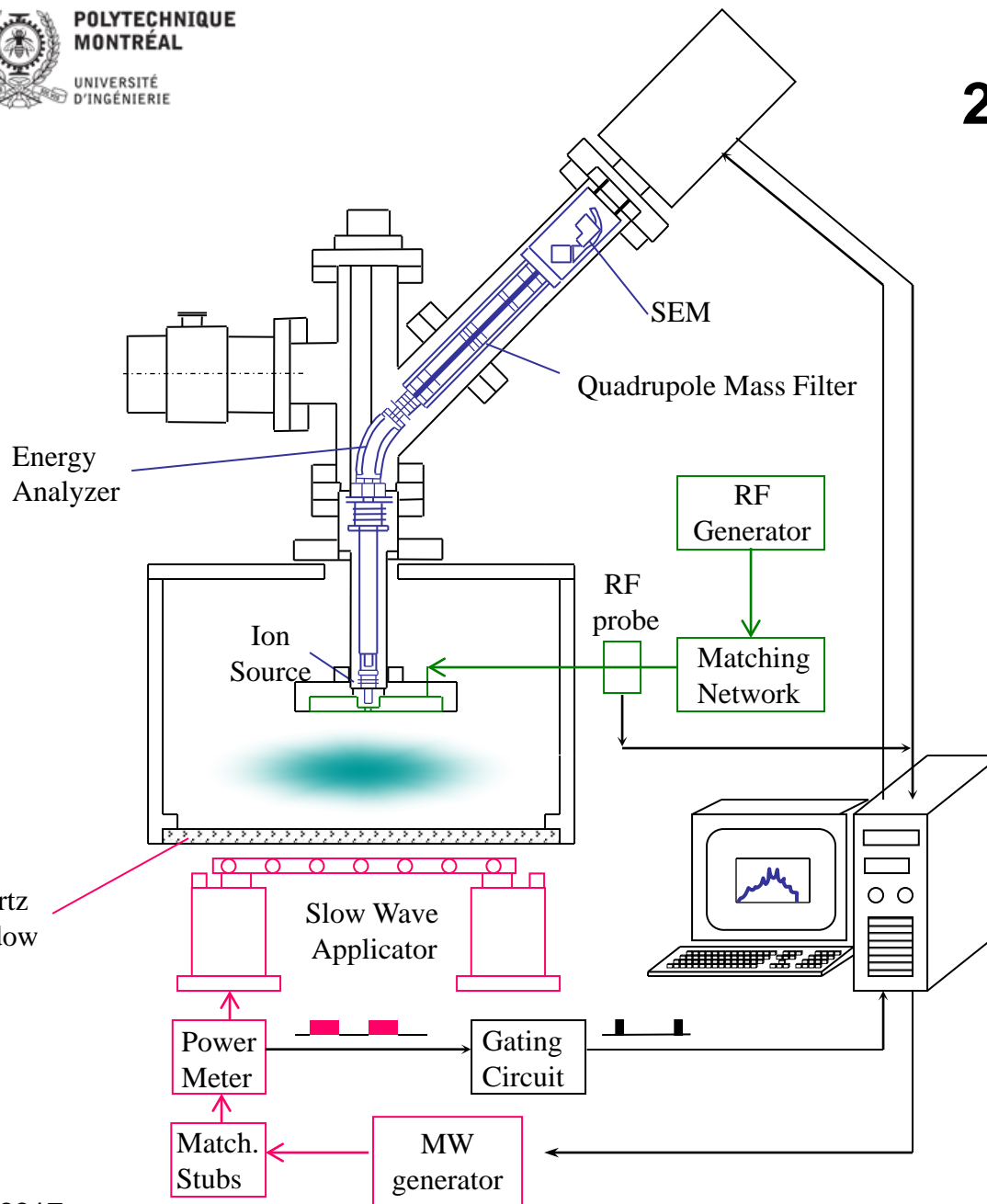
$$A \approx 2\pi (s+a) L$$



$$A = 4\pi (s+a)^2$$

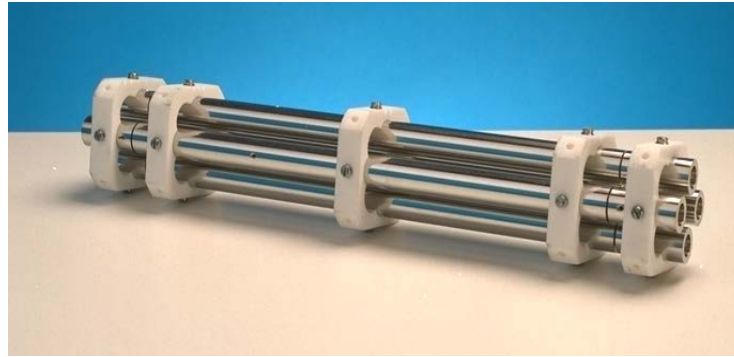


2. Mass spectrometry



- Hiden EQP-1000 plasma probe:
- mass- and time-resolved energy distributions of positive ions, negative ions, neutrals.

Quadrupole mass analyser



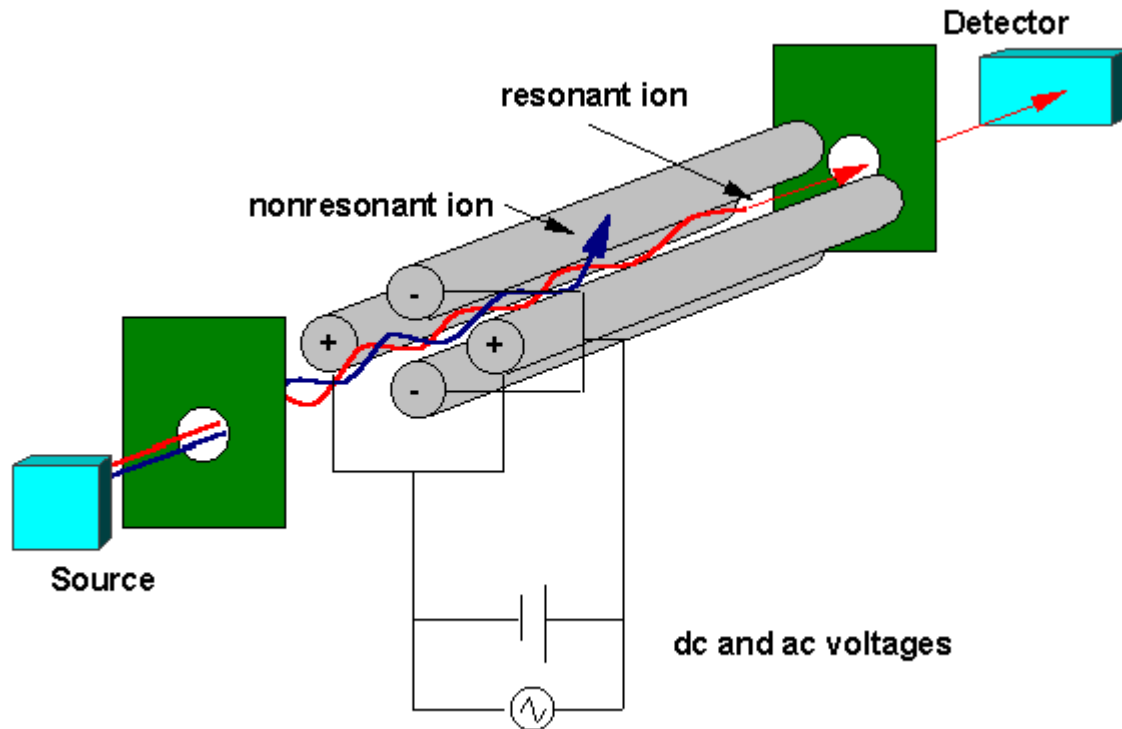
Quadrupoles are four precisely parallel rods with a direct current (DC) voltage and a superimposed radio-frequency (RF) potential. And by scanning a pre-selected radio-frequency field one effectively scans a mass range.

Quadrupole mass analyzers have been used in conjunction with electron ionization sources since the 1950s and are the most common mass spectrometers in existence today. Quadrupoles have three primary advantages:

First, they are tolerant to a relatively poor vacuum ($\sim 5 \times 10^{-5}$ Torr)

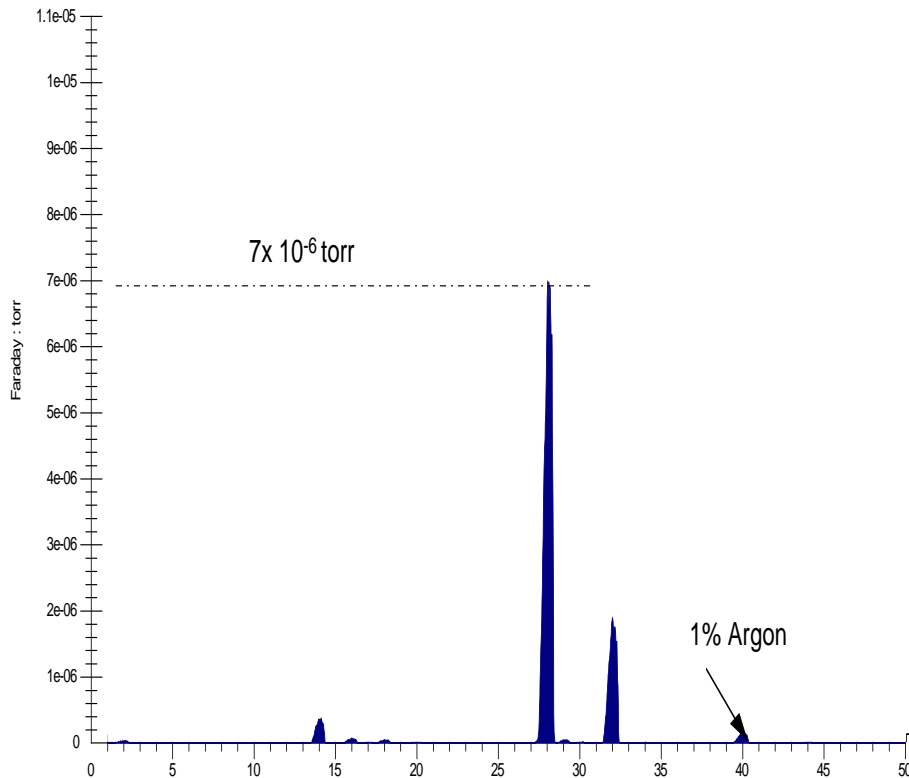
Secondly, quadrupoles are now capable of routinely analyzing up to a m/z of 3000, which is useful, e.g., for the analysis of polymers and biomolecules.

Finally, the relatively low cost of quadrupole mass spectrometers makes them attractive for use in many applications.



Separation by $v \rightarrow$ par M/Z
 i.e.
 $\text{Ar}^{++} \quad M/Z=40/2=20$
 and
 $\text{Ne}^+ \quad M/Z=20/1=20$
 are not resolved

RGA mode (Residual Gas Analysis)



Analysis of the neutrals

Gas composition

Detection of impurities

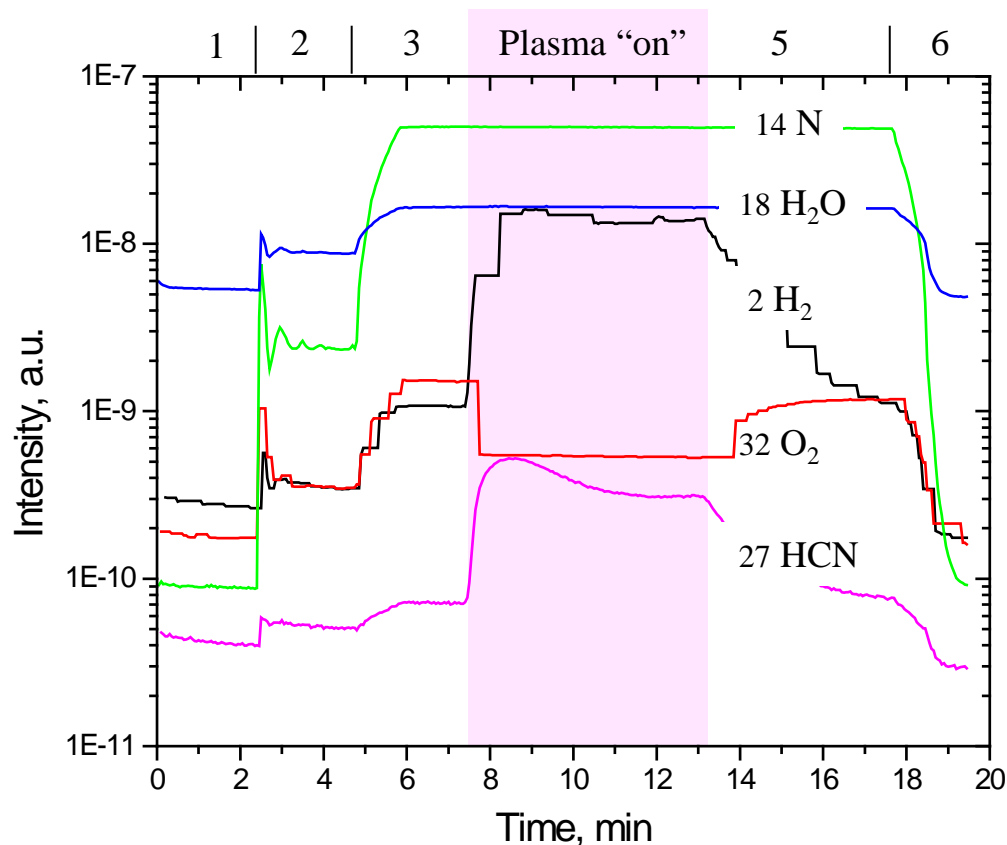
Process kinetics

‘End point detection’

Real and virtual leaks

Mass-spectrometry - application

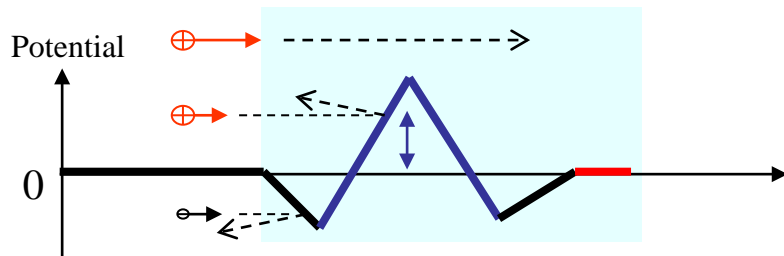
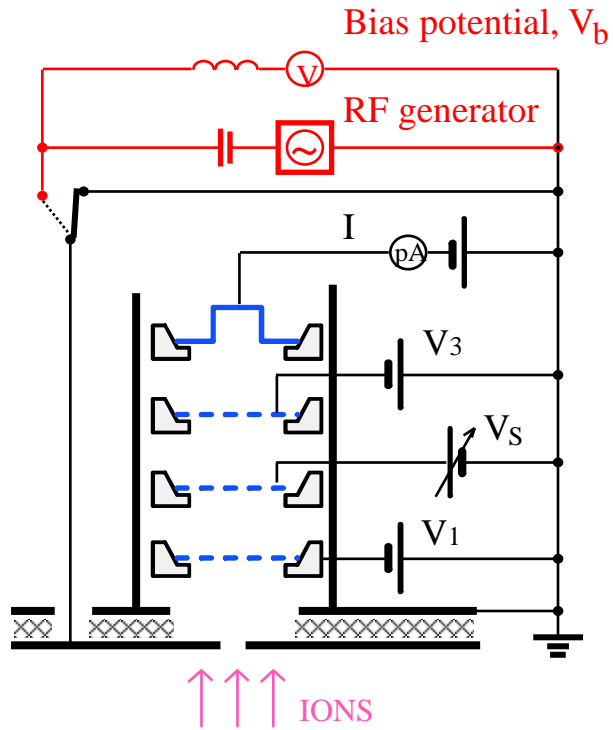
Polymer (PP) treatment in N₂ plasma



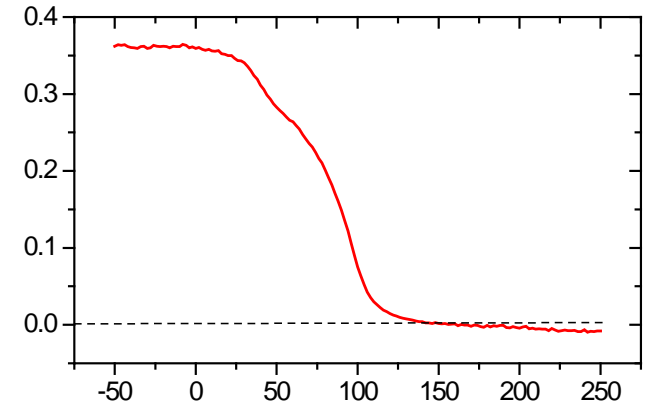
- 1- residual gas
- 2- N₂ 15 sccm, p = 20 mTorr
- 3- throttle valve activated, p = 200 mTorr
- 4- Rf 50/1 W, V_b = -233....-207 V
- 5- Rf "off"
- 6- valve open, after 1 min gas is closed

Example: results from Polytechnique

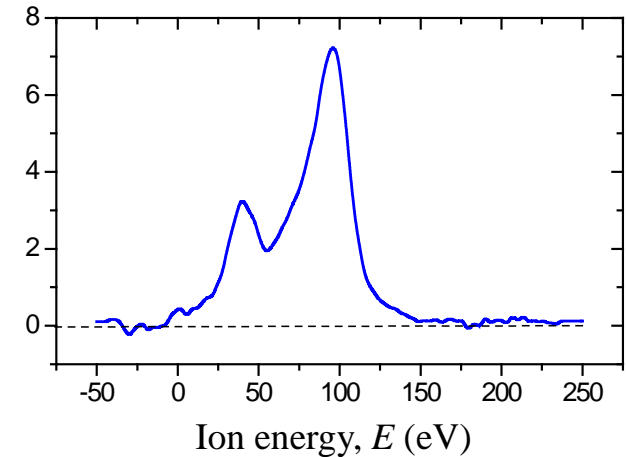
3. Multigrid electrostatic ion energy analyzer



Collector current, I (μA)

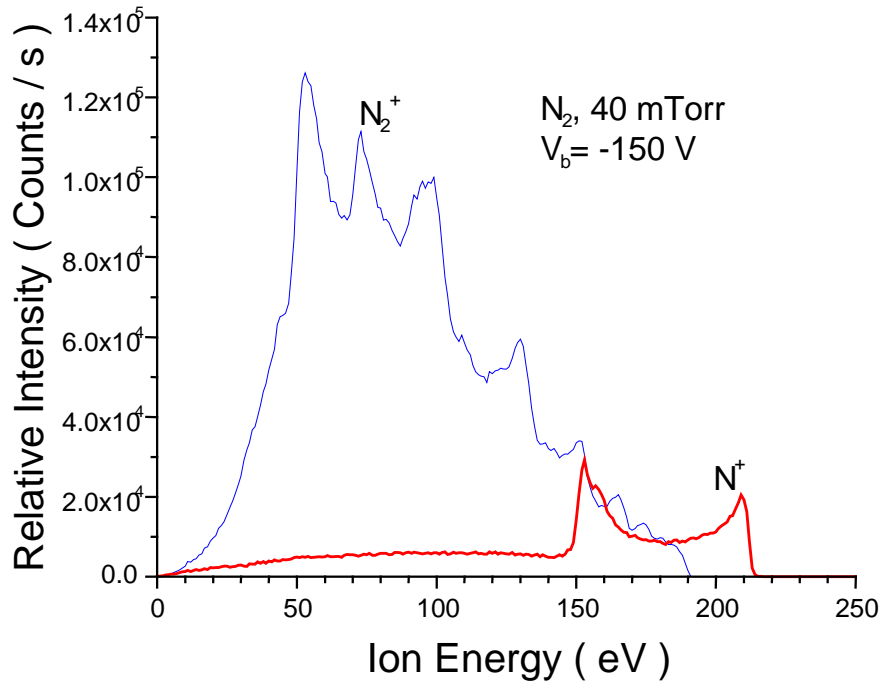


IEDF, $f_i(E)$ (nA/V)

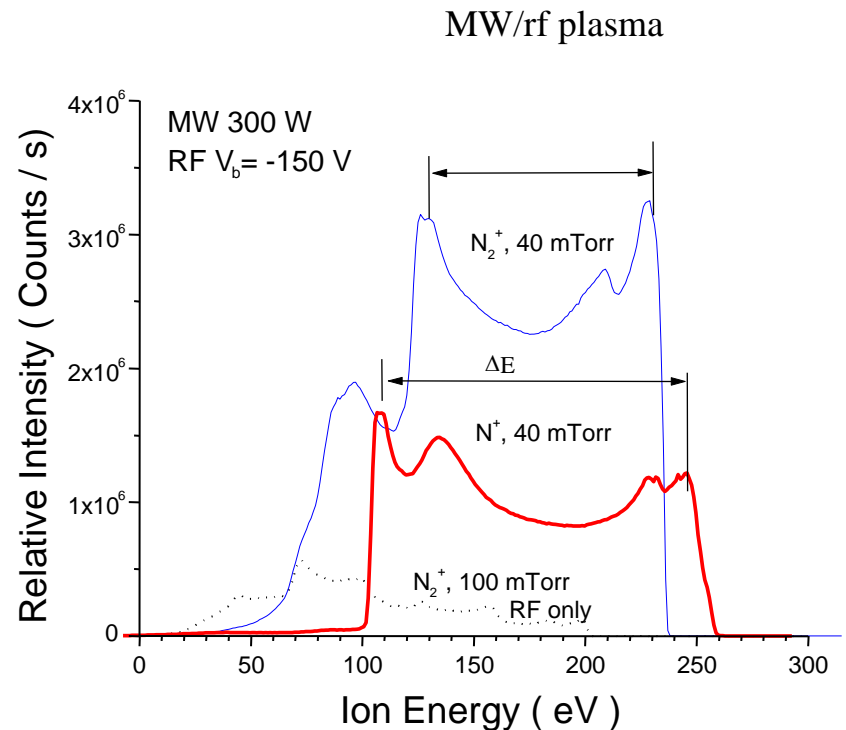


IEDF on the RF-powered electrode

$$E_{\max} = |V_b| + V_p + (\Delta E/2) > |V_b|$$



Les ions N_2^+ subissent plus des collisions dans la gaine à cause de procédés résonants de transfert de la charge



La gaine plus petite dans les plasmas denses mène à des énergies des ions plus importantes:

- moins des collisions
- plus de modulation

4. Quartz crystal microbalance

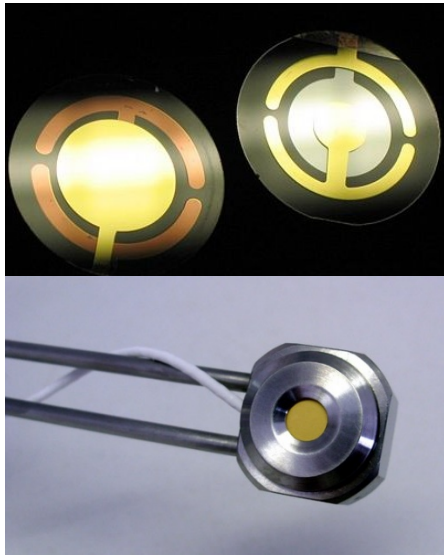
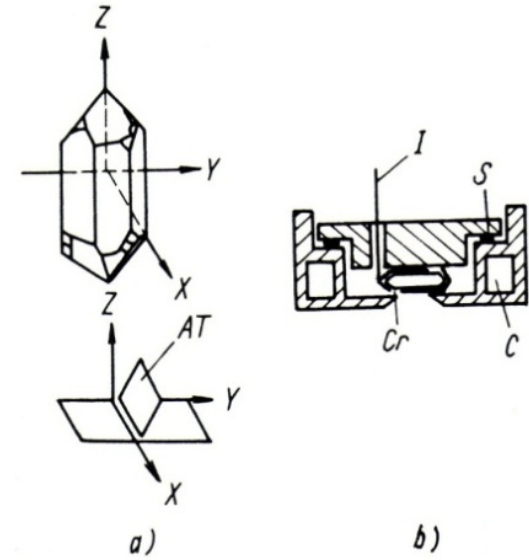


Fig. 45: (a) orientation of AT cut in quartz; (b) crystal holder: I – inlet bushing, S – seal, Cr – crystal, C – cooling.



Incrément d'épaisseur:

$$dt = \frac{1}{\rho_K S} dm$$

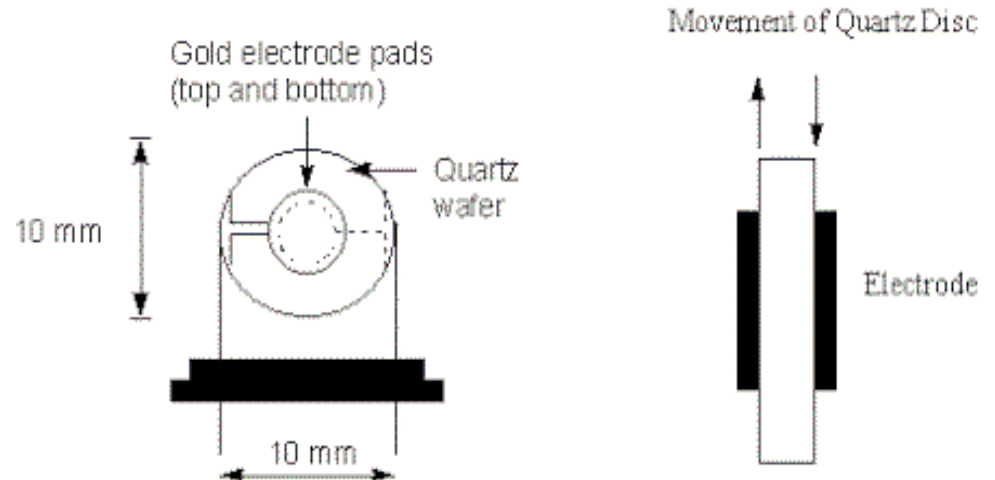
Sauerbrey equation:

$$\Delta f = - \Delta m / A (f_0^2 / N \rho_q)$$

Completing the story:

$$E_p \sim E_i \cdot \Phi_i / \Phi_N$$

$$\Phi_N = r_D \frac{\rho N_A}{m_A}$$



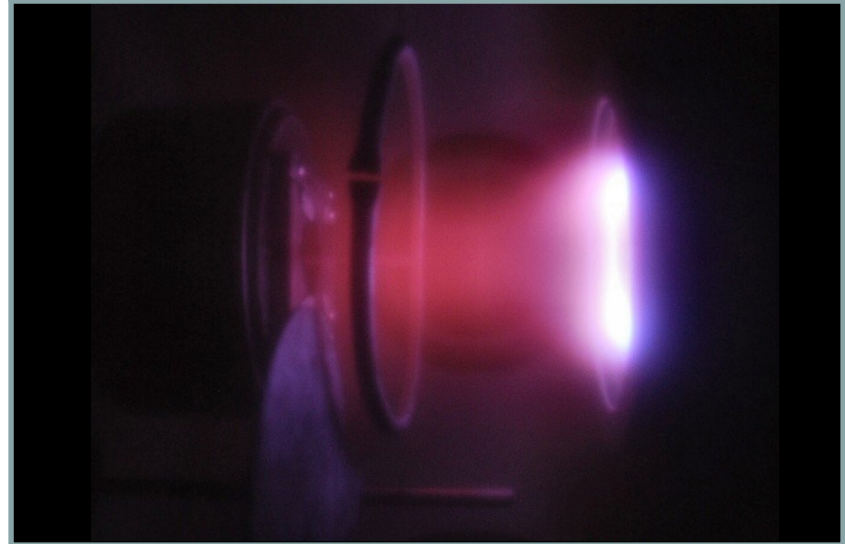
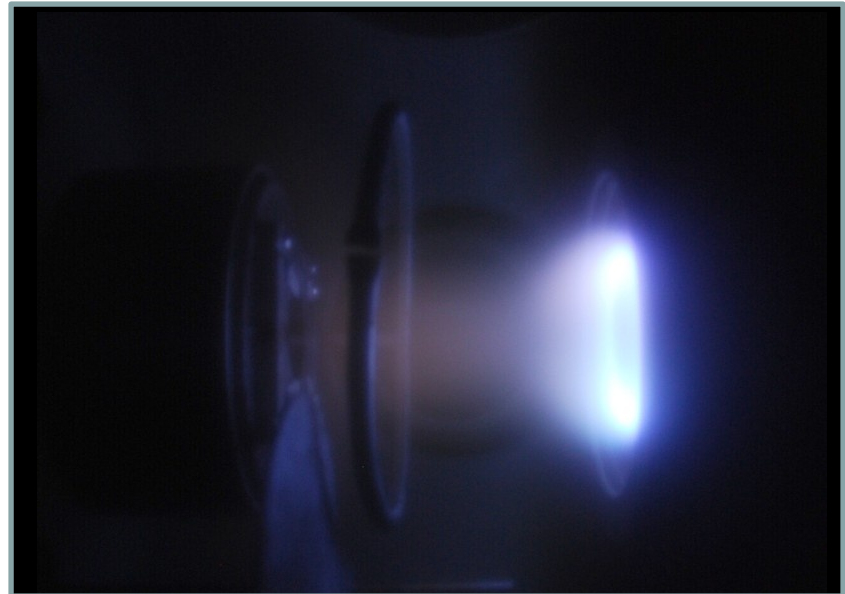


5. Optical diagnostics

- HIPIMS discharge
- Cr target
- 50 Hz – 200 μ s pulses

- 2 configurations:
 - 2.2 mTorr Ar
 - 2.2 mTorr Ar + N₂ (reactive mode)

Images courtesy of Matěj Hála (LaRFIS)



Optical emission spectroscopy - OES

Assessment of the light emission in the NIR-VIS-nearUV range (200 – 1000 nm or 1-5 eV).

Emission from the electronically excited states of atoms, radicals, ions, molecules.

Identification of species based on the wavelength of the peaks (bands) and the knowledge of the spectroscopy.

Usual wavelength resolution between 0.1 et 1 nm.

Simple to install, frequently used for qualitative approaches (e.g., end point detection during etching, identification of impurities etc.).

Space- and time- resolved OES

Examples for the discharges in Ar and N₂

C M Ferreira and J Loureiro

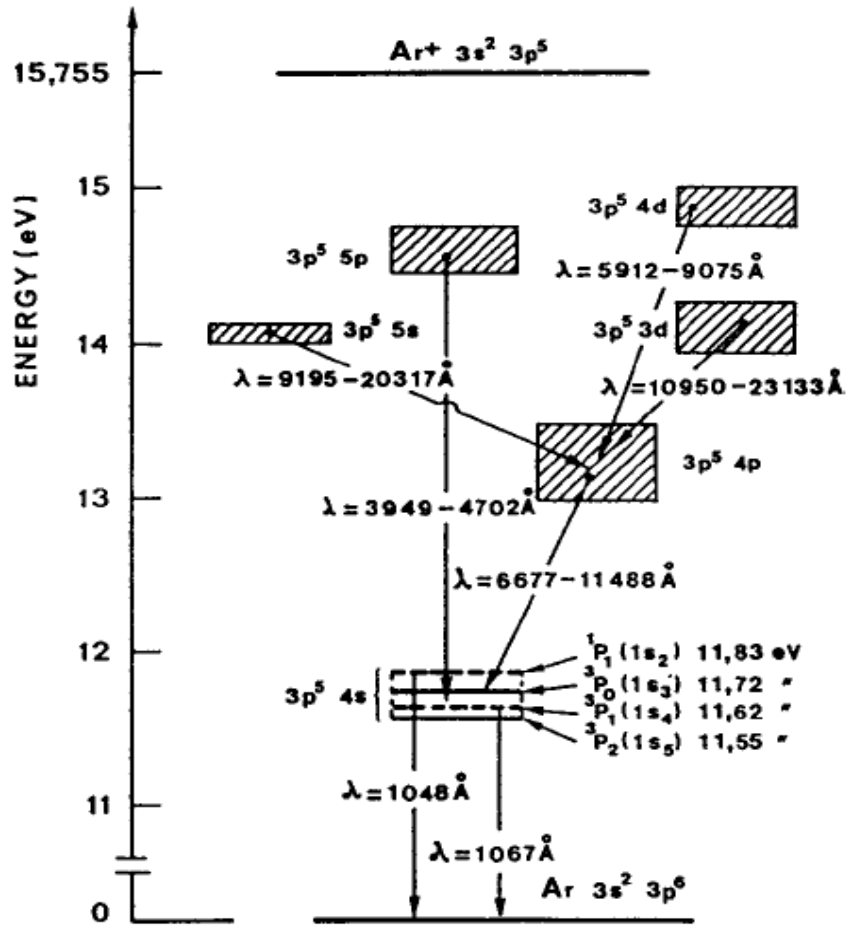


Figure 1. Energy levels of Ar.

C M Ferreira and J Loureiro

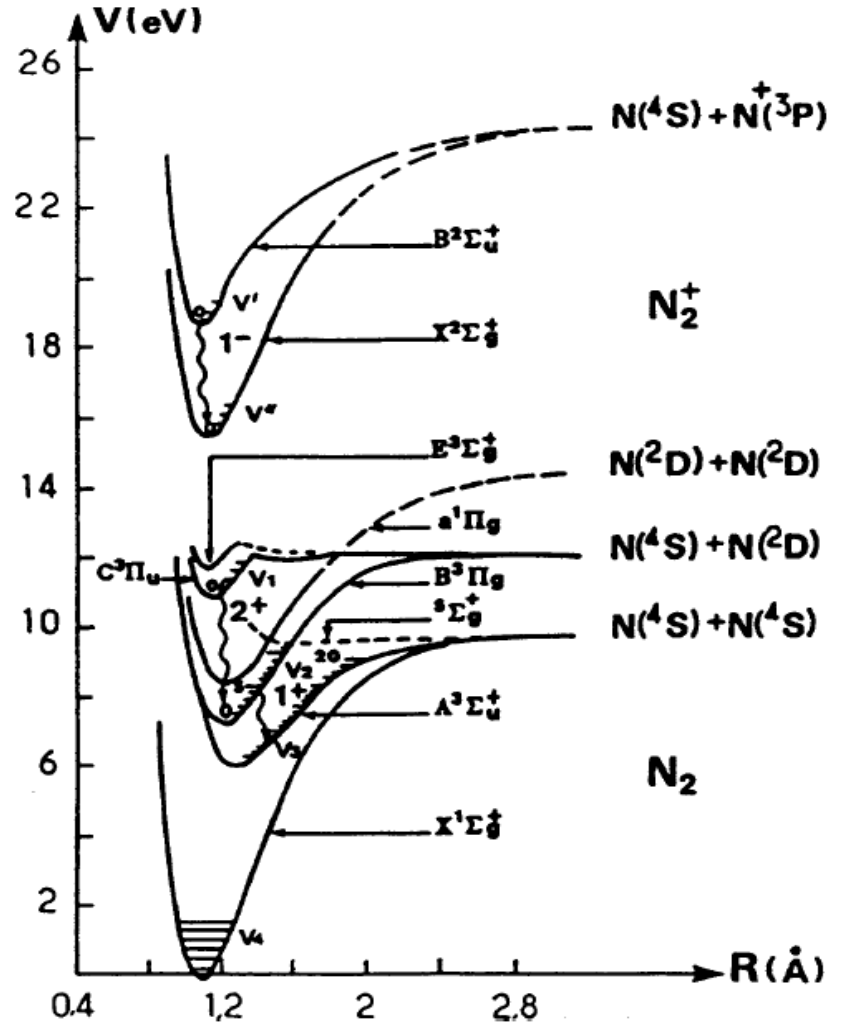
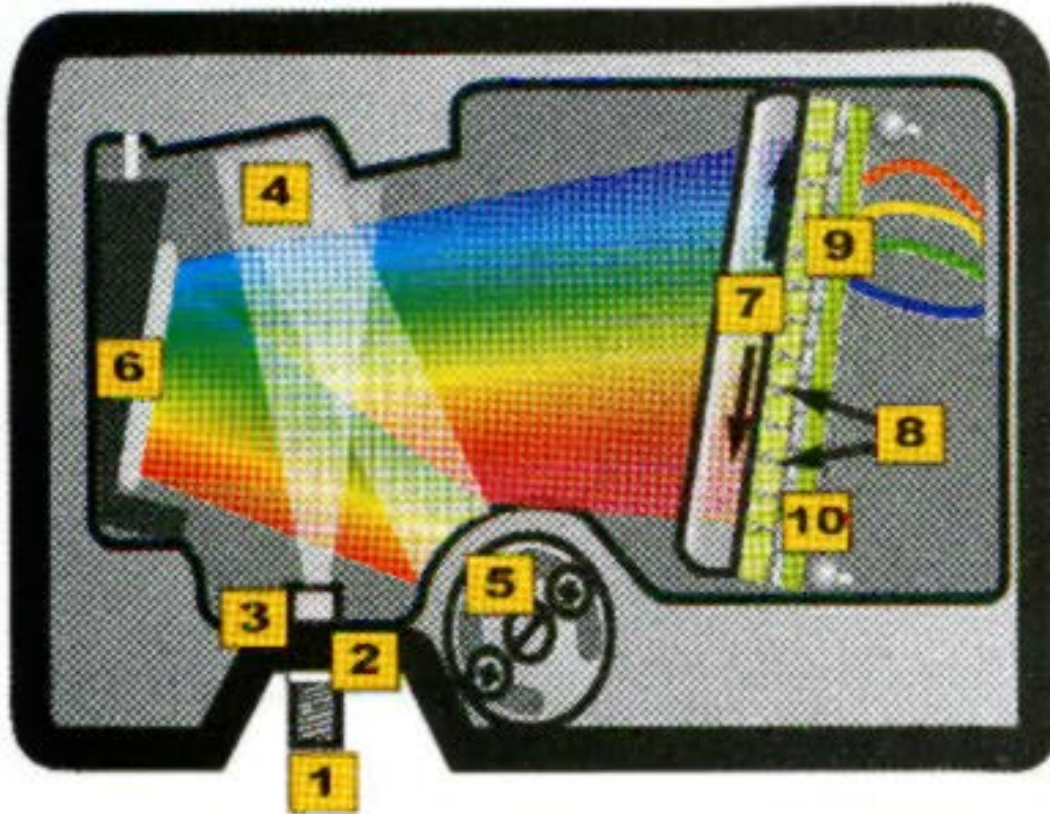


Figure 9. Energy level diagram of N₂.

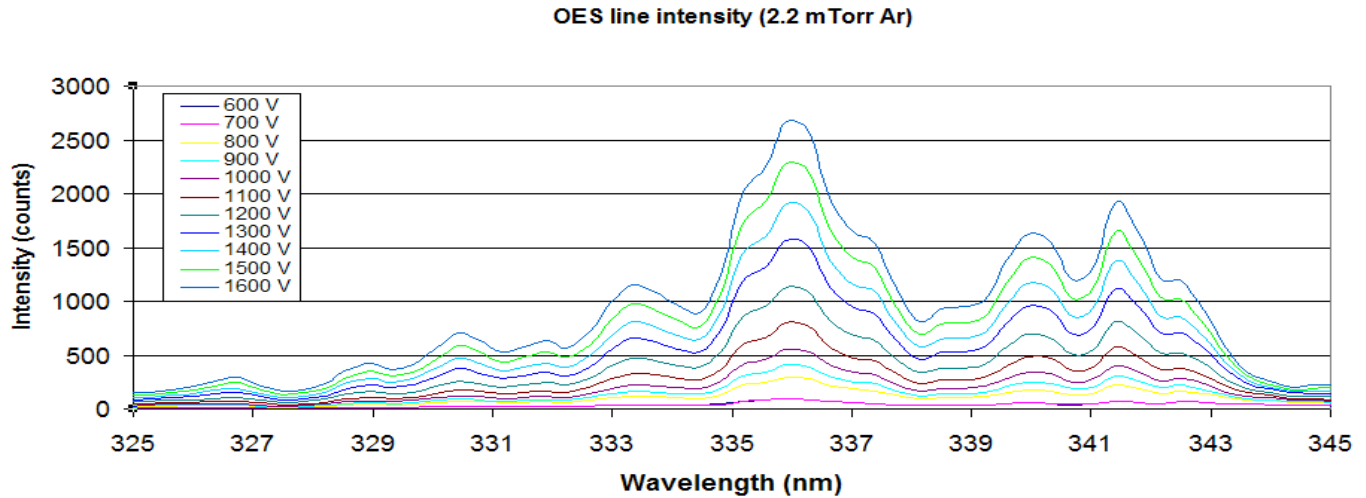
Optical spectrometer



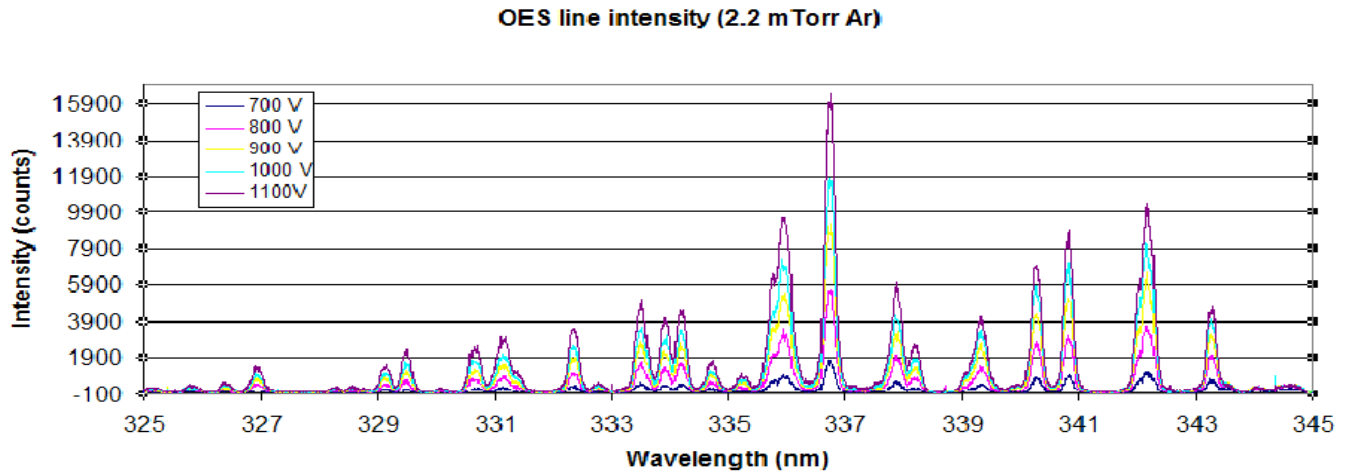
- 1 Entrance
- 2 Entrance slit
- 3 Filter
- 4 Collimation mirror
- 5 Dispersive element (grating)
- 6 Focusing mirror
- 7 Collection lenses
- 8 Harmonics optical filters
- 9 UV-option
- 10 Detector

Spectrometer resolution

$\Delta\lambda = 2 \text{ nm}$



$\Delta\lambda = 0.2 \text{ nm}$



Line assignment

NIST Atomic Spectra Database

<http://www.nist.gov/srd/atomic.htm>

Kurucz Atomic Line Database

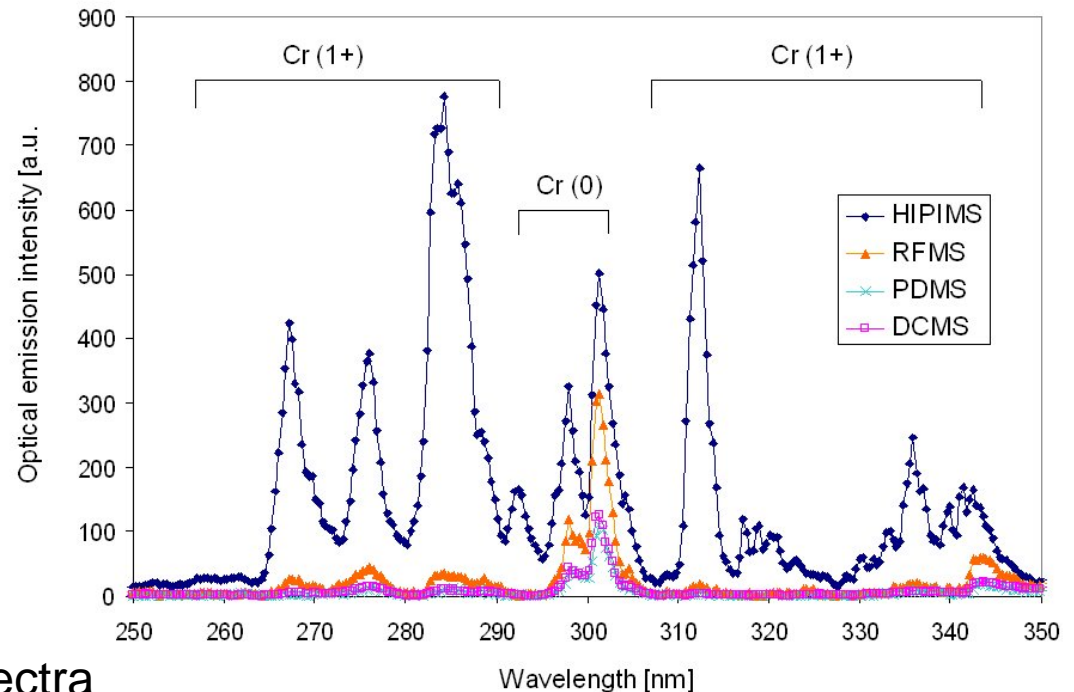
<http://www.cfa.harvard.edu/amp/ampdata/kurucz23/sekur.html>

PLASUS SpecLine software

<http://www.plasus.de>

The Identification of Molecular Spectra

Reginald William Blake **Pearse**, Alfred Gordon **Gaydon**
London: Chapman and Hall, 1976, 4th ed.



Emissions from impurities

Species	Wavelength (nm)	Source of impurity
CO	292.5, 302.8, 313.8, 325.3	Polymer oxidation, carbon
N ₂	315.9, 337.1	Air leak, nitride etching
OH	281.1, 306.4	Water, alcohol, degassing
NO	288.5, 289.3, 303.5, 304.3, 319.8, 320.7, 337.7, 338.6	Polyimide, nitride oxidation
Al	308.2, 309.3	Sputtering of Al
Cu	324.8, 327.4	Etching of Cu or brass
CN	289.8, 304.2	Nitride etching, sputtering of polyimide
Si	288.2	Sputtering of Si, dissociation of silane (SiH ₄)

G.S. Selwin, Optical diagnostic techniques for plasma processing, AVS monograph Series, M-11, AVS 1993.

Actinometry: measurement of the radical density

Addition of a « small » known quantity of inert gas [Act], e.g., Ar

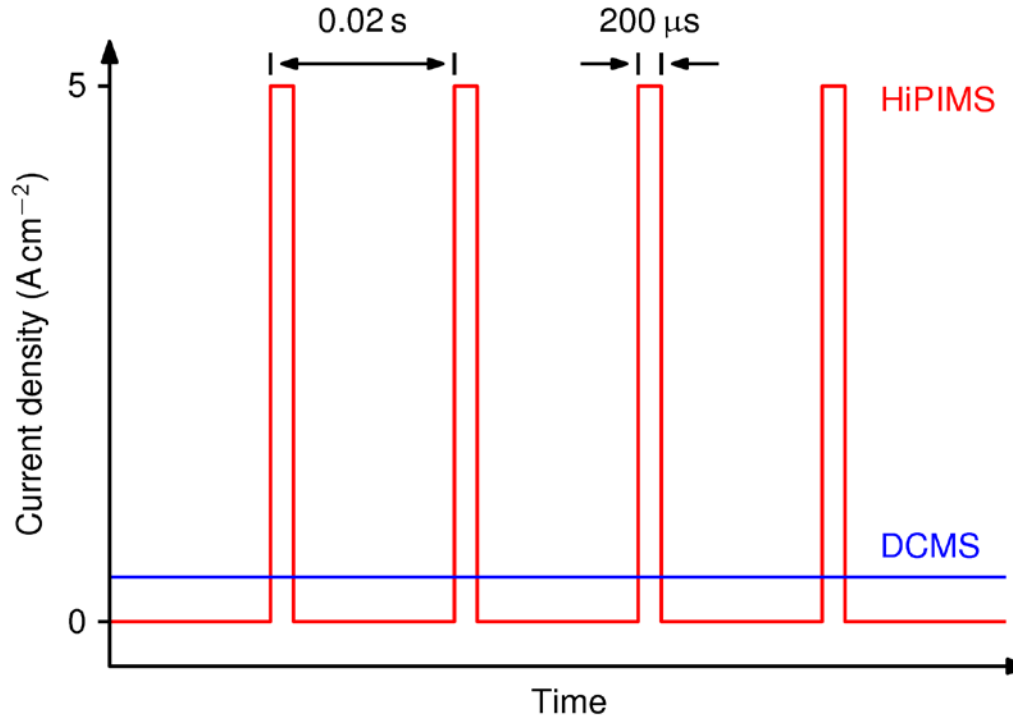
$$I(X^*) \propto K_e n_e [X]$$

$$\frac{I(X^*)}{I(\text{Act}^*)} = \frac{k_D(\lambda_x)}{k_D(\lambda_{\text{Act}})} \frac{[X]}{[\text{Act}]} \frac{K_{eX}}{K_{e\text{Act}}}$$

↑
↓
 Instrument's response [X]



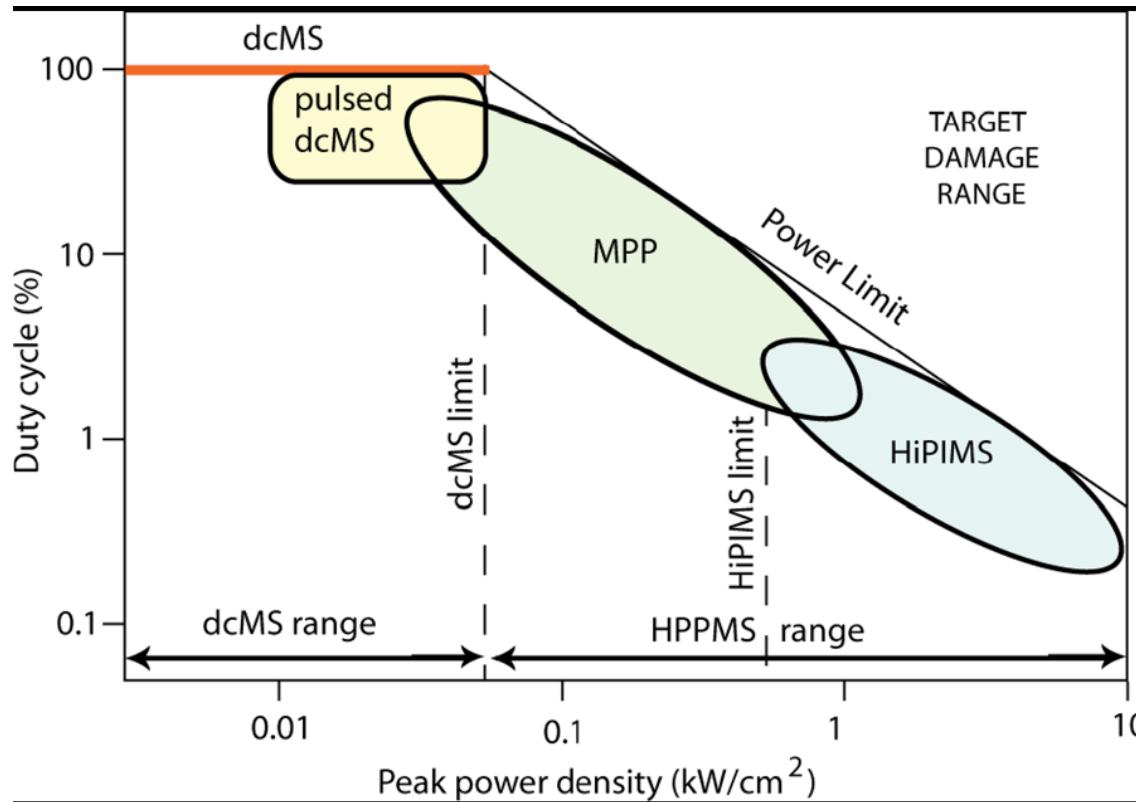
High Power Impulse Magnetron Sputtering - HiPIMS



New coating properties due to:

- high density plasmas – films obtained from ionized species
- high ion fluxes toward the substrate
- effect of ion bombardment on the microstructural evolution

Pulsed discharges

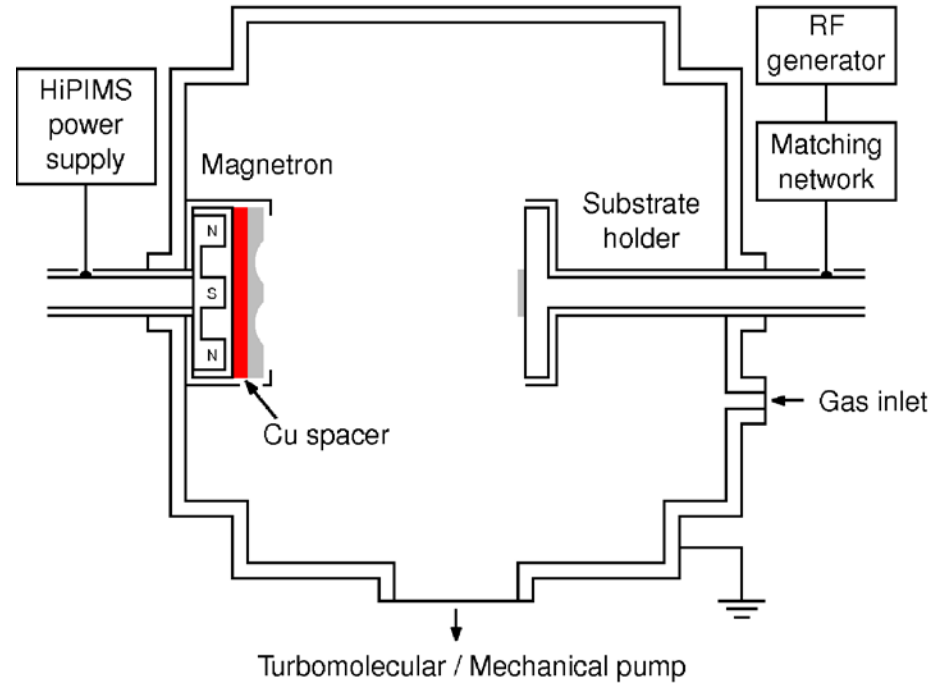
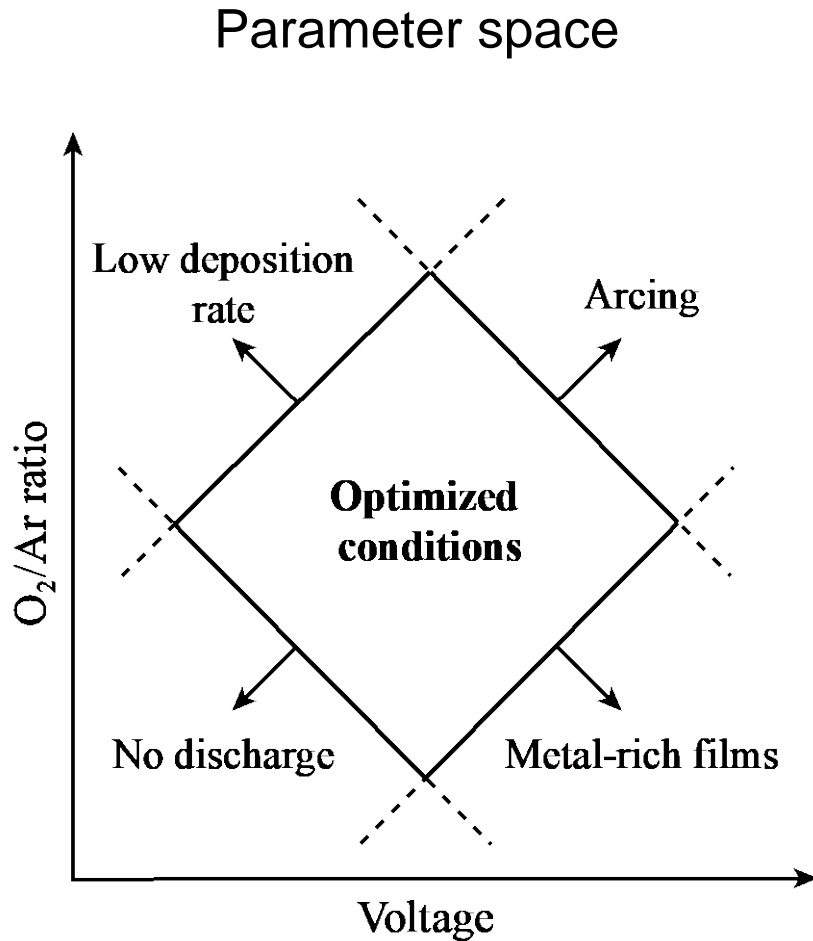


Nomenclature
for pulsed
discharges

Recent review articles and comparisons:

- J.T. Gudmundsson, N. Brenning, D. Lundin and U. Helmersson, J. Vac. Sci. Technol. A 30 (2012) 030801-1-35 (above)
- A. Anders, Surf. Coat. Technol. (2011), J. Vac. Sci. Technol. A 28 (2010) 783
- K. Sarakinos et al., Surface & Coatings Technology, 204 (2010) 1661
- MPP vs. HiPIMS: M. Hala et al, SCT 2012, JPD-AP, 45 (2012) 055204

HiPIMS process optimization



Effect of magnetic field:

J. Capek et al., J. Appl. Phys., 111 (2012)

Hysteresis suppression:

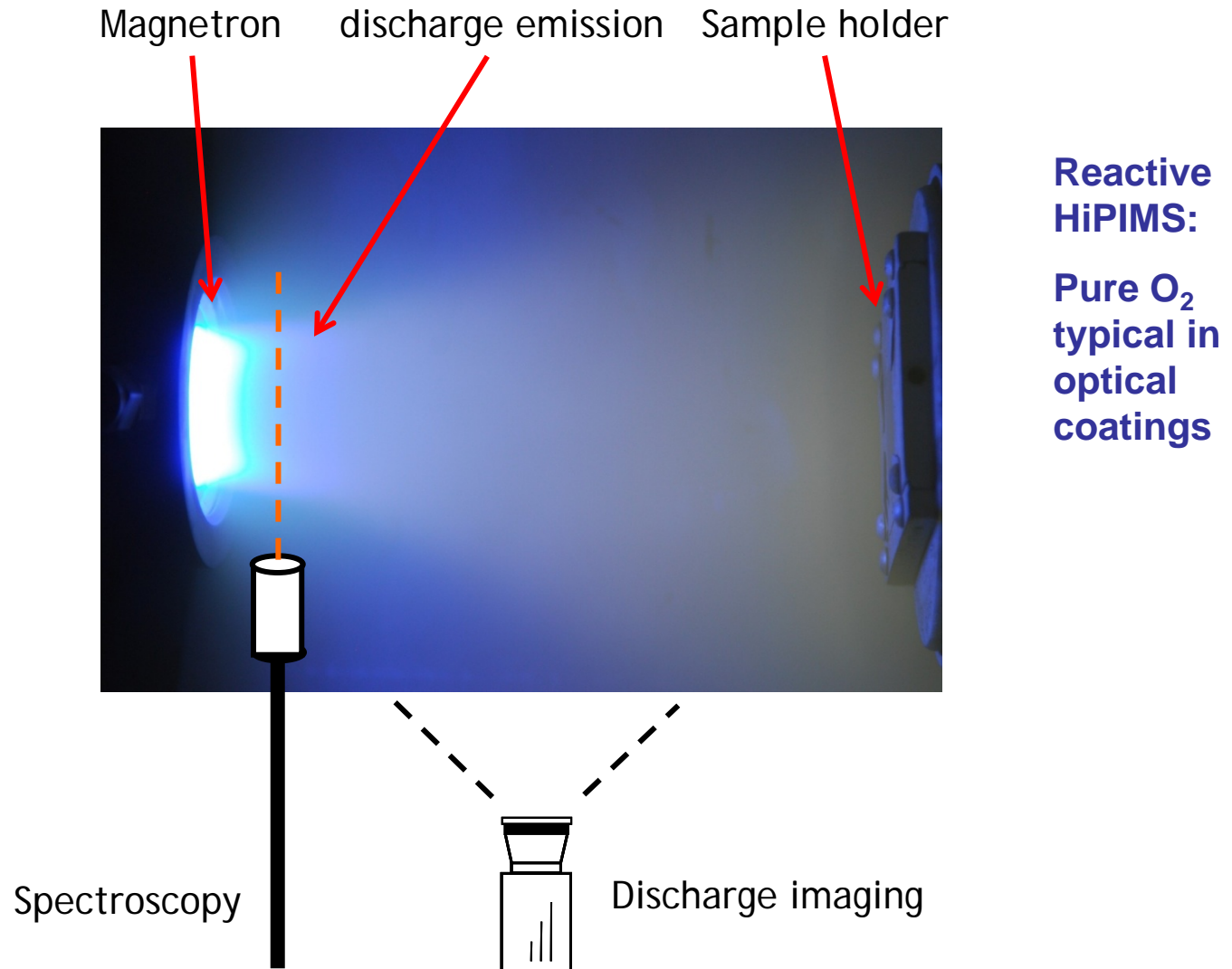
M. Hala et al., J. Phys. D: Appl. Phys., 45 (2012)

M. Hala et al., Surf. Coat. Technol. 2012

Time and space resolved OES:

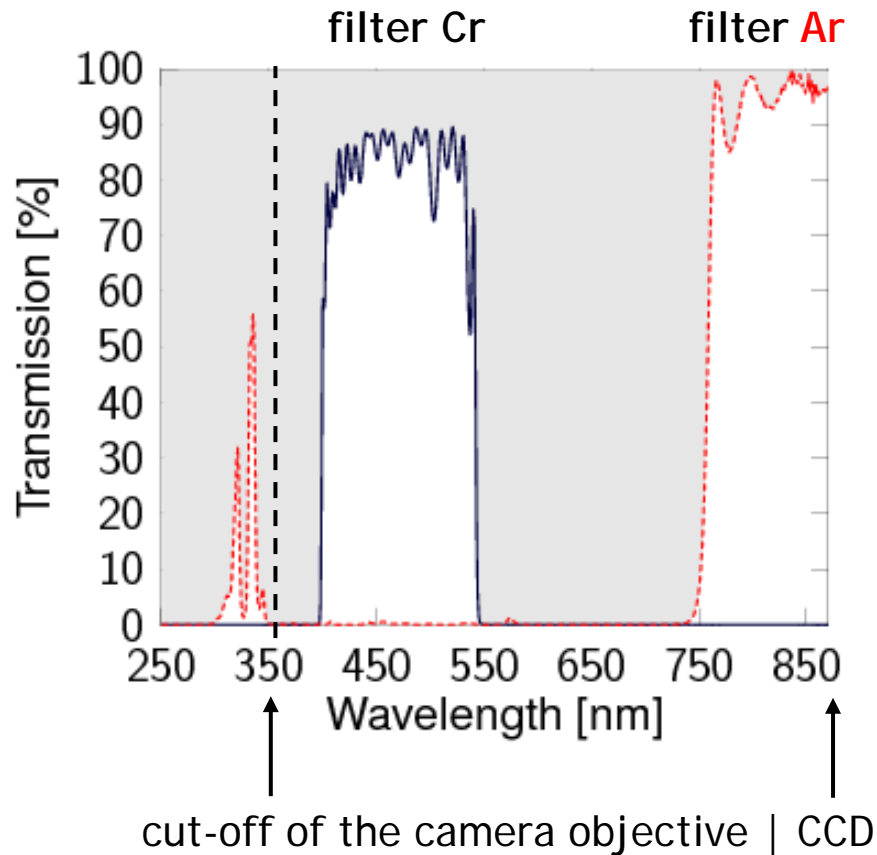
M. Hala et al., IEEE Trans. Pl. Sci., 38 (2010)

OES diagnostics – from the target to the substrate



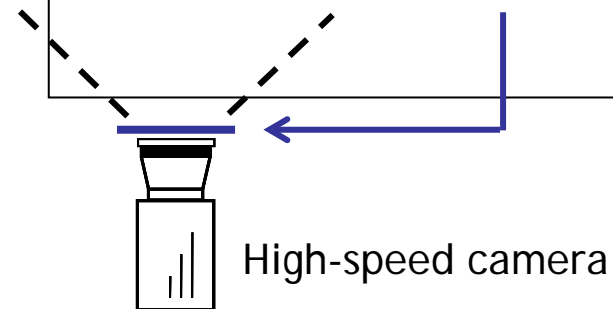
HIPIMS: Optical filters for species-resolved imaging

Filter performance and application



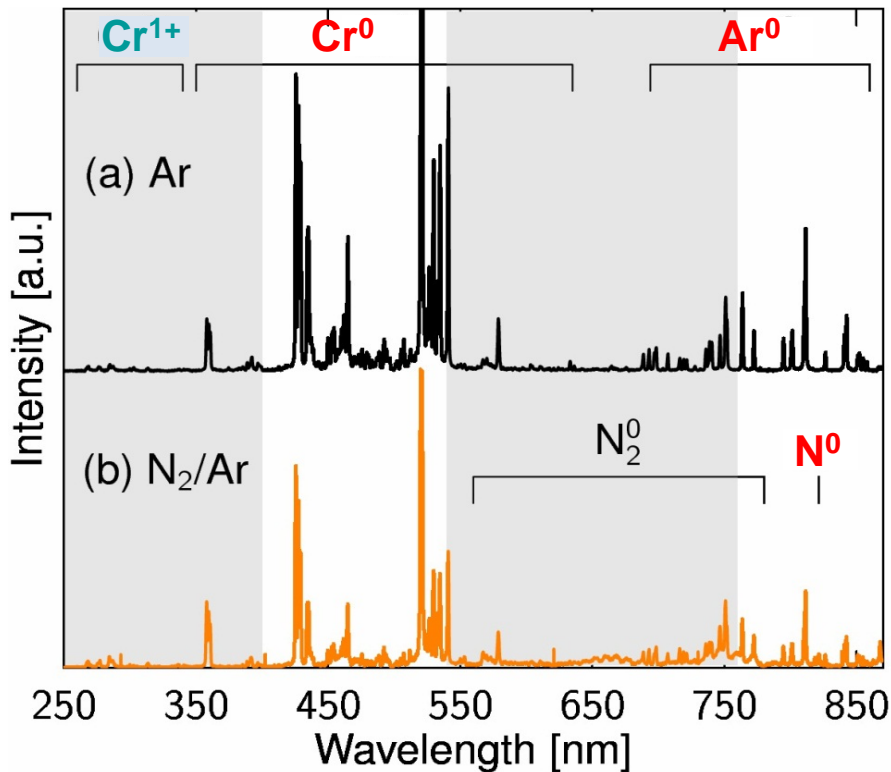
Introduction of custom-made band-pass interference filters

- high-transmission regions:
- 400 to 540 nm - filter Cr
- above 750 nm - filter Ar



HIPIMS with a Cr target: Discharges in Ar, N₂, and in Ar/N₂ mixtures

5-cm magnetron $p = 4$ Pa (30 mTorr)
 $U_c = -2000$ V OES at $d = 3$ cm

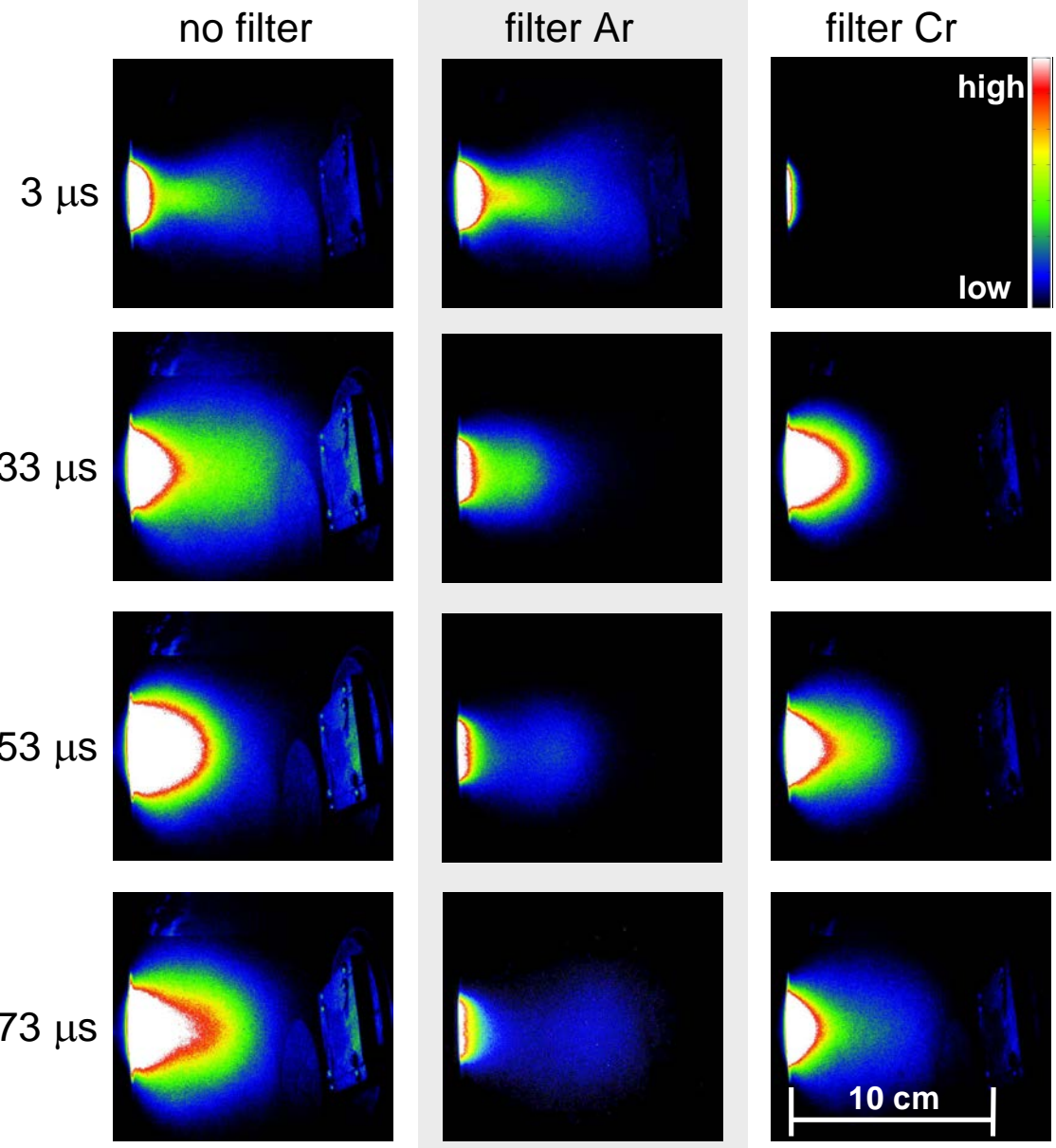


Sputtering of Cr

Two spectral regions of interest selected

- neutral chromium emission lines
- neutral gas emission lines and bands

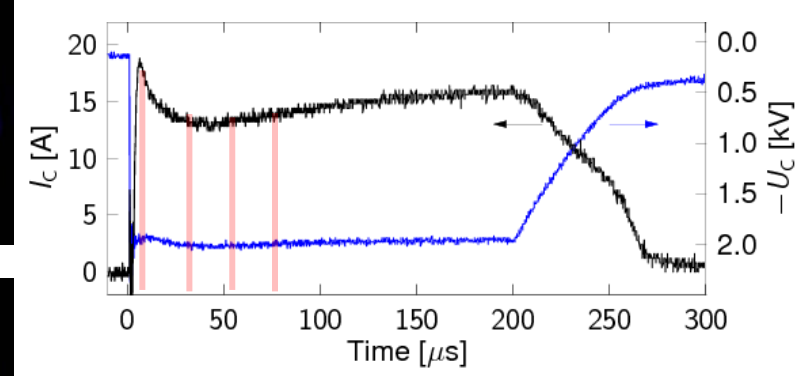
Dynamics of the HiPIMS discharge in Ar



Ignition phase
 Electron avalanches and
 working-gas ion generation

Metal-dominated phase
 Self-sputtering process
 Plasma rich in sputtered Cr
 expands outwards the target

Current and voltage waveforms





Bibliography

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PHS 6317 Nanoengineering of thin films

Course schedule – Winter 2024

12 January	Introduction – Scientific and technological challenges
19	Fabrication methods – Vacuum physics and vapor-phase techniques
26*	Fabrication methods – Plasma processes and process optimization
2 February	Fabrication methods - Plasma-surface interactions and diagnostics
9**	Fabrication methods – Thermal/Plasma spray technologies
16*	Optics of thin films 1, optical characterization, <i>Miniquiz1 (5%)</i>
23*	Optics of thin films 2, design of optical filters
1*** March	<i>Presentations – Emerging fabrication techniques (30%)</i>
	<i>March 4-8 - Winter/Spring break</i>
15**	Tribomechanical properties of films and coatings
22**	Electrochemical properties – corrosion and tribo-corrosion(<i>filter-20%</i>)
5 April	Passive functional films and coatings, <i>Miniquiz 2 (5%)</i>
12	Active functional films and coatings
16	Life cycle analysis and environmental impact
19***	<i>Presentations – Emerging applications of nanostructured films (40%)</i>

Deadlines:

Project #1 – Fabrication technique:

Choice of the subject: **26 January**

Abstract and references: **9 February**

Report and presentation: **1st March**

Projet #2 – Design of an optical filter:

Choice of the subject: **23 February**

Report: **22 March**

Projet #3 – Application of nanostructured thin films:

Choice of the subject: **16 February**

Abstract and references: **15 March**

Report and presentation: **19 April**